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A System of Fortran IV Computer Programs for Crystal Structure Computations

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A System of Fortran IV Computer Programs for Crystal Structure Computations

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ABSTRACT

This report gives detailed descriptions and instructions for use of a system of programs for crystallographic calculations, including least-squares refinement with generalized systems of constraints, calculation of bond distances and angles with errors, Fourier synthesis, plotting of contours in Fourier maps, and preparation of structure factor tables for publication.

Key Words:

Computer programs; contour plotting; constrained refinement; crystallographic calculations; Fourier section; Fourier synthesis; least squares

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These programs, although tested on many problems and several computing systems, may not give correct results in all circumstances. Therefore, neither the authors nor their institutions will guarantee the correctness of the program in all respects, but the authors will greatly appreciate being informed of discrepancies in the code or desirable options not currently included.

RFINE4: A program for least squares refinement
including general constraints

General Description

This program, called RFINE4, performs the calculations necessary to refine crystal structures using the techniques of full-matrix least-squares refinement. In addition, it can compute bond distances and angles or thermal ellipsoids so that these functions may be monitored throughout the various stages of a refinement. File control capabilities have been designed so that parameters may be saved at the end of a given computer run or, alternatively, virtually any parameter may be changed at almost any time.

A scheme of derivative modification and parameter restoration which eliminates the need for coding special subroutines to treat constrained parameters has been included in this program. This method will handle thermal and positional restrictions for atoms in positions of special symmetry and, in conjunction with the occupancy refinement capability, a multiposition, partially ordered structure may be constrained to a particular chemical composition. Provision has been made for incorporating parameters which are not members of the set used in conventional least-squares refinement. Any set of linear constraints may be specified, and also groups of atoms may be treated as rigid bodies both with respect to position and orientation (shape constraints) and with respect to thermal motion.

In its present form, the program allows a maximum of 60 atoms, 20 chemical species, 10 scale factors, 1320 parameter dependencies and 200 refined parameters for a structure in any space group. With the maximum number of parameters and no use of overlays the program requires approximately 65000 words of core storage. However more restricted problems can be operated in smaller core sizes, and the program can be further reduced in size by means of overlays. A suggested overlay structure is given in Appendix A. Some operating systems allow for dynamic allocation of core. Such provisions can be used to advantage.

File and Record Structure

In the following discussion a record is the unit of information formally defined as a logical record, i.e. the amount of information transferred in a single non-formatted read or write statement. This description is independent of any physical device which may be associated with the file and the program has been coded so as to operate fairly efficiently with any type of auxiliary storage currently available. Furthermore, a data set shall mean the collection of records needed to describe a structure. Any reference to file or data labels should not be confused with file control information for a particular computer system.

Master File. The file referred to as ISC1 and assigned to logical unit 10 is the main file of the program. This file consists of a data set containing all the information required to resume least-squares refinement. This data set has two label records, one or more structure factor records, a constraint relations record, a variance-covariance record, and a record containing variances of previously refined parameters (useful in large problems where the refinement must be "blocked"). The label records contain a 12-character alphanumeric identification tag, a cycle number and all the atom parameters, symmetry data and scattering factor information needed for this structure. The reflection data consist of the Miller indices, the observed structure factor on a relative scale, the standard deviation of F_{Obs} , the value of $\sin^2\theta/\lambda^2$ for the reflection, an integer specifying which scale factor applies to this reflection, β --the extinction parameter, a flag to mark reflections which had an intensity less than the minimum observable, the diffractometer angles χ , ϕ and $\omega + \theta$ in radians, and the value of each of the scattering curves for this reflection. These quantities are packed into a buffer, starting with word 2, until another reflection would require the buffer to be larger than 1023 words. An end of reflection records marker, which is non-zero only in the last block, is contained in word 1. The information for a single reflection is never split between two records and all records, including the last which may be only partially filled, are the same length. The end of the reflection list is marked by a Miller index h having a value of 3000. If the number of scattering curves is N , the number of reflections per record (n) may be found from the integral part of $1022/(N + 12)$. The length of the record is then 1023 minus 1022 modulo n . The variance-covariance record contains the variance-covariance matrix for the previous cycle of refinement in packed, upper triangular format.

Intermediate File. This file, named ISC2 and assigned to logical unit 29, contains the structure factor records for the current structure. A distinct file allows the scattering factor information to be changed without reading the structure factors from cards.

Auxiliary Files. A file named ISC3 and assigned to logical unit 11 is used as an alternative structure factor input. A file named ISC4 and assigned to logical unit 12 is used to pass information to Fourier synthesis, structure factor tabulation and statistical analysis programs. A file named ISC5 and assigned to logical unit 28 is used for temporary storage of constraint relationships.

System Files. This program uses a file named IN, logical unit 5, as a card read file, a file named IOUT, logical unit 6, as the print file, and a file named IPUN, logical unit 1, as the punch file. These assignments may be changed for a particular system by a block data subprogram.

Description of Routines

Main Program. The main program serves as a driver for the least-squares section. It reads one card which contains a 12-character label.

If a new data set is being constructed, this label will be inserted into that file. Control is then transferred to subroutine RFINE. If the updated information is written back to file ISCL, the subroutine exits normally. In that event, the main program prints a message stating that the file has been updated.

Subroutine RFINE. This routine is the primary one for the structure factor and least-squares calculation and is responsible for controlling the functions computed and the parameters used.

When this routine is first entered, initialization is accomplished and the main cycle loop is entered. The first step is to read the title and control cards for the cycle. If this is the first cycle of the current run, the new parameter indicators from the control card are interrogated and if all are non-zero, signifying that all parameters are to be loaded from cards, the data set on file ISCL is presumed not to exist; however, if any of the indicators are zero, the first two records of that data set are loaded into memory. Next, any new parameters required are read from cards. As new parameters are read, the values are printed.

If the unit cell parameters are to be changed, that card is read and the direct space metric tensor is prepared. This is a 3 x 3 symmetric matrix whose elements are the scalar products of the unit cell vectors. This matrix is then inverted using subroutine SYMINV described below. The inverse matrix is then the reciprocal space metric tensor and the determinant of the original matrix is the square of the unit cell volume. Note: If the unit cell parameters are to be changed, the structure factors must also be changed if the effects of the cell data are to be applied to the values of $\sin \theta/\lambda$.

New symmetry cards, if required, are now read. Each card lists an equivalent position in very nearly the same form as Vol. I of the International Tables with only one major difference; positions related by a center of inversion or lattice centering must not be included since they are internally generated. Using this scheme, all space groups may be generated by using a maximum of 24 cards. Each symmetry data card is transformed into matrices R and T satisfying the equation

$$X' = RX + T$$

with X' equal to the vector of transformed coordinates, X is the position vector with components, xyz, R is a 3 x 3 rotational matrix and T is a vector describing the translation associated with this symmetry operation.

At this point in the program, new scattering factor coefficients are read, if desired. We must emphasize two points of caution concerning the changing of the scattering factors. First, since the blocking of structure factors depends upon the number of scattering factors used, if that number is changed, new structure factors must be read. Violation of this rule will lead to unpredictable, but probably catastrophic, results. The second rule requires that the scattering factors be changed

only when file ISC2 is being written, that is, either on the first cycle of a given run or when new structure factors are being read from cards. If this restriction is violated, the new curves are loaded to core and subsequently included in the data set for this structure, but they are never used to compute scattering factors for the reflections.

The new atom parameters, if required, are now read from cards. The scale factors are read first, followed by the extinction parameters and the atom cards. The atom parameters needed are an identification label of 6 characters, an equipoint fraction which is the multiplicity of the position occupied by this atom divided by the multiplicity of an atom in the general position of this space group, the total occupancy of the site (usually one), the occupancy of species A (needed if more than one species present in this site), the identification of scattering factor(s) to be applied to this atom, fractional coordinates for the atom, and temperature factor information, as well as third and fourth cumulant parameters, consistent with the temperature factor type card described below. The forms of the cumulant expressions used in this program are:

$$F = \sum_j f_j \exp[i(2\pi \sum_k h_k x_k^j - \sum_{klm} \sum h_k h_l h_m c_{klm}) - \sum_{kl} (h_k h_l \beta_{kl}^j - \sum_{mn} \sum h_j h_l h_m h_n h_{klmn}^j)]$$

atoms

x_k^j is the k^{th} fractional coordinate of atom j , β is the array of anisotropic thermal coefficients, and c and d are the arrays of third and fourth cumulant coefficients. After the atom parameter cards have been read, the special parameter cards are read. The first card gives the total number of special parameters (up to 60). Then one card for each special parameter contains its name, three integers specifying its type, and its initial value.

At this point in the program, the parameter refinement selection information is read. A parameter of the model is varied in the least-squares refinement if its associated indicator is one; parameters with zero indicators are changed only if they are linked to refined parameters by dependency cards. If new parameter selection information is read, constraint data are also read. If no dependency relationships exist for this structure, a blank card must be included in the data deck. The method used to treat parameter constraints is from Finger (1969) and essentially consists of the application of the chain rule to the derivatives of the structure factor with respect to the parameters of the model. The user must determine the dependent parameters of the model using the rules of Levy (1956) for thermal coefficients or the equations of Finger (1969) for chemical constraints and then prepare the data cards. The program currently will not allow the constraining of the total occupancy for a site with only one species present; however, this may be accomplished by including a null scattering curve which is made the second species present. The amount of the first species may then be refined and constrained.

At this point, all structural data except the observed structure factors have been read. If these are to be read, a data card containing a FORMAT specification is read. Two optional cards may be read, one to specify the wavelength if it is needed for the computation of extinction corrections and the other to specify an "ignorance factor", ρ , to be used in computing weights according to the formula

$$w = 1/[\sigma^2 + (\rho F_{\text{obs}})^2].$$

Subsequently, the subroutine INPUT is called to read and process a reflection card. The data are then added to a buffer which, if full, is output on file ISC2. If the old structure factors are desired and this is the first cycle of a given computer run, the buffer is filled from file ISC1, the scattering factors are recomputed if necessary and the buffer is written on file ISC2. If this is not the first cycle of a given run, the old structure factors are read from file ISC2. After the data for a reflection have been obtained, the calculated structure factor and partial derivatives are computed in subroutine SFAC, the results tested to determine if this reflection should be used in the normal equations matrix, and the contributions of this reflection to the residuals are calculated. Next, the structure factors are printed, if desired, with the rejected data marked with a single asterisk in the right margin. In addition, the reflections having intensities less than the minimum observable value are marked with a single asterisk next to the value of F_{obs} and a double asterisk in the right margin.

If the reflection is to be included in the matrices, subroutine MATRIX is entered; then the next observation is processed. As soon as the end of the reflection list is encountered, the residuals for this cycle are printed. Next, the normal equations matrices are converted to correlation matrices to prevent overflow or underflow of the determinant during the matrix inversion, which is accomplished by subroutine SYMINV, adapted from Busing and Levy (1962). If the matrix is non-singular, the inverse is converted to a variance-covariance matrix and the parameter shifts are computed. Subroutine RESET is entered to compute the new values of any dependent parameters. The ratios of the parameter shifts to the standard deviations are tested to find the largest absolute value and the magnitudes of the ratios are averaged. At this point in the program, the correlation matrix, if requested, is printed. The twenty off-diagonal elements of the correlation matrix with largest absolute values are always printed. Then the optional bond functions are computed by routine BODAN1 and the thermal functions by routine ELVIB1.

Finally, a run continuation card is read. If column 1 is non-zero, another cycle is to be performed. However, if this column is blank or zero, the program prepares to terminate. If the new values for the parameters are not to be saved, the program exits. On the other hand, if these parameters are to be kept, a new label record is written on ISC1, the structure factor records are copied from ISC2 to ISC1 and the variance-covariance record is output. The current values of all parameters may be punched on cards. This routine then returns control to the main program.

Subroutine BODAN1. This subroutine uses the symmetry operators supplied on cards combined with the action of centers of symmetry, if present, and the effects of multiple lattice points and cell translations to generate all atomic locations within a spherical shell centered on each atom in the asymmetric unit. The search for the contents of this shell is done efficiently by enclosing the central atom with a unit cell shaped parallelepiped tangent to the sphere. For each location inside this box, a table of generated positions is checked to determine if this location is unique and if it is, the bond distance is computed. If this is within the desired range, the distance and coordinates are printed and this location is added to the table of generated positions.

If bond angles are also desired, each atom in the asymmetric unit is used as the central atom with the atom positions generated in the bond distance calculation considered. The peripheral atoms are identified only by their alphanumeric tag and a number which points to an entry in the bond distance output where the coordinates of the generated atom are listed. Caution--if the maximum bond distance is large, very many angles will be generated.

Subroutine ELVIB1. For each anisotropic atom, the equivalent isotropic temperature factor of Hamilton (1959), the root-mean-square (rms) amplitudes of vibration (in Å) of the principal axes and the orientations of these axes with respect to the direct cell axes are computed, or if the temperature factor matrix of an atom is nonpositive-definite, this is reported. This routine will also compute the thermal corrections to bonds using the formulae of Busing and Levy (1964). To assist the interpretation of the orientations of thermal ellipsoids relative to the bonding, the rms amplitude of the ellipsoid in the direction of the bond is computed and printed. BODAN1 is used to generate the necessary atomic locations.

Subroutine INPUT. This subroutine reads a reflection data card, computes $\sin^2\theta/\lambda^2$, evaluates the scattering factors for this observation and computes σ_F for the observation. Maximum and minimum values of F_{obs} and $\sin^2\theta/\lambda^2$, are determined in this routine.

Subroutine MATRIX. This subroutine calculates the derivatives of the residual from the derivatives of the calculated structure factor and accumulates the sums required in the normal equations matrices.

Subroutine MODIFY. This routine applies the equations

$$\frac{\partial A}{\partial p_n} = \sum_m \frac{\partial A}{\partial p_m} \frac{\partial p_m}{\partial p_n}$$

and

$$\frac{\partial B}{\partial p_n} = \sum_m \frac{\partial B}{\partial p_m} \frac{\partial p_m}{\partial p_n}$$

to the calculated derivatives. A and B are the real and imaginary portions of the calculated structure factor, p_n is the independent parameter, p_m

represents a dependent parameter, the summation is over all the dependencies, the unprimed derivative denotes the one calculated without regard for dependencies and the primed derivative is needed to form the least-squares matrices.

Subroutine RCALC. This subroutine accumulates the terms needed to calculate the discrepancy factors which are computed for all reflections and separately for those data used in the refinement. A weighted residual, R_w which is computed using the formula

$$R_w^2 = \frac{\sum w (|F_o| - |F_c|)^2}{\sum w |F_o|^2}$$

for refinement on F or

$$R_w^2 = \frac{\sum w (|F_o|^2 - |F_c|^2)^2}{\sum w |F_o|^4}$$

for refinement on F^2 , is determined for each class of data. In addition, the conventional discrepancy index

$$R = \frac{\sum ||F_o| - |F_c||}{\sum |F_o|}$$

is computed for all reflections in each class. In addition, the ranges of variation of F and $\sin^2\theta/\lambda^2$ are each divided into eight subranges and the sums needed for R are accumulated. (Note: the maximum and minimum values are dynamically determined during any cycle in which new structure factors are read and the distribution of residuals for such a cycle will be meaningless.) If the weighting scheme is correct, the expression $(1/s) \sum w (F_o - F_c)^2$, where the sum is taken over a subset of the full data set containing s reflections, should be independent of the composition of the subset. If we divide this expression by the constant $(1/t) \sum w F_o^2$, where t is the total number of reflections in the data set and the sum is taken over the entire set, and take the square root of the quotient, the result should also be independent of the composition of the subset. This number, which can be considered the average contribution to weighted R for reflections in the subset (Note that the expression is equal to weighted R if $s=t$.) is printed in the output for each subset.

Subroutine RESET. This subroutine is entered once for special parameters and once for each atom to compute the updated values of all dependent parameters. Linear relationships and rigid-body parameters are computed directly. Other non-linear systems of constraints may be handled by the user through subroutine SPVAL, supplied as a dummy.

Subroutine SFAC. This subroutine computes the structure factor and partial derivatives with the symmetry operators applied to reciprocal space; i.e. the Miller indices are transformed rather than the atomic coordinates. If H^T represents the transpose of the vector of Miller indices and X'

represents the j th symmetry transformed coordinate for the n th atom, then the argument of the trigonometric functions needed to calculate the contribution of this atom to the structure factor may be written as $H^T X'_{nj}$. Utilizing the expression for X' from page 3,

$$H^T X' = H^T (RX + T) = H^T RX + H^T T.$$

The final form is the method used in this subroutine.

As the routine is entered for each reflection, the matrix products $H^T R_j = H_j^T$ and $H^T T_j$ are computed and saved. Then the structure factors and partial derivatives are accumulated. If 3rd and 4th cumulant terms are absent, the structure factor

$$F = \sum_n a_n f_n \sum_j T_{nj} P_{nj}$$

with

$$P_{nj} = \exp [2\pi i (H_j^T X'_n + H^T T_j)]$$

and

$$T_{nj} = \exp (-H_j^T \beta_n H'_j)$$

for anisotropic atoms or

$$T_{nj} = \exp (-B_n \sin^2 \theta / \lambda^2)$$

for isotropic atoms, the n summation is over the atoms in the asymmetric unit, the j summation is over the symmetry operators, a_n is an occupancy term, f_n is the value of the scattering curve for the n th atom, i is $\sqrt{-1}$ and β_n is the matrix of anisotropic thermal coefficients. When anomalous dispersion is included, the scattering factor becomes

$$f_n = f_{o_n} + f'_n + i f''_n$$

with f_{o_n} the wave length independent part, f'_n the real part of the anomalous dispersion and f''_n the imaginary part. Including this expression in the structure factor equation, applying Euler's rule and writing F in the form $F = A + iB$, we find that

$$A = \sum_n \left[a_n (f_{o_n} + f'_n) \sum_j T_{nj} \cos 2\pi (H_j^T X'_n + H^T T_j) - a_n f''_n \sum_j T_{nj} \sin 2\pi (H_j^T X'_n + H^T T_j) \right]$$

and

$$B = \sum_n \left[a_n (f_{o_n} + f'_n) \sum_j \sin 2\pi (H'_j X_n + H^T T_j) \right. \\ \left. + a_n f''_n \sum_j \cos 2\pi (H'_j X_n + H^T T_j) \right]$$

The required partial derivatives are found by differentiating each of the above equations with respect to the components of X_n and β_j . After all sums have been accumulated, the subroutine MODIFY is called to perform any chainrule operations required. If this is to function properly, all derivatives must be calculated although the refinement indicators would suggest that certain derivatives are not needed.

Subroutine SFAC also includes an entry point named EXCALC which calculates the extinction factor of Zachariasen (1967) as extended by Coppens and Hamilton (1970), and revised by Nelmes and Thornley (1973). Using this scheme, the structure factor is corrected for extinction by the relationship

$$F_c^* = F_c y^{1/2} \\ y = (1 + \beta(\theta) F_c^2 r^*)^{-1/2}$$

$$\beta(\theta) = \begin{cases} \frac{-2 e^4}{m^2 c^4 V^2 A \sin 2\theta} \frac{(+ \cos^4 2\theta)}{(1 + \cos^2 2\theta)} \frac{dA}{d\mu} & \text{for x-rays} \\ \frac{\lambda^2}{V^2 A \sin 2\theta} \frac{dA}{d\mu} & \text{for neutrons} \end{cases}$$

λ is the wavelength, V is the cell volume, A is the transmission factor, μ is the linear absorption coefficient, and e , m and c have their usual meanings. The program allows three different forms for the extinction; a) isotropic with r^* refined, b) Type I anisotropic with $r^* = (\bar{D}'ZD)^{-1/2}$ with z_{ij} refined and c) Type II anisotropic with $r^* = (\bar{N}'WN)^{-1/2}$ with W_{ij} refined. If \bar{p} is a unit vector parallel to the incident beam and \bar{s} is a unit vector parallel to the diffracted beam, \bar{D} is a unit vector parallel to $\bar{p} \times \bar{s}$ and $\bar{N} = \bar{p} \times \bar{D}$. The reference coordinate system for Z and W is attached to the crystal and has its x -axis parallel to the incident beam and its z axis vertical when all diffractometer angles are 0.

Subroutine SYMINV. The method used by this matrix inversion routine has been described by Busing and Levy (1962) and was coded by Mr. James Mundstock of the Numerical Analysis Center of the University of Minnesota.

Subroutine REJECT. This routine may be used to exclude reflections from the normal equations matrices for other than the standard reasons. If a reflection is to be rejected, the variable NREJ in Common Block /F/ should be set to one.

Subroutine WEIGHT. This routine may be used to compute a non-standard weighting scheme. Upon entry, the information contained in the standard deviation field of the structure factor card will be in the variable WT in Common Block /F/. This variable must be set to the desired weight information when the routine is exited.

Subroutine RDEGN. This subroutine reads the dependent parameter information from cards, and rearranges the array of relationships in ascending order first of independent atom and parameter designators and then of dependent atom and parameter designators. Special parameters are arbitrarily assigned atom number 0.

Subroutine DERIVS. This subroutine is entered once at the beginning of each cycle. It computes the current values of derivatives of conventional parameters with respect to rigid body parameters. (Other non-linear derivatives may be supplied by the user through subroutine SPDERI). If any independent parameters are themselves actually dependent on other parameters (such as when the values of the elements of the rigid-body motion tensors are restricted by symmetry) the derivatives with respect to the true independent parameters are computed. Then the independent parameter designators are replaced by their row indices in the normal equations matrix, and the array is packed to eliminate any redundant relations.

Subroutine PAREXT. This subroutine reads the special parameter cards, and prints the names and initial values of the parameters.

Subroutine TRNFRM. This subroutine is entered once at the beginning of a run to compute the transformation matrices required to convert parameters from the crystal system to a standard orthonormal coordinate system and back again.

Subroutine FILLIN. This subroutine stores special parameter values in the proper positions in rigid-body parameter arrays.

Function ERRCAL. This function subroutine determines the standard deviation of a dependent parameter according to the approximate formula

$$\sigma_k' = \left(\sum_{i=1}^n \sum_{j=1}^n \frac{\partial P_k}{\partial P_i} \frac{\partial P_k}{\partial P_j} \sigma_{ij} \right)^{1/2},$$

where n is the number of refined parameters and σ_{ij} is the covariance of the ith refined parameter with the jth refined parameter.

Subroutine EULER. This subroutine computes an orthogonal matrix which is necessary to transform parameters from a general orthonormal coordinate system to the standard orthonormal coordinate system defined by x parallel to \underline{a} and z parallel to \underline{c}^* . The relative orientations are defined by Eulerian angles $\phi, \chi,$ and ω . Here ω is the angle through which the special coordinate system must be rotated clockwise, as viewed down the positive z axis of the standard system, about the z axis of

the standard system to bring the z axis of the special system into the x-z plane of the standard system; χ is a clockwise rotation about the y axis of the standard system (viewed down the positive y axis) to bring the z axes of the two systems into coincidence; ϕ is a clockwise rotation about the common z axis to bring the x and y axes into coincidence. Three additional entry points, DTDPHI, DTDCHI, and DTDOMG compute the derivatives of the elements of the transformation with respect to ϕ , χ , and ω respectively.

Subroutine MULMM. This subroutine forms the product of two 3 x 3 matrices. An alternate entry, MULMV, multiplies a three component column vector by a 3 x 3 matrix.

Subroutine TFM. This subroutine has two entry points. TFM2 transforms a second cumulant tensor in an orthonormal system to a set of anisotropic temperature factors in the crystal system. TFM3 does the same for a third cumulant tensor.

Subroutine TRNSPS. This subroutine generates the transpose of a 3 x 3 matrix.

Function IPAK. This function packs 4 integer variables into a single computer word. The version given is appropriate only to the UNIVAC 1108. Other versions must be used for other machines. If the integer word length of the machine is shorter than 32 bits other adjustments must be made.

Functions SKTLS, D2KDT, D2KDL, and D2KDS. These functions compute the second cumulants for an atom and their derivatives with respect to the rigid body motion parameters \underline{T} , \underline{L} , and \underline{S} .

Functions TKTLS, D3KDL, and D3KDS. compute the third cumulants and their derivatives with respect to \underline{L} and \underline{S} .

Subroutine CORECT. This subroutine applies libration corrections to the atomic positions in a rigid body.

Function DETERM and subroutine SOLVE are used by CORECT. Subroutine VXV forms the vector product of two vectors. Functions AIJ, BIJK, CIJKL, DIJKLM, EIJ, FIJ, AXA, AXAXB, PIJKLM, EL4. are a set of functions used in the rigid body relations.

Common Blocks and Variables

1. Common Block /LSMAT/

B(200)	Normal equations vector
IEXT	Extinction type indicator
IPARA (1000)	Atom Parameter refinement indicators
MRANK	Order of the normal equations matrices
KCYL	Cycle number for the data set
LABEL (3)	12 character label for the data set

JSCRF (10)	Refinement switches for scale factors
NRSF	Number of scale factors refined
SIGMA	Standard deviation of a parameter
MDEGN	Twice the number of constraint relationships
A(22740)	Constraints array and normal equations matrix or inverse. The dimensions are a maximum. The actual number for a given problem is given by the expression $MDEGN + (MRANK * (MRANK + 1)) / 2$. If, as on the UNIVAC 1108, the operating system allows dynamic core allocation, this number can be determined at run time.

2. Common Block /A/:

BETA(6,60)	Temperature factor coefficients
G(3,3)	Real space metric tensor
ISOT(60)	Temperature factor type indicators
NATOM	Number of atoms in the asymmetric unit
TAG(2,60)	Alphanumeric atom tags or labels
TITLE(18)	Alphanumeric title information
XYZ(3,60)	Atomic positions
PI	Value of π
CR(10,60)	Third cumulant coefficients
DR(15,60)	Fourth cumulant coefficients

3. Common Block /C/:

CELLP(3,4)	Coordinates of lattice points
ICENT	Centric indicator
JCELL	Number of lattice points
NSYM	Number of symmetry operators
RMAT(3,3,24)	Rotational symmetry operators
TRANS(3,24)	Translational symmetry operators

4. Common Block /D/:

ACALC	Real part of calculated structure factor
AIND(60)	Individual atom contributions to ACALC
ANOM(2,20)	Anomalous dispersion corrections
BCALC	Imaginary part of calculated structure factor
BIND(60)	Individual atom contributions to BCALC
DADB(6,60)	Derivatives of ACALC with respect to temperature factors
DADO(60)	Derivatives of ACALC with respect to occupancy
DADX(3,60)	Derivatives of ACALC with respect to position
DBDB(6,60)	Derivatives of BCALC with respect to temperature factor
DBDO(60)	Derivatives of BCALC with respect to occupancy
DBDX(3,60)	Derivatives of BCALC with respect to position

H(3)	Miller indices in real representation
IH(3)	Miller indices in integer representation
ISCAT(2,60)	Table used to select atomic scattering factor
ISCL	Number of scale factor for this reflection
MFSEL	Function selector
OCCA(60)	Occupancy of species A
OCCUP(60)	Total occupancy of site
SCALE(10)	Scale factors
SCAT(20)	Values of scattering factor for current reflection
SITE(60)	Equipoint fraction for atom site
DADC(10,60)	Derivatives of ACALC with respect to 3rd cumulant
DBDC(10,60)	Derivatives of BCALC with respect to 3rd cumulant
DADD(15,60)	Derivatives of ACALC with respect to 4th cumulant
DBDD(15,60)	Derivatives of BCALC with respect to 4th cumulant
AMINUS	ACALC for opposite absolute orientation
BMINUS	BCALC for opposite absolute orientation
DRDE(6)	Derivatives of r^* (extinction factor) with respect to coefficients of tensor
NDEGN	Number of constraint relationships

5. Common Block /E/:

DMAX	Maximum bond distance
DMIN	Minimum bond distance
RECELL(6)	Reciprocal cell lengths and cosines
EXANG(3)	ϕ , χ and $\theta + \omega$ (in radians) for current reflection

6. Common Block /F/:

DELTA	Weighted residual for current reflection
FCALC	Calculated structure factor
FOBS	Observed structure factor
FOMAX	Maximum observed structure factor
FOMIN	Minimum observed structure factor
IREJ	Rejection mode indicator
MREF	Refinement mode indicator
MREJ	Minimum observable indicator
NREJ	Used to indicate whether or not a reflection is rejected
NUMBER(36)	Counters for subdivisions of R factors
RDEN(36)	Denominators for R factors
RHO	Current value of $\sin^2\theta/\lambda^2$
RHOMN	Minimum value of RHO
RHOMX	Maximum value of RHO
RNUM(36)	Numerators for R factors

WT	Weight for current reflection
EXBETA	Factor $\beta(\theta)$ for extinction correction
EXX	Factor $\beta(\theta)F^2r^*$ used in extinction
EXY	$(1 + EXX)^{-1/2}$
FISGN	Absolute orientation parameter
IFSGN	Orientation determination indicator
EXTIN(6)	Extinction parameter matrix
KEXTRF(60)	Refinement switches for extinction parameters
DELMAX	Maximum permitted value of $\Delta F/\sigma_F$

7. Common Block /G/:

BUFF(1023)	Array used primarily for blocking structure factor records
FCURVE(9,20)	Scattering curve coefficients
FRMT(18)	Variable format specification for reading structure factors
IWT	Weight calculation type indicator
NSCAT	Number of scattering factors
BETFAC	Used in extinction correction
WVLNTH	Wavelength of radiation
WTFAC	"Ignorance factor" in computation of weights

8. Common Block /TAPE/:

IN	Logical unit number of the card read unit (5)
INN	Logical unit number of the structure factor input unit (5 or 11)
IOUT	Logical unit number of the print file (6)
ISC1	Logical unit number of the least-squares file (10)
ISC2	Logical unit number of the intermediate file (29)
ISC3	Logical unit number of the auxillary file (11)
ISC4	Logical unit number of the Fourier file (12)
ISC5	Logical unit number for saving constraints list (28)
IPUN	Logical unit number for punch file (1)

Dependent Parameter Input

In certain structures, the parameters of the model may not be independently variable. If they are merely constrained to have a fixed value, there are no difficulties as the refinement selection variable for this parameter is set to zero. However, if a parameter of the model is required to be equal to a linear combination of variable quantities, the situation is greatly complicated. In the least-squares refinement of such a structure, the contribution of the dependent parameter to the derivative of the structure factor with respect to the independent variable must be computed if the shifts are to be properly evaluated.

Similarly, the correct value of the dependent parameter must be restored at the end of the cycle if the structure factors are to be properly computed in the next cycle. This program utilizes a new algorithm to perform the derivative modification and parameter restoration. The method of preparing the input data cards will be shown with the aid of examples.

Example 1: Atom 6 is an anisotropic atom on a 3-fold axis parallel to c. Employing the rules of Levy (1956), the following relationships are required for this atom:

$$\beta_{13} = \beta_{23} = 0$$

$$\beta_{11} = \beta_{22} = 2 \beta_{12}$$

The first equations relate parameters to a constant and thus may be ignored. However, this is not the case for the second, and since β_{11} must be the independent variable, the following equations are applied as constraints to the least-squares solutions:

$$\beta_{22} = \beta_{11}$$

$$\beta_{12} = 1/2 \beta_{11}.$$

The resulting Parameter Constraint Cards (See page 24) for this situation would be:

<u>Dependent</u>		<u>Independent</u>		<u>Constant</u>	<u>Comments (not on card)</u>
6	6	6	5	1.0	$\beta_{22} = \beta_{11}$ for atom 6
6	8	6	5	0.5	$\beta_{12} = 0.5 \beta_{11}$
0					End of list

Example 2: Grunerite has four independent sites (atoms 1 to 4) for Fe and Mg, but the total amount of each is known from the chemical analysis. Therefore, we want to refine the values of the Mg-occupancies for the first three atoms and constrain the fourth to agree with the bulk chemistry. In the notation of Finger (1969), the constraining equation is

$$\sum_m b_m a_{mn} = C_n$$

with b_m the multiplicity of the m th site, a_{mn} the fractional occupancy for the n th species in the m th site, and C_n the total number of atoms of species n per unit cell. In grunerite, sites 1 through 4 have multiplicities 4, 4, 2, and 4 respectively and there are two formula units per unit cell. If we constrain the formula to be $Fe_{6.2}Mg_{0.8}Si_8O_{22}(OH)_2$ and substitute into the above equation, we find that

$$4a_{1Mg} + 4a_{2Mg} + 2a_{3Mg} + 4a_{4Mg} = 1.6$$

Solving for a_{4Mg} ,

$$a_{4Mg} = 0.4 - a_{1Mg} - a_{2Mg} - 1/2 a_{3Mg}$$

The Parameter Dependency Cards needed to constrain this chemistry would be:

<u>Dependent</u>	<u>Independent</u>	<u>Constant</u>	<u>Comments (not on card)</u>
4 1	0 0	0.40	Initialization
4 1	1 1	-1.0	Site 1 dependence
4 1	2 1	-1.0	Site 2
4 1	3 1	-0.5	Site 3
0			End of list

Alternatively, the latest version allows up to 5 independent parameters to affect one dependent one on the same card, so the first four cards above may be replaced by the card as follows:

4 1 0 0 0.40 1 1 -1.0 2 1 -1.0 3 1 -0.5

Note that when occupancies are constrained, the dependent value must first be initialized with a card containing zeros in the independent parameter fields.

Example 3: Like many chemical groups, phosphate groups often have thermal vibration that can be represented by the motions of a rigid body, which can be expressed as the elements of the \underline{T} , \underline{L} , and \underline{S} tensors introduced by Schomaker and Trueblood (1969). Expressions for the second and third cumulants of the probability distribution functions for individual atoms (Johnson, 1969) as functions of the elements of \underline{T} and \underline{L} are given by Prince and Finger (1973), and the corresponding expressions including \underline{S} can be readily derived (Prince, unpublished but given as a FORTRAN expression in this program). If atom 3 is an oxygen atom of a phosphate group and special parameters 1 through 24 are 3 coordinates of the origin to which the motions are referred, 6 elements of \underline{T} , 6 elements of \underline{L} , and 9 elements of \underline{S} , the constraint cards will be set up as follows: First, because of the so called "trace of \underline{S} singularity", the three diagonal elements of \underline{S} are not independent, and S_{33} can be set equal to $-S_{11} - S_{22}$ by means of the card 0 18 0 16 -1. 0 17 -1. The anisotropic temperature factors may depend on all of the rigid body elements, so there must be six cards of the form

3 5	0 4	0.	0-24	0.
3 6	0 4	0.	0-24	0.
3 7	0 4	0.	0-24	0.
3 8	0 4	0.	0-24	0.
3 9	0 4	0.	0-24	0.
3 10	0 4	0.	0-24	0.

Here the minus sign before the 24 indicates that the dependent parameter depends on special parameters 4 through 24 inclusive. The coefficients are given as zeros because, being non-linear, they change from cycle to cycle and are therefore computed in each cycle according to the current values of the refined parameters. Third cumulants are independent of \underline{T} , but may be dependent on any element of \underline{L} or \underline{S} . Therefore a typical constraint card for a third cumulant would have the form

3 12 0 10 0. 0-24 0.

The program uses the information on the constraint cards to allocate space in any array and then, in non-linear cases, fills in the space at the beginning of each cycle. Therefore if a given relationship is not listed it will never be used whether or not its value is actually zero. Because of symmetry some relationships, particularly those involving \underline{T} , may be identically zero. It will save space and almost certainly time to omit these from the list.

Details of Data Input

1. File Name Card: Columns 1-12 contain an alphanumeric label to be written into a new data set. This label will be printed when the file is read.
2. Title Card: Any desired Hollerith information in columns 1-72. This information appears at the top of most pages of the output.
3. Control Card:

<u>Column</u>	<u>Variable</u>	<u>Description</u>
1	MFSEL	Function selector 0 - Structure factors only 1 - Least-squares refinement
2	MSF	Structure factor output selector 0 - No structure factor output 1 - Printed structure factors 2 - Printed and written (for a Fourier program) on file ISC4 3 - Written on file ISC4
3	MCORR	Correlation matrix* 0 - Not printed 1 - Printed
4	MBODAN	Bond distance, angle selector 0 - None computed 1 - Distances only 2 - Distances and angles computed
5	MELVIB	Ellipsoids of vibration 0 - None computed

*The values of the 20 largest off-diagonal correlation coefficients will be printed for every least-squares cycle.

3. Control Card (Cont.):

<u>Column</u>	<u>Variable</u>	<u>Description</u>
		1 - Ellipsoids computed for anisotropic atoms
		2 - Ellipsoids and thermal corrections to bonds computed
6	MREF	Refinement type indicator 0 - Refine on F^2 1 - Refine on F^2
7	IFILE	Rewrite data set indicator 0 - Data set rewritten if this is the last cycle of the current run 1 - Data set not rewritten 2 - Data set rewritten. On input the standard deviations of parameters refined in previous cycles will be read in. 3 - Data set not rewritten. Standard deviations read in.
8	NEW(1)	If non-zero, read new cell parameters*
9	NEW(2)	If non-zero, read new bond distance limits
10	NEW(3)	If non-zero, read new symmetry operators
11	NEW(4)	If non-zero, read new scattering factors†
12	NEW(5)	If non-zero, read new scale factors and atom parameters. If equal to one, all atoms will be read If equal to two, only selected atoms will be read. If equal to 3 only scale and extinction will be read. If equal to 4 only special parameters will be read.
13	NEW(6)	If non-zero, read temperature factor type card
14	NEW(7)	If non-zero, read parameter selection card(s) and parameter dependency card(s)
15	NEW(8)	If non-zero, read new structure factors. Values 1, 2, and 3 correspond to various options for the order of the list, as explained below.

For all zero values in columns 8-15, the old values are read from file ISCl or the values in memory are used. The above integers are required for all cycles.

16-20	DMIN	Minimum bond distance in Angstroms. Needed only if NEW(2) \neq 0.
21-25	DMAX	Maximum bond distance in Angstroms. Needed only if NEW(2) \neq 0.

*Note that if the new cell parameters will affect $\sin\theta/\lambda$, and therefore the atomic scattering factors for various reflections, structure factors must be read in.

†Warning: New scattering factor curves must be read only in the first cycle of a given computer run or when new structure factors are being read in, or they will never be used in computation.

3. Control Card (Cont.):

<u>Column</u>	<u>Variable</u>	<u>Description</u>
26	ICENT	Centric indicator, needed only if NEW(3) \neq 0 0 - Centric 1 - Acentric
27	ICELL	Cell type indicator, needed only if NEW(3) \neq 0 0 - Primitive cell 1 - A-centered cell 2 - B-centered cell 3 - C-centered cell 4 - I-centred cell 5 - F-centered cell 6 - R-centered cell
28	MANOD	Anomalous dispersion indicator, needed only if NEW(4) \neq 0 0 - No corrections are to be used 1 - Include anomalous dispersion corrections
29-30	NSCAT	Number of scattering curves. This is needed only if NEW(4) \neq 0. (0 < NSCAT < 21)
31-32	NATOM	Number of atoms in asymmetric unit. This is needed only if NEW(5) \neq 0. (0 < NATOM < 61)
33-34	NSF	Number of scale factors. This is needed only if NEW(5) \neq 0. (0 < NSF < 11)
35	NEWEXT	Extinction change indicator (needed only if NEW(5) \neq 0) 0 - New extinction parameters not read 1 - Extinction parameters read from cards
36	IWT	Weight type, needed only if NEW(8) \neq 0. 0 - Standard deviation of F on cards 1 - Standard deviation of F ² on cards 2 - Weight on cards 3 - Sigma for F is to be computed in WEIGHT 4 - Compute weight in subroutine WEIGHT 5 - Standard deviation of F on cards will be altered by "ignorance factor" by $\sigma = (\sigma^2 + (pF)^2)^{1/2}$
37	INN	Structure factor source indicator, needed if NEW(8) \neq 0. 0 - Structure factors on cards 1 - New structure factors from file ISC3
38	IREJ	Rejection parameter, needed only if NEW(8) \neq 0. 0,5 - No reflections rejected 1,6 - Reject if I less than the minimum obs. 2,7 - Reject if I less than the minimum obs. or $ F_o - F_c /\sigma_F$ greater than DELMAX 3,8 - Reject if $ F_o - F_c /\sigma_F$ greater than DELMAX In both of these cases weights will be altered by $w' = w(1 - 3x^4 + 2x^6)$, where $x = F_o - F_c /(\sigma_F * \text{DELMAX})$ 4,9 - Use special routine REJECT

3. Control Card (Cont.):

<u>Column</u>	<u>Variable</u>	<u>Description</u>
NOTE: Values of IREJ from 5 to 9 allow the rejection mode to be changed even though NEW(8) = 0.		
39-43	DELMAX	Maximum allowable difference between observed and calculated structure factors on an absolute scale. This is needed only if NEW(8) \neq 0 and IREJ is 2 or 3, or if IREJ is 7 or 8.
44-53	JSCRF	Scale factor refinement switches (needed only if NEW(7) \neq 0)
54-59	KEXTRF	Extinction factor refinement switches (needed only if NEW(7) \neq 0)
60	JXPAR	Extra parameter indicator 0 - No extra parameters 1 - Extra parameters will be read (needed only if NEW(5) \neq 0)
61	IFSGN	Orientation determination parameter 0 - Do not determine the orientation 1 - Change to orientation with lower weighted \underline{r} (needed only if NEW(7) \neq 0)

4. Cell Card: Needed only if NEW(1) \neq 0.

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1-8	A(1)	\underline{a} axis length in angstroms
9-16	A(2)	\underline{b} axis length
17-24	A(3)	\underline{c} axis length
25-32	A(4)	Alpha in degrees
33-40	A(5)	Beta in degrees
41-48	A(6)	Gamma in degrees

5. Symmetry Cards: Needed only if NEW(3) \neq 0.

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1-3	JTNS(1)	Translational part of \underline{x}'
5-6	IRMAT(1,1)	First positional part of \underline{x}'
8-9	IRMAT(2,1)	Second positional part of \underline{x}'
11-13	JTNS(2)	Translational part of \underline{y}'
15-16	IRMAT(1,2)	First positional part of \underline{y}'
18-19	IRMAT(2,2)	Second positional part of \underline{y}'
21-23	JTNS(3)	Translational part of \underline{z}'
25-26	IRMAT(1,3)	First positional part of \underline{z}'
28-29	IRMAT(2,3)	Second positional part of \underline{z}'
34	IEF	End flag, non-zero on last card only 0 - Another symmetry card follows 1 - This is the last card

The translational operators are of the following form:

bbb 1/2 1/3 2/3 1/4 3/4 1/6 or 5/6. The positional operators are of the form bW = W or -W with W equal to X, Y, or Z and b signifies a blank. The symmetry position X Y Z must be included.

6. Scattering Factor Cards: Needed only if NEW(4) ≠ 0.

<u>Columns</u>	<u>Description</u>	
1-8	a ₁	These coefficients must satisfy the equation
9-16	b ₁	
17-24	a ₂	$f(x) = c + \sum_{i=1}^4 a_i \exp(-b_i x^2)$
25-32	b ₂	
33-40	a ₃	
41-48	b ₃	
49-56	a ₄	with x = sinθ/λ
57-64	b ₄	
65-72	c	
73-80	Identification	

Coefficients for scattering curves of this form have been tabulated by Cromer and Waber (1965) for relativistic Dirac-Slater wave functions, by Cromer and Mann (1968) for Hartree-Fock wave functions and by Doyle and Turner (1968) for relativistic Hartree-Fock wave functions. If anomalous dispersion coefficients are being used (MANOD = 1), the above card is followed by one with the real part of the anomalous dispersion in col. 1-8 and the imaginary part in col. 9-16. Coefficients for the hydrogen atom are given by Forsyth and Wells (1959).

NOTE: The scattering curves should be changed only on the first cycle of a given computer run or when NEW(8) = 1. New structure factors must be read (NEW(8) = 1) if the number of scattering curves is to be changed.

7. Scale Factor Cards: Needed only if NEW(5) ≠ 0.

The NSF scale factors are punched with 8 columns per value and 9 values per card and should be the values needed to place the calculated structure factors on the same scale as the observed.

8. Extinction Cards: Needed only if NEW(5) ≠ 0 and NEWEXT ≠ 0. Format (6E12.6)

<u>Columns</u>	<u>Value</u>
1-12	r* for isotropic extinction or r* ₁₁ for anisotropic
13-24	r* ₂₂
25-36	r* ₃₃
37-48	r* ₁₂
49-60	r* ₁₃
61-72	r* ₂₃

9. Atom Parameter Cards: Needed only if NEW(5) \neq 0.

If NEW(5) = 1, the entire atom list is read with two cards per atom.
 If NEW(5) = 2, the Atom Number is read with Format (I2) followed by the two cards for that atom. Card reading is terminated by a blank Atom Number card.

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
Card 1-6	TAG	Alphanumeric identifier
7-12	SITE	Equipoint fraction
13-18	OCCUP	Total occupancy of site
19-24	OCCA	Occupancy of species A in this site Needed only if multiple occupancy
Card 2 1-2	ISCAT(1)	Number of scattering curve for species A
3-4	ISCAT(2)	Number of scattering curve for species B (blank if single element in site).
9-15	XYZ(1)	\underline{x} of atom in fractional coordinates
16-22	XYZ(2)	\underline{y}
23-29	XYZ(3)	\underline{z}
30-36	BETA(1)	\underline{B} for an isotropic atom <u>or</u> β_{11} for an anisotropic atom
37-43	BETA(2)	β_{22}
44-50	BETA(3)	β_{33}
51-57	BETA(4)	β_{12}
58-64	BETA(5)	β_{13}
65-71	BETA(6)	β_{23}
73	IEF	Indicator of third cumulant
Card 3 -	Needed if IEF \neq 0.	
1-8	C ₁₁₁	
9-16	C ₂₂₂	
17-24	C ₃₃₃	
25-32	C ₁₁₂	
33-40	C ₁₂₂	
41-48	C ₁₁₃	
49-56	C ₁₃₃	
57-64	C ₂₂₃	
65-72	C ₂₃₃	
73-78	C ₁₂₃	
80	IEF ³	Fourth cumulant ind.

Card 4-5 - Needed if IEF \neq 0.

Punch d_{1111} , d_{2222} , d_{3333} , d_{1112} , d_{1113} , d_{1122} , d_{1133} , d_{1222} , d_{1223} ,
 d_{1233} , d_{1333} , d_{2223} , d_{2233} , d_{2333} in order with 8 columns per value.

10. Special parameter cards: Needed only if NEW(5) \neq 0 and JXPAR \neq 0.

Card 1: Columns 3-4 contain the number of special parameters, NPAR.

If NPAR>0 the succeeding cards contain the names, initial values, and identifiers according to the following form.

Columns 1-8	Name of parameter, up to 8 alphanumeric characters.
Columns 9-10	Type of parameter, 0-linear function with coefficient given on constraint card. 1-rigid body system 2-defined by user in subroutines SPVAL and SPDERI
Columns 11-12	Integer indicating which rigid-body system, if more than one, this parameter refers to.
Column 13-14	Parameter designator. If the type is 1 the code is as follows 1-X coordinate of origin (in crystal axes system) 2-Y coordinate of origin 3-Z coordinate of origin 4- ω angle for transformation to standard, orthonormal coordinate system 5- χ angle for transformation 6- ϕ angle for transformation 7-X coordinate of an atom in the special system 8-Y coordinate of an atom 9-Z coordinate of an atom 10-T ₁₁ 11-T ₁₁ 11-T ₂₂ 12-T ₃₃ 13-T ₁₂ 14-T ₁₃ 15-T ₁₃ 16-L ₂₃ 16-L ₁₁ 17-L ₁₁ 17-L ₂₂ 18-L ₂₂ 18-L ₃₃ 19-L ₃₃ 20-L ₁₂ 20-L ₁₃ 21-L ₁₃ 21-L ₂₃ 22-S ₂₃ 23-S ₁₁ 23-S ₂₂ 24-S ₂₂ 24-S ₃₃ 25-S ₃₃ 26-S ₁₂ 26-S ₁₃ 27-S ₁₃ 27-S ₂₃ 28-S ₂₃ 28-S ₂₁ 29-S ₃₁ 29-S ₃₂ 30-S ₃₁ 30-S ₃₂

Columns 15-24 initial value of this parameter.

11. Extinction and Temperature Factor Type Card: Needed only if NEW(5) or NEW(6) \neq 0.

Column 1 contains the extinction factor code:

0 - Isotropic, do not change

1 - Anisotropic Type I (mosaic spread dominates)

- 2 - Anisotropic Type II (domain size dominates)
- 3 - Now Isotropic, change to Type I
- 4 - Now Isotropic, change to Type II
- 5 - Now Type I, change to Isotropic
- 6 - Now Type II, change to Isotropic
- 7 - Now Type I, change to Type II
- 8 - Now Type II, change to Type I

The temperature factor type code is punched with one column per atom beginning in Col. 2 with the following code:

- 0 - Now isotropic, do not change
- 1 - Now anisotropic, do not change
- 2 - Now isotropic, change to anisotropic
- 3 - Now anisotropic, change to isotropic
- 4 - Now 3rd cumulant, do not change
- 5 - Now anisotropic, change to 3rd cumulant
- 6 - Now 3rd cumulant, change to anisotropic
- 7 - Now 4th cumulant, do not change
- 8 - Now 3rd cumulant, change to 4th
- 9 - Now 4th cumulant, change to 3rd

12. Parameter Selection Cards. Needed only if NEW(7) \neq 0. If JXPAR \neq 0 the first card contains refinement selection for the special parameters in the first NPAR columns. A zero in a column means that the corresponding parameter will not be refined and a one means that it will. After this cards with the refinement indicators for the conventional parameters punched in columns 1-80. If the number of atom parameters is such that more than 80 values are required, the parameter selection information should be continued in column 1 of the next card. The order of parameters is:

- a) occupancy - If single occupancy, the total occupancy is refined. If multiple occupancy, the occupancy of species A is refined.
- b) x coordinate
- c) y coordinate
- d) z coordinate
- e) thermal parameters, one for isotropic atoms, six for anisotropic atoms. The thermal coefficients occur in the same order as on the Atom Parameter Card 2.
- f) 3rd and 4th cumulant parameters (if needed).

13. Parameter Constraint Cards(s): Needed only if NEW(7) \neq 0.

a) <u>Columns</u>	<u>Description</u>
1-3	Integer specifying the dependent atom number.
5-6	Dependent parameter number. This number is 1 for occupancy, 2-4 for x through z respectively, 5 for <u>B</u> or β_{11} , and 6, 7, 8, 9, 10 for β_{22} , β_{33} , β_{12} , β_{13} and β_{23} respectively. Values of 11 to 20 treat 3rd cumulant parameters and 21-35 are for the 4th cumulants.

13. Parameter Constraint Cards(s) (Cont.):

a) Columns	Description
7-9	Atom number of first independent parameter. Special parameters are arbitrarily indicated as atom number 0.
10-12	Parameter number of first independent parameter. Atom 0 parameter 0 designates an initializing constant in a linear constraint function.
13-20	Coefficient of first relationship.
21-23	Atom number of second independent parameter
24-26	Second independent parameter number
27-34	Second coefficient
35-37	Third independent atom number
38-40	Third independent parameter number.
41-48	Third coefficient
49-51	Fourth independent atom number
52-54	Fourth independent parameter number
55-62	Fourth coefficient
63-65	Fifth independent atom number
66-68	Fifth independent parameter number
69-76	Fifth coefficient.

If the independent atom number is zero, designating a special parameter, and the constraints are non linear, the second and fourth independent parameter numbers may be negative to denote the end of an inclusive list beginning with the first (third) independent parameter number.

b) One (1) blank card or a card with zero in column 3.

14. Structure Factor Cards: Needed only if NEW(8) \neq 0.

a) Format Card: This card contains the format of the input structure factor data. The number and order of variables on a card (or tape record) depends on the value of NEW(8), as explained in detail below. All records must contain at least four integer fields, for the indices and an observed/unobserved indicator, and two floating point fields for F_{Obs} and σ_F or other weight information. They may contain other information, such as a scale factor group identifier, the factor $\beta(\theta)$ used in extinction corrections, and the setting angles, needed for anisotropic extinction corrections.

b) Only if IWT=5 include a card with the "ignorance factor" punched as a real number in the first 8 columns.

c) Only if NEW(8)=3 include the wavelength in Å in the first 8 columns. For neutron data only an approximation to $\beta(\theta)$ will be computed according to the formula $\beta(\theta) = [(2\lambda^2/(V^2\sin^2\theta))] \times 10^8$, where V is the unit cell volume in Å³. The refined quantity then will be the product \bar{T}^* , with \bar{T} assumed to be approximately constant.

- d) Data Cards in a form consistent with Format Card: If NEW(8)=1 the list is in this order.

<u>Variable</u>	<u>Description</u>
IH(1)	h for reflection
IH(2)	k
IH(3)	l
FOBS	Observed structure factor
SIGMA	Weight information consistent with IWT on Control Card
EXBETA	Factor $\beta(\theta)$ for extinction
I	Number of scale factor for this reflection. If zero, the scale factor is the same as the preceding reflection. Scale factor 1 is assumed for the first reflection.
MREJ	Minimum Observable Parameter 1 - Intensity above minimum observable. 2 - Intensity below minimum observable.
IEF	End-of-list marker, zero on all data cards
TTH	2θ These angles are needed only if anisotropic
OMEG	ω extinction is to be calculated and must
CHI	χ conform to the diffractometer conventions
PHI	ϕ given by Busing and Levy (1967, p. 458).

If NEW(8) = 2 the input list is IH(1), IH(2), IH(3), MREJ,I,FOBS,EXBETA, SIGMA, with the same meanings as above. The end of the data must be marked by an end-of-file.

If NEW(8) = 3 the list is IH(1), IH(2), IH(3), MREJ,FOBS,SIGMA. EXBETA is computed, and again the end of data must be marked by an end-of-file.

- e) End-of-list card - A card with a non-zero value in the field of variable IEF or an end-of-file card appropriate to the system.

15. Run Continuation and Parameter Punch Card: Needed for all cycles.

<u>Column</u>	<u>Variable</u>	<u>Description</u>
1	ICONT	0 - No more cycles. The data set on file ISCI will be updated if IFILE from the Control Card is zero
2	JPUN	1 - Read a new title card and start another cycle 0 - Do not punch any atom parameters 1 - Punch atom cards in form required by 'X-RAY67' 2 - Punch atom cards in form required by this program
3-4	ISCI	3 - Punch atom cards in both forms If this field is non-zero its value will be substituted as the unit number for the binary master file, making it possible to try new courses of refinement without destroying previous stages.

BONDAN: A program for computing bond distances, angles, and thermal ellipsoids, with errors

This program uses the master binary file created by RFINE to compute bond distances and angles, and also thermal ellipsoids, with associated standard deviations. If the rigid body model is used, the atomic positions of the rigid body will be corrected for libration before calculation of distances and angles. The program will also accept input from cards by means of the program BADTEA. The complete description of BADTEA is included in Appendix B. The details of data input are as follows:

1. Input format indicator card

Col. 1-2 1-input from cards via BADTEA.
 2-input from binary file created by RFINE.

If the input format indicator is 1, see appendix B for further input. If the input format indicator is 2, the card input continues as follows.

2. Title Card: Any desired hollerith information in columns 1-72.

3. Search Card: Format(I2,3A4)

If column 2 is zero or blank, a search of the data tape will be made to find a data set with a label the same as columns 3-14. The error calculation will be performed on that data set. If column 2 is non-zero, the first data set on the tape will be used in the error calculation.

4. Parameter Card: Format(2I1,3F8.0)

<u>Column</u>	<u>Variable</u>	<u>Description</u>
1	MBODAN	Bond distance, angle selector 0 - None computed 1 - Distances only 2 - Distances and angles computed
2	MELVIB	Thermal ellipsoid selector 0 - No ellipsoids computed 1 - Thermal ellipsoids computed for anisotropic atoms
3-10	DLIMIT(1)	Minimum bond distance output
11-18	DLIMIT(2)	Maximum bond distance used in angles output
19-26	DLIMIT(3)	Maximum bond distance output

5. Cell variance-covariance matrix: Format(6E12.6)

This matrix is the matrix output by the lattice constant program of C. W. Burnham.

<u>Column</u>	<u>Description</u>
Card 1	
1-12	Variance of \underline{a} (in angstroms**2)
13-24	Covariance of \underline{a} with \underline{b}
25-36	Covariance of \underline{a} with \underline{c}
37-48	Covariance of \underline{a} with alpha (in angstrom-radians)
49-60	Covariance of \underline{a} with beta
61-72	Covariance of \underline{a} with gamma
Card 2	
1-12	Variance of \underline{b}
13-24	Covariance of \underline{b} with \underline{c}
25-36	Covariance of \underline{b} with alpha
37-48	Covariance of \underline{b} with beta
49-60	Covariance of \underline{b} with gamma
61-72	Variance of \underline{c}
Card 3	
1-12	Covariance of \underline{c} with alpha
13-24	Covariance of \underline{c} with beta
25-36	Covariance of \underline{c} with gamma
37-48	Variance of alpha (in radians**2)
49-60	Covariance of alpha with beta
61-72	Covariance of alpha with gamma
Card 4	
1-12	Variance of beta
13-24	Covariance of beta with gamma
25-36	Variance of gamma

If the errors in the cell constants have a small effect on the distances, the last 4 cards may be replaced by blanks.

FOURIER

This program uses the binary structure factor file created by RFINE (ISC4-unit 12) as input for a Fourier synthesis. The map is written on unit 11 for input to the plotting program CNTPLT or the arbitrary section program ARBSECT. The details of data input are as follows:

1. Title Card: Any desired alphanumeric information in columns 1-72. This information heads all map sections.
2. Parameter Card: Format (6I1, 2X, 9I4, 3F8 0.4)

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1	ITYPE	Map type indicator 0 - Fourier map 1 - Difference Fourier
2.	ISECT	Section parameter 0 - \underline{x} across, \underline{y} down and \underline{z} sections 1 - \underline{x} " " \underline{z} " " \underline{y} " 2 - \underline{y} " " \underline{x} " " \underline{z} " 3 - \underline{y} " " \underline{z} " " \underline{x} " 4 - \underline{z} " " \underline{y} " " \underline{x} " 5 - \underline{z} " " \underline{x} " " \underline{y} "
3	INCENT	Centric indicator 0 - Centric 1 - Acentric
4	KREJ	0 - Ignore rejection flag and include all reflections. 1 - Do not include any reflections with the rejection flag set.
5	IPLT	If non-zero, map sections will be written to unit S2 for plotting or calculation of an arbitrary section.
6	LSPC	If zero, the lines of the map will be double spaced. A non-zero value indicates single spacing.
9-12	IX	Number of divisions along horizontal axis (>0)
13-16	IXI	Initial point
17-20	IXF	Final point
21-24	IY	Number of division along vertical axis (>0)
25-28	IYI	Initial line
29-32	IYF	Final line
33-36	IZ	Number of divisions along section axis (>0)
37-40	IZI	Initial section
41-44	IZF	Final section
45-52	EXXAG	Map exaggeration desired
53-60	FOOO	Number of electrons in unit cell for Fourier.

E. Additional Problems:

If additional maps are to be run using the same structure factor list, a complete set of cards beginning with the Title Card should be included. An end-of-file in the card stream terminates the program.

LISTFC

This program is an adaption of the XRAY67 program LIST FC (Stewart et al., 1967). It has been altered to stand alone and read the structure factor file (ISC4 - unit 12) created by RFINE. The output of the program has been changed so that the "phase in millicycles" has been replaced by sigma (Fobs). Input is as follows:

Card 1.

Col. 1-6 compound identification; Col. 7-78 any title.

Card 2.

Col. 14 (1)/(2)/(3) for h index varies (most)/(next most)/(least) rapidly

15 Same for k index

16 Same for l index

(Note that the sum and product of Cols. 14, 15, and 16 must equal 6.)

17-20 Number of lines per list page.

21 (blank)/(A) for (DO)/(DO NOT) internally change the value of the number of lines in order to make the bottom of the last page as even as possible.

22-24 Number of list columns per page. Note that the product of the number of lines and the number of columns cannot exceed 2000. That is no more than 3000 items for the number of reflections and headings (including spaces) per page.

26 Number of blank print columns before the LISTFC column.

28 Number of print columns for most rapidly changing index.

30 Number of print columns for F_{obs}

32 Number of print columns for F_{calc}

34 Number of print columns for σ_F

36 Special flag for unobserved reflections (blank=*)

38 Special flag for severely extinct reflections (blank=E)

40 Special flag for special reflection (JCODE=4)

The next eight fields are (blank)/(1) for (do not)/do

42 Print symbol for unobserved or severely extinct reflections.

This symbol switch adds one print column

44 For centric structures, attach sign of A to F_{calc}

46 Double space the lines

48 Restore each LISTFC page to the top of the printer page

50 Print title at the top of each printer page

52 Punch a set of "FCARD" cards

56 Print a minus sign on F_{obs} for unobserved reflections

58 Write a separate copy of FC list on unit 7

62 Number of times to try to get headings at the top of all columns

64 (1)/(2)/(3) for headings separated by (no blank
lines)/(1 blank line above)/(1 above and 1
below) (blank=3)

65-72 factor F_s are to be multiplied by (blank=10)

73-80 factor σ_s are to be multiplied by (blank=10)

Note that all F and σ values are printed as integers,
so that scale factor must be sufficient to preserve a
sufficient number of significant figures.

CNTPLT

CNTPLT is a contour plotting program for Fourier maps and other similar functions. The routines contained in this program have been derived from multiple sources with the original version of subroutine ICONT written by S. H. Zisk and N. M. Brenner of M.I.T. Lincoln Lab. Subroutine INTPLT uses the rational polynomial spline interpolation of D. V. Ahuja, I.B.M. Systems Journal, p. 208-217, (1968). The other routines have been modified from code prepared by G. Ford, Purdue University.

The present version of these routines have been written to be as machine independent as possible. It is believed that only the call to the plotter function PLOTS (Sequence No. A5300) and the two functions MARK and UNMARK called by ICONT are machine specific. This is the main contribution of the present author (LWF).

Method

The main contouring subroutine, ICONT, takes the function values at the grid points of the map and computes the coordinates of the intersection of a specified contour line with the lines of the grid. Linear interpolation is used in this process. The second contouring subroutine, CPLOT, coordinates the drawing of the contours and produces any desired contour labels. The third contouring routine, INTPLT, produces a smooth curve through the intersections located by ICONT. Rational cubic polynomials are used to fit a spline-like curve through neighboring points. Two such curves meet smoothly because the first and second derivatives are single valued along the composite curve. The plotter line is drawn as a series of straight line segments with the number of such segments specified by the user.

The main program includes various options which allow labeling of plot sections and/or grid points, drawing of the bounding parallelogram, and other similar functions.

Input

The values of the function to be plotted are read from a binary input file (unit 10) with each section occupying two records. The first contains the variables MA, MB, JZ, MZ where MA and MB are the number of grid points along x and y respectively. The second record contains the data for the map section at JZ/MZ. These data are assumed to be in real form and are packed in an array which is MAXMB. The output file produced by program FOURIER is in this form.

Input

1. Title Card: Format (20A4)
2. Control Card: Format (F5.0, I5,3F5.0,6I5,F5.0,2I5)

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1-5	TLEHGT	Plotting height of title in inches. If ≤ 0 , no title will be plotted
6-10	NLABL	Number of vertex labels to be plotted
11-15	A	Width of plot (in inches) parallel to <u>x</u> -axis of Fourier. If $A > 0$, an 11' plotter is assumed. If a 30" machine is available, A should be less than zero.
16-20	B	Length of plot (in inches) parallel to <u>y</u> -axis of Fourier which is parallel to plotter <u>x</u> -axis.
21-25	ALP	Angle between Fourier axes (in degrees)
26-30	NA	Number of grid points parallel to Fourier <u>x</u> -axis
31-35	NB	Number of grid points parallel to Fourier <u>y</u> -axis
36-40	NP	Number of interpolation points per spline. The default value is 4.
41-45	NCONT	Number of sets of contour levels (NCONT ≤ 10)
46-50	NLINE	Number of line vertices specified (NLINE ≤ 20)
51-55	NCROSS	Number of crosses to be placed on plot (NCROSS ≤ 20)
56-60	SCROSS	Size of cross (in inches)
61-65	NSECT	Number of sets of sections specified
66-70	NZ	Grid spacing of section levels.

3. Contour Card(s): Format (3F5.0,I5)
There should be NCONT of these cards.

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1-5	SBEG	Height of initial contour
6-10	CSTEP	Step between contours
11-15	SLIM	Height of final contour
16-20	NSIG	Number of digits after decimal point in contour label. If NSIG < 0 , contours will not be labelled.

4. Line Vertex Card(s): Format (16F5.0)

The positions of the line vertices in map grid coordinates should be punched. A line will be drawn from point i to point i+1 if $x_{i+1} > 0$. No line will be drawn if $x_{i+1} < 0$. Omit these cards if NLINE ≤ 0 .
Note: The first grid point is (1,1), not (0,0). i.e. add (1,1) to scaled coordinates.

5. Cross Card(s): Format (16F5.0)

The map grid coordinates of the crosses should be punched sequentially. Omit these cards if NCROSS \leq 0.

6. Section Selection Cards: Format (3I5)

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1-5	INITZ	Sections from INITZ
6-10	ISTEPZ	to IFINZ in steps
11-15	IFINZ	of ISTEPZ will selected and contoured.

There should be NSECT of these cards.

7. Vertex Label Card(s): Format (5F5.0,A6)

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1-5	WX	x-grid coordinate
6-10	WY	y-grid coordinate
11-15	DX	Plotter x-axis offset
16-20	DY	Plotter y-axis offset
21-25	HGT	Label height in inches
26-31	LABL	Alphanumeric label

There should be NLABL of these cards.

Tape output for Calcomp plotter is on Unit 12.

ARBSECT

This program calculates an arbitrary section of a Fourier map from a complete set of sections calculated in regular intervals parallel to the crystallographic axes. The input sections may be computed with the regular Fourier program and are assumed to be in file No. 11. The plane of the output section is specified by the coordinates of the plane to be calculated.

Program ARBSECT has several options available. If only a fraction of the unit cell is used as input, it will calculate the electron density in the accessible portion only with the remainder replaced by asterisks in the printout. However, if the map for a complete unit-translation has been computed, the program will use the translation symmetry to calculate a complete section. No other symmetry operations are used. Other options include (a) describing the points used to define the plane in terms of map or fractional coordinates as desired, (b) saving the resulting section in file 12 for later plotting, (c) computing the entire section or selecting a portion of it, and (d) calculating and printing the geometry including axial lengths and interaxial angle, of the output section.

Method

The input coordinates of the three points defining the plane are initially converted to map coordinates if necessary. The coefficients of the plane in the equation $a_1x + a_2y + a_3z + a_4 = 0$ may be found from the determinant equation

$$\begin{vmatrix} x & y & z & 1 \\ x_1 & y_1 & z_1 & 1 \\ x_2 & y_2 & z_2 & 1 \\ x_3 & y_3 & z_3 & 1 \end{vmatrix} = 0$$

where x_i , y_i , and z_i are the coordinates of the i 'th point. This plane will have a line of intersection with each section of the original map. For the values of y and z corresponding to each line and section of the output map, the x -coordinate of this point in the plane is determined. A cubic function of the form $ax^3 + bx^2 + cx + d$ is fitted to the four adjacent grid points on the line, and the value of this function at the intersection point is used for the output at that y and z . This process is repeated until all output points have been determined.

Input

The input map sections are read from file 11 and the resulting map is output to file 12. These assignments may be changed by redefining variables ISC and ISCl respectively.

1. Title Card - Format (18A4)

Columns 1-72 of this card may contain any desired information.

2. Control Card - Format (8I3)

<u>columns</u>	<u>Variable</u>	<u>Description</u>
1-3	IO	If IO≠0, the output section will be written on Unit 12.
6	IZO	Section number of output
9	ISPC	If ISPC = 0 the output map will be single spaced; double spaced if ISPC=1.
12	IMRK	If IMRK=0, the y- and z- limits of the input sections will be used as the x-, and y-limits, respectively, of the output section. If IMRK ≠0, these values are read from this card.
13-15	IYI	Initial value of x in transformed section
16-18	IYF	Final value of x in transformed section
19-21	IZI	Initial value of y in transformed section
22-24	IZF	Final value of y in transformed section

3. Cell Card - Format (6F8.0)

<u>Columns</u>	<u>Description</u>
1-8	Length (in Å) of cell axis across page in original section
9-16	Length of cell axis down page in original section
17-24	Length of cell axis out of page in original section
25-32	Angle (in degrees) between axis 1 and 2
33-40	Angle between axes 1 and 3
41-48	Angle between axes 2 and 3

The above length and axes are required only if the program is to compute and print the axial length and interaxial angle of the transformed section. If not, this card may be blank.

4. Plane Card - Format (9F8.0, I2)

<u>Columns</u>	<u>Description</u>
1-8	x- coordinate of first point
9-16	y- " " " "
17-24	z- " " " "
25-32	x- " " second "
33-40	y- " " " "
41-48	z- " " " "
49-56	x- " " third "
57-64	y- " " " "

4. Plane Card - (Cont.)

<u>Columns</u>	<u>Description</u>
65-72	z- coordinate of third point
74	Coordinate type indicator. If zero, the coordinates are given in grid spacings. If non-zero, the points are given in fractional coordinates.

Additional arbitrary slices may be computed by supplying additional data decks beginning with the Title Card.

Form of Input Sections

The input Fourier sections are read from Unit 11 with unformatted reads. There must be two records per section as follows:

Record 1:

<u>Word</u>	<u>Variable</u>	<u>Description</u>
1	JXA	Number of grid points calculated parallel to x
2	JYA	Number of grid points calculated parallel to y
3	KZC	Section number
4	IZ	Number of sections per unit cell
5	IX	Number of intervals per unit cell parallel to x
6	IXI	Initial grid points parallel to x
7	IXF	Final grid point parallel to x
8	IY	Number of intervals per unit cell parallel to y
9	JYI	Initial grid point parallel to y
10	JYF	Final grid point parallel to y
11	JZI	Initial grid point parallel to z
12	JZF	Final grid point parallel to z

Record 2:

This record consists of the JXA*JYA values of the map in this section. These real values must be packed in an array with the x coordinate as the first subscript and y as the second subscript.

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Appendix A
Overlay scheme for RFINE

When program RFINE is run under operating systems which charge according to the product of core allocation and CPU time, substantial savings can be achieved by using an overlay structure which causes only that portion of the program which is actually needed to be resident in core. Furthermore, there can be large savings if the core allocated for the dependency list and the normal equations matrix can be adjusted as appropriate to a particular problem. On UNIVAC machines operating under EXEC 8 this latter function is accomplished dynamically at run time by means of the subroutine CORSZ, which makes use of executive requests ER MCORE\$ and ER LCORE\$. On other machines which don't have a similar function capability, this can be achieved by a run time recompilation of the short main program, with the dimension of the array A in common block LSMAT appropriately adjusted.

The program has been run successfully with a structure consisting of a main stem and three overlay segments as follows:

Main stem: main program, subroutines RFINE and CORSZ.

Overlay 1: Subroutines RESET, DERIVS, RDEGN, and PAREXT plus auxiliary functions called by them, including DIJKLM, DETERM, EL4, PIJKLM, BIJK, CIJKL, AIJ, VXV, SOLVE, EIJ, FIJ, IPAK, PDEGN, D3KDS, D2KDS, P3KDL, P2KDL, D2KDT, TKTLS, TFM, SKTLS, CORECT, MULMM, TRNSPS, EULER, FILLIN, SPVAL, ERRCAL.

Overlay 2: Subroutines INPUT, SFAC, RCALC, MATRIX, MODIFY, and SYMINV.

Overlay 3: Subroutines TRNFRM, BODAN1, and ELVIB1.

Appendix B

BADTEA-Alternate input for bond distances and angles, and thermal ellipsoids

A. IDENTIFICATION

TITLE: Crystallographic error analysis

NAME: U M BADTEA

PROGRAMMER: Larry W. Finger

DATE: December 27, 1965 (revised November 1968)

B. PURPOSE

U M BADTEA (University of Minnesota program for computing Bond angles and Distances, and Thermal Ellipsoids with error Analysis) will calculate bond distances, bond angles, thermal ellipsoids and the errors associated with each computed value. The program was converted to Fortran IV with the assistance of C. T. Prewitt.

C. USAGE

1. Input deck order:

Title card
Cell card
Function card
Symmetry card(s)
*Standard Deviations of cell parameters
*Correlation matrix of cell parameters
Atom cards
*Temperature Factor Standard Deviations
*Temperature Factor Correlation matrix
*Atomic Position Standard Deviations
*Atomic Position Correlation Matrix

*These data may not be needed. The next section describes in detail the conditions requiring these input data. All input from Atom Cards to the end of the deck may come from a modified ORFFF tape.

2. Description of input deck:

a. Title Card

FORMAT (18A4)

Columns

Description

1 - 72

Identifier for problem. This should be any title which identifies the compound.

b. Cell Card

FORMAT (6F10.5)

Columns	Description
1 - 10	\underline{a} axis length, in Å
11 - 20	\underline{b} axis length
21 - 30	\underline{c} axis length
31 - 40	α in degrees
41 - 50	β
51 - 60	γ

c. Function Card

FORMAT (5I4, 3X,A1,6X, 3F10.5)

Columns	Description
1 - 4	Number of atoms in asymmetric unit (≤ 60)
5 - 8	Centric Indicator 0 - Structure is centric 1 - Structure is non-centric
9 - 12	Bond Distance, Angle Parameter 0 - No angles or distances calculated 1 - Distances only 2 - Angles and Distances
13 - 16	Ellipsoid Indicator 0 - None calculated 1 - Ellipsoids calculated for anisotropic atoms
17 - 20	Error Indicator 0 - Errors not calculated 1 - Errors calculated. 2 - Errors calculated with structure information read from modified ORFFE tape.
24	Lattice Type Code - This column should be punched with a P, A, B, C, F, I, or R depending on the lattice type.
31 - 40	Minimum bond distance to be printed
41 - 50	Maximum distance used in angle calculation.
51 - 60	Maximum bond distance to be printed.

d. Symmetry Cards

FORMAT (3(A3,2(1X,A2),1X),I4)

Columns	Description
1 - 3	Translational part of \underline{x}'
5 - 6	First positional part of \underline{x}'
8 - 9	Second positional part of \underline{x}'
11 - 13	Translational part of \underline{y}'
15 - 16	First positional part of \underline{y}'
18 - 19	Second positional part of \underline{y}'
21 - 23	Translational part of \underline{z}'
25 - 26	First positional part of \underline{z}'
28 - 29	Second positional part of \underline{z}'

Columns	Description
34	End of Symmetry Deck Indicator Blank - more symmetry cards follow 1 - this is the last card

Note: The translational parts of the symmetry operators are of the form: $bbb \frac{1}{2} \frac{1}{3} \frac{2}{3} \frac{1}{4} \frac{3}{4} \frac{1}{6}$ or $\frac{5}{6}$ where b signifies a blank. The positional parts are of the form: $bw + w - w$ where w may be X, Y or Z. Symmetric positions which are related by a center of inversion or a multiple lattice point must not be included since these positions are internally generated. However, position $\underline{x} \underline{y} \underline{z}$ must be included and must be first.

e. Standard Deviations of Cell Parameters FORMAT (6F10.8)

This card and the cards in section f. below are needed only if errors are to be calculated.

Columns	Description
1 - 10	Standard Deviation of \underline{a}
11 - 20	Standard Deviation of \underline{b}
21 - 30	Standard Deviation of \underline{c}
31 - 40	Standard Deviation of α in degrees
41 - 50	Standard Deviation of β
51 - 60	Standard Deviation of γ

f. Cell Parameter Correlation Matrix FORMAT (6F8.5)

Columns	Correlation Coefficient of
Card 1:	
1 - 8	\underline{a} with \underline{a} (1.0)
Card 2:	
1 - 8	\underline{a} with \underline{b}
9 - 16	\underline{b} with \underline{b} (1.0)
Card 3:	
1 - 8	\underline{a} with \underline{c}
9 - 16	\underline{b} with \underline{c}
17 - 24	\underline{c} with \underline{c} (1.0)
Card 4:	
1 - 8	\underline{a} with α
9 - 16	\underline{b} with α
17 - 24	\underline{c} with α
25 - 32	α with α (1.0)
Card 5:	
1 - 8	\underline{a} with β
9 - 16	\underline{b} with β
17 - 24	\underline{c} with β
25 - 32	α with β
33 - 40	β with β (1.0)

Cell Parameter Correlation Matrix (Cont).

Columns Correlation Coefficient of

Card 6:

1 - 8	\underline{a} with γ	
9 - 16	\underline{b} with γ	
17 - 24	\underline{c} with γ	
25 - 32	α with γ	
33 - 40	β with γ	
41 - 48	γ with γ	(1.0)

g. Atom Cards FORMAT (2A3, 7X, 3F7.5, I2/6F8.5)

There should be a set of 2 atom cards for each atom in the asymmetric unit.

Position Card:

Columns	Description
1 - 6	Identification for atom
14 - 20	\underline{x} in fractional coordinates
21 - 27	\underline{y} in fractional coordinates
28 - 34	\underline{z} in fractional coordinates
36	Temperature factor type
	0 - isotropic
	1 - anisotropic

Temperature factor card:

1 - 8	β_{11} or B
9 - 16	β_{22}
17 - 24	β_{33}
25 - 32	β_{12}
33 - 40	β_{13}
41 - 48	β_{23}

The anisotropic coefficients should be those for which the temperature factor expression is

$$\exp [-(h^2\beta_{11} + k^2\beta_{22} + l^2\beta_{33} + 2hk\beta_{12} + 2hl\beta_{13} + 2kl\beta_{23})].$$

h. Temperature Factor Standard Deviations FORMAT (6F10.8)

These cards are needed only for anisotropic atoms when ellipsoids and errors are to be calculated.

Columns	Description
1 - 10	Standard Deviation of β_{11}
11 - 20	Standard Deviation of β_{22}
21 - 30	Standard Deviation of β_{33}

Temperature Factor Standard Deviations (Cont)

Columns	Description
31 - 40	Standard Deviation of β_{12}
41 - 50	Standard Deviation of β_{13}
51 - 60	Standard Deviation of β_{23}

i. Temperature Factor Correlation Matrix FORMAT (6 F8.5)

These cards are needed only for anisotropic atoms when ellipsoids and errors are to be calculated.

Columns	Correlation Coefficient of
Card 1:	
1 - 8	β_{11} with β_{11} (1.0)
Card 2:	
1 - 8	β_{11} with β_{22}
9 - 16	β_{22} with β_{22} (1.0)
Card 3:	
1 - 8	β_{11} with β_{33}
9 - 16	β_{22} with β_{33}
17 - 24	β_{33} with β_{33} (1.0)
Card 4:	
1 - 8	β_{11} with β_{12}
9 - 16	β_{22} with β_{12}
17 - 24	β_{33} with β_{12}
25 - 32	β_{12} with β_{12} (1.0)
Card 5:	
1 - 8	β_{11} with β_{13}
9 - 16	β_{22} with β_{13}
17 - 24	β_{33} with β_{13}
25 - 32	β_{12} with β_{13}
33 - 40	β_{13} with β_{13} (1.0)
Card 6:	
1 - 8	β_{11} with β_{23}
9 - 16	β_{22} with β_{23}
17 - 24	β_{33} with β_{23}
25 - 32	β_{12} with β_{23}
33 - 40	β_{13} with β_{23}
41 - 48	β_{23} with β_{23} (1.0)

Each anisotropic atom has a Standard Deviations card and a Correlation Matrix.

j. Standard Deviations of Atomic Positions FORMAT (3F10.8)

These cards are needed only if bond distances or angles are to be calculated with errors.

Standard Deviations of Atomic Positions (Cont)

Columns	Description
1 - 10	Standard deviation of \underline{x}
11 - 20	Standard deviation of \underline{y}
21 - 30	Standard deviation of \underline{z}

There should be one card of this type for each atom in the input list.

k. Atomic Positions Correlation Matrix FORMAT (10F8.5)

These cards are needed only if bond distances or angles are to be calculated with errors. The lower triangle of this matrix is read by rows with each row starting on a new card. When a row contains more than ten elements, it should be continued on the next card.

Columns	Correlation Coefficient of
Card 1:	
1 - 8	\underline{x} of atom 1 with \underline{x} of atom 1 (1.0)
Card 2:	
1 - 8	\underline{x} of atom 1 with \underline{y} of atom 1
9 - 16	\underline{y} of atom 1 with \underline{y} of atom 1 (1.0)
Card 3:	
1 - 8	\underline{x} of atom 1 with \underline{z} of atom 1
9 - 16	\underline{y} of atom 1 with \underline{x} of atom 2
17 - 24	\underline{z} of atom 1 with \underline{z} of atom 1 (1.0)
Card 4:	
1 - 8	\underline{x} of atom 1 with \underline{x} of atom 2
9 - 16	\underline{y} of atom 1 with \underline{x} of atom 2
17 - 24	\underline{x} of atom 1 with \underline{x} of atom 2
25 - 32	\underline{x} of atom 2 with \underline{x} of atom 2 (1.0)

This scheme should be continued until all elements of the matrix have been punched.

D. METHOD

1. Bond distances:

If X is a column matrix of fractional atomic coordinates for an atom in the asymmetric unit and Y is the column matrix of the coordinates of a symmetry related atom, then Y and X satisfy the following equation:

$$Y = RX + T \quad (1)$$

where R is a rotation-like operation in that it involves axis interchanges and T is a translation operation which includes

glide and screw components as well as origin shifts. Defining Z as a column matrix whose coefficients are the differences in fractional coordinates between an atom at X and an atom at Y , then

$$Z = X - Y \quad (2)$$

If G is defined as the real space metric tensor which has elements

$$g_{ij} = \underline{a}_i \cdot \underline{a}_j \quad (3)$$

where the \underline{a} 's are the real space axis vectors, then G is the following matrix:

$$G = \begin{pmatrix} a^2 & ab \cos \gamma & ac \cos \beta \\ ab \cos \gamma & b^2 & bc \cos \alpha \\ ac \cos \beta & bc \cos \alpha & c^2 \end{pmatrix} \quad (4)$$

If Z^T denotes the transpose of Z which involves an interchange of the rows and columns of Z , it may be shown that the square of the bond distance, s^2 , between the atoms is determined by the following matrix equation:

$$s^2 = Z^T G Z \quad (5)$$

In the program, all atoms within a spherical shell centered on each atom in the asymmetric unit are located and the distances are calculated. The size of the spherical shell is determined by the minimum and maximum distances to be considered which are input parameters. The search for the contents of the shell is made efficient by enclosing the central atom with a unit cell shaped parallelôpiped tangent to the sphere with all atomic locations outside this parallelopiped excluded. The position of those atoms which lie within the spherical shell are stored in a table. This table also includes the atom number and the number of the R matrix used to generate this position which is needed to properly compute the partial derivatives of the bond distance with respect to the positional coordinates. These two numbers are stored in packed form in the same storage location. Each time a new atom is generated, this table is searched to determine whether this atom has already been included. This search assures that atoms in special positions are properly treated although they may be generated in several different ways.

2. Bond angles:

All possible bond angles about each atom in the asymmetric unit are computed using the table of positions prepared during the bond distance calculation. Each pair of atoms from this table is checked to determine whether their distances from the central atom are within the limits, and if so, the bond angle is computed. If

X denotes the column matrix of the central atom with Y_1 and Y_2 denoting the column matrices of the peripheral atoms, the bond angle θ for the angle $Y_1 - X - Y_2$ can be shown to satisfy the following relationship:

$$\cos \theta = \frac{(Y_1 - X)^T G (Y_2 - X)}{S_{1X} S_{2X}} \quad (6)$$

Where G is the real space metric tensor (see equation (4))

S_{1X} is the bond distance from the atom of X to the atom at Y_1 and

S_{2X} is the bond distance from the atom at X to the atom at Y_2 .

3. Ellipsoids of Vibration:

The conversion of anisotropic thermal coefficients is a problem of finding the characteristic values and characteristic vectors of a particular matrix. Note that characteristic value, proper value, principal value and eigenvalue are equivalent terms. The matrix equation that must be solved is the following:

$$(B - \lambda G^{-1})Q = 0 \quad (7)$$

where B is the matrix of anisotropic temperature coefficients

λ is a characteristic value of the equation

G^{-1} is the reciprocal space metric tensor with elements

$g_{ij}^{-1} = \frac{b_i}{\text{vectors}_i} \cdot \frac{b_j}{\text{and}_j}$ where the b 's are the reciprocal space axis

Q is a column matrix of the coefficients of the characteristic vector. This is a vector in reciprocal space.

If equation (7) is premultiplied by G, it is transformed into the standard form of a characteristic value problem.

$$(GB - \lambda I)Q = 0 \quad (8)$$

where I is the identity matrix and

G is the real space metric tensor defined in equations (3) and (4).

Equation (8) is a set of homogeneous equations of order 3 which have a solution if the determinant of the coefficients is zero. Thus the characteristic values may be found from the equation:

$$\det (GB - \lambda I) = 0 \quad (9)$$

Solution of this equation gives three values of λ which satisfy equation (8). In order to have a meaningful physical situation, it is necessary that the λ 's which are the roots of equation (9) be real and positive. If they are not, the set of temperature coefficients is said to be non-positive definite. This is sometimes referred to as complex amplitudes of vibration or negative temperature factors.

Each of the roots of equation (9) can then be inserted into equation (8) and the resulting equation solved for the characteristic vector by the method of cofactors. After the coefficients of Q are determined, they may be used to form the reciprocal space vector \underline{q} and the angle, θ_i , between this vector \underline{q} and the real space axis vector \underline{a}_i may be found by forming the dot product of the two vectors:

$$\underline{a}_i \cdot \underline{q} = |\underline{a}_i| |\underline{q}| \cos \theta_i \quad (10)$$

This equation may be simplified since

$$\underline{a}_i \cdot \underline{q} = \underline{a}_i \cdot (q_1 \underline{b}_1 + q_2 \underline{b}_2 + q_3 \underline{b}_3) \quad (11)$$

and

$$\underline{a}_i \cdot \underline{b}_j = w_{ij} = \begin{matrix} 1 & \text{for } i = j \\ 0 & \text{for } i \neq j \end{matrix} \quad (12)$$

thus

$$\underline{a}_i \cdot \underline{q} = q_i \quad (13)$$

Equation (12) is the definition of the reciprocal space axis vectors. Equation (10) can now be rewritten

$$\cos \theta_i = \frac{q_i}{|\underline{a}_i| |\underline{q}|} \quad (14)$$

The root-mean-square amplitude of vibration along the i 'th characteristic vector is called μ_i and is found from the i 'th root, λ_i of equation (9) by the following relationship:

$$\mu_i = (\lambda_i / 2\pi^2)^{1/2} \quad (15)$$

4. Error Analysis:

If y is a computed value which is a function of experimentally determined variables x_1, x_2, \dots, x_n such that:

$$y = y(x_1, x_2, \dots, x_n) \quad (16)$$

then the variance of y , denoted by σ_y^2 is found from the equation

$$\sigma_y^2 = \sum_{i=1}^n \sum_{j=1}^n \frac{\partial y}{\partial x_i} \frac{\partial y}{\partial x_j} \text{cov}(x_i, x_j) \quad (17)$$

where $\text{cov}(x_i, x_j)$ is the ij 'th element in the variance-covariance matrix of the x 's.

In crystallographic calculations, the variables for which the variance-covariance matrix elements are known include the unit cell parameters, the atomic positions and the temperature factor coefficients. If the dependence of the bond distance on temperature factors is neglected, as is done in this program, the error in the bond distance will depend only on the cell parameters and the atomic positions. Similarly the ellipsoids will depend only on the unit cell parameters and the temperature factor coefficients. Thus, for crystallographic problems, equation (17) may be rewritten in the form:

$$\begin{aligned} \sigma_y^2 = & \sum_{i=1} \sum_{j=1} \frac{\partial y}{\partial a_i} \frac{\partial y}{\partial a_j} \text{cov}(a_i, a_j) \\ & + \sum_{i=1}^m \sum_{j=1}^m \frac{\partial y}{\partial z_i} \frac{\partial y}{\partial z_j} \text{cov}(z_i, z_j) \end{aligned} \quad (18)$$

where the a 's are the unit cell parameters and the z 's are the atomic parameters. The variance-covariance matrix is the inverse of the normal equations least squares matrix. The error formula in equation (18) is a "full matrix" error formula. The so-called "diagonal" form includes only the terms in equation (18) which have $i=j$. This approximation usually gives a smaller error. All partial derivatives required for computing the errors are analytically evaluated in this program. This procedure is better than numerical differentiation because it is more accurate, easier and faster to do and allows singularities in the derivatives to be detected easier. The necessary derivatives are evaluated using the chain rule of derivatives.

E. OUTPUT

1. General Output:

The first output consists of the information contained on the Title Card. Then the real space axis lengths, the cosines of the real space angles, the reciprocal space axis lengths and the cosines of the real space angles, the reciprocal space axis lengths and the cosines of the reciprocal angles are printed. The real space cell volume is also printed. Then the lattice type and

centric indicator is printed followed by the symmetry operations. Next, if errors are to be calculated, the standard deviations of the cell parameters and the cell parameter correlation matrix are printed. Then the atomic positions and temperature factors are printed. If ellipsoids and errors are to be calculated, the standard deviations of the thermal parameters and temperature factors are printed. If ellipsoids and errors are to be calculated, the standard deviations of the atomic positions and the correlations matrix for the positions are then printed. This completes the general output.

2. Bond Distance and Angle Output:

For each atom in the asymmetric unit, all atoms within the bond distance limits are generated. These atoms are added to a table of generated positions. For each bond distance within the allowable range, the atom identifier, the fractional coordinates, the bond distance, the error, if calculated, and the number of this atom in the table are printed. In the bond angle section of the program, all atoms except those in the asymmetric unit will be referenced by this atom number rather than by coordinates. This number makes it easy to determine quickly what angle has been calculated.

The bond angle section output consists of the atom identifier and coordinates of the central atom which is one of those in the asymmetric unit. The peripheral atoms are each referenced by an atom identifier and an atom table number. The bond angle and its error, if calculated, complete the output for each angle.

3. Ellipsoid of Vibration Output:

For each anisotropic atom, the equivalent isotropic B and its error are calculated and printed. Then for each of the characteristic values, the r.m.s. amplitude of vibration and the angles that the associated characteristic vector makes with the real cell axes as well as the errors in these quantities are printed. No output occurs for isotropic atoms.

4. Page Estimates:

The main program will produce approximately one page of output plus 1/2 page per atom if errors are to be calculated. The bond distance and angle subroutine will require about one page for each 60 distances or angles calculated. However, the user should keep the bond distance limits as small as possible since if n distances are within the limits, the number of angles computed will be approximately $1/2 n^2$. The ellipsoids of vibration subroutine will require one page for each three atoms.

F. PROGRAM ERRORS AND ERROR STOPS

1. There are two kinds of errors which return control to the monitor through a STOP statement. If a symmetry card cannot be interpreted because the information is not of the correct form or because it is punched in the wrong columns, the program executes a STOP 11 statement and returns to the monitor. The card in error will be the last symmetry card listed on the output. If the user attempts to read more than 24 symmetry cards, the program will return to monitor with a STOP 22 instruction. A different kind of error can occur in the bond distance calculation. If the distance limits are such that more than 1000 atom positions are generated, the program prints a diagnostic message and returns to the main program. This error does not terminate the program and ellipsoids of vibration may be calculated correctly after this condition occurs. However, bond angles will not be calculated.

G. COMMON VARIABLES AND DESCRIPTION

XYZ(3,60)	- Fractional coordinates of atoms in asymmetric unit
BETA(6,60)	- Temperature factor coefficients
A(3)	- Real cell axis lengths
ANG(3)	- Cosines of the real cell angles
AS(3)	- Reciprocal axis lengths
CS(3)	- Cosines of the reciprocal cell angles
ATOM(2,60)	- Atom identifiers
SIGA(6,6)	- Variance-covariance matrix for real cell parameters
SIGB(6,6,60)	- Variance-covariance matrix for thermal coefficients
RS(3,3,48)	- Rotational matrix part of symmetry operator
TS(3,48)	- Translational part of symmetry operator
TP(4,3)	- Location of lattice points in fractional coordinates
ITF(60)	- Temperature factor type indicator
CORR(16290)	- Variance-covariance matrix for atomic positions. This is stored in packed form.
XYZP(3,1000)	- Fractional coordinates of atoms generated in the bond distance subprogram.
IATP(1000)	- Atom identifier of atoms generated in bond dis- tance calculation.
NA	- Number of atoms in asymmetric unit
NSS	- Number of symmetry operations
VOL	- Volume of real space unit cell
DLIMIT(3)	- Array of bond distance limits
PI	- The value of the constant π
G(3,3)	- Real space metric tensor
NLP	- Number of lattice points in the unit cell
IERR	- Error calculation indicator
TITLE(18)	- Alphanumeric title information

H. PROGRAM NAMES AND DESCRIPTION

1. U M BADTEA:

This is the main program which handles the input and calls the bond distance and ellipsoid of vibration programs.

2. BODAN(IBOD):

This subprogram calculates bond distances and errors and if the argument IBOD is equal to 2, calculates the bond angles and errors.

3. ELVIB:

This subprogram calculates the ellipsoid of vibration parameters and associated errors.

4. VARIAN(A,B,C,D,E,II):

This subprogram calculates the variance of a computed value where the partial derivatives of the value with respect to the cell parameters are stored in array B, the partial derivatives with respect to the structure parameters are stored in array C, the cell covariance matrix is stored in array D, the structure parameters covariance matrix is in array E, the argument II contains the atom number when the variance of ellipsoid parameters is calculated otherwise it contains 1 and the computed variance is output in argument A.

5. CELLD(B,A,AN,R,CS,VOL):

This subprogram computes the partial derivatives of the reciprocal cell parameters with respect to the real cell parameters. These derivatives are used in computing the ellipsoid errors. Array B contains the partial derivatives after execution. Arrays A, AN, R and CS are the input values of the real cell axis lengths, the real cell cosines, the reciprocal axis lengths and cosines of the reciprocal cell angles respectively. The argument VOL is the input value of the real cell volume.

6. DERDET(A,B,C):

This subprogram calculates the partial derivatives of matrix B with respect to the thermal coefficients and stores them in array A. Array C contains an intermediate set of partial derivatives.

7. CORRI (SIGZ,NN,II,JJ,CORR,KK,LL,MM) :

This subprogram prepares the atomic positional correlation matrix for atoms II and JJ from the packed matrix CORR of rank MM and stores it at the KK,LL position of the array SIGZ which is of rank NN.

I. SYSTEM REQUIREMENTS

U M BADTEA requires two tape units, a standard input tape and a standard output tape. All input is BCD from Logical Unit Number 5 while output is BCD to Logical Unit Number 6. The program requires approximately 32K storage locations. If the modified ORFFE tape is to be used, it is read from logical unit 4.

Appendix C

LISTINGS OF PROGRAMS

Fortran listings of all programs and subprograms are included herein. Example runstreams, with the output they produce, are available on request from either author.


```

SUMAX=FOMIN-RHOMN-RHOMK,(JSCRF(I),I=1,NSF)-NRSE
9,NPAR,(IPAR(I),(PARNAM(J),J=L+2),IPAR(I),(=1,NPAR)+FISGNRNF150
O,IFSON-EGGY-KEKTRF
RFE1760
READIISJ(J)
1(I(ANDM(J),J=L+2),I=1,NSCAT),TEXT,EXTIN,((TAG(J),I),J=L+2),ISOT(I)RNFEL780
2(I(ISCAT(J),J=L+2),FOCCAT(I),OCCUP(I),SITE(I),INZ(J),J=L+2),
4,DEG(A(KDEG(I),I=1,LOGEN)
RFE1810
NOEGN-LDEGN/2
WRITE(IUOUT,33)LABEL
C CHECK FOR NEW PARAMETERS
140 IF(NEW(I))30,180A,150
C READ NEW CELL PARAMETERS AND CALCULATE RECIPROCAL CELL
150 READ(IN,81(I),I=1,6)
WRITE(IUOUT,9)(I(I),I=1,6)
IF(ABS(A(I))-90.01-0.001115A+15A,155
154 A(I)=0.0
155 A(I)=COS(A(I)*PI/180.0)
160 CONTINUE
I=0
00 170 J=L+2
I=I+1
G1,I)=A(I)*J
G1,I)=G(I)*J**2
8(I)=G(I)*I
IJ=L+1
I=I+1
IK=9-I-J
G(I,J)=A(I)*J*A(I)*K
G(I,J)=G(I,I)*J
8(I)=G(I)*A(I)**2
8(I)=G(I)*3
CALL SYMINV(B*3+A*0+A*L*0E-10,VOL,JKRANK)
VOL=SQRT(VOL)
RECELL(1)=SORT(8(I))
RECELL(2)=SORT(8(I))
RECELL(3)=SORT(8(I))
RECELL(4)=8(I)/RECELL(1)*RECELL(3)
RECELL(5)=8(I)/RECELL(1)*RECELL(3)
RECELL(6)=8(I)/RECELL(1)*RECELL(2)
RECELL(7)=4./RECELL(1)**2
EGGY(2)=4./RECELL(2)**2
EGGY(3)=4./RECELL(3)**2
EGGY(4)=4./RECELL(1)*RECELL(2)
EGGY(5)=4./RECELL(1)*RECELL(3)
EGGY(6)=4./RECELL(2)*RECELL(3)
180 IF(IEF=1)0,180,ND-NPAR-NE-OIGALL TRNFRM
IF(NEW(I))190,200,190
C NEW BOND DISTANCE LIMITS
190 OMN=BUFF(I)
OMAX=BUFF(I)
200 IF(NEW(3))12,10,420+2,10
C NEW SYMMETRY OPERATORS
210 ICENT=10BUFF(13)
RFE1740
WRITE(IUOUT,7)
220 CELLP(I,I)=0.0
00 220 I=L+3
JCELL=1
ICELL=1BUFF(4)
IF(CELL(230),320,230)
230 IF(CELL(232),270,300
232 JCELL=1
00 240 I=L+3
240 CELLP(I,I)=0.5
JCELL=2
IF(CELL(4),I)=0.5
280 CELLP(I,I)=0.0
290 CELLP(I,I)=0.0
GU TO 320
300 JCELL=3
DO 310 I=2,3
CELLP(I,I)=FLOAT(I-1)/3.0
CELLP(2,I)=FLOAT(4-I)/3.0
310 CELLP(I,I)=CELLP(2,I)
C READ NEW SYMMETRY CARDS
320 NSYM=0
330 NSYM=NSYM+1
READ(IN,12)(JTNS(I),(IRMAT(K,I),K=1,2),I=1,3),IEF
WRITE(IUOUT,13)(JTNS(I),(IRMAT(K,I),K=1,2),I=1,3),IEF
00 340 J=L+8
IF(JTNS(I)-ITNS(J))340,350,340
340 WRITE(IUOUT,64)NSYM
CALL EXIT
350 TRANS(I,NSYM)=TRS(J)
RMAT(I,I,NSYM)=0
00 390 K=L+2
IJ=IRMAT(K,J)
00 360 L=L+1,10
360 CONTINUE
GO TO 342
370 IF(1-ABS(KRMT(L))390,380,390
380 RMAT(J,I,NSYM)=SIGN(L,IRMAT(L))
390 CONTINUE
400 IF(NSYM-24)330,410,410
410 WRITE(IUOUT,68)
00 420 I=NEW(4)430+460,430
C NSCAT=READ NEW SCATTERING FACTORS
430 NSCAT=10BUFF(6)
WRITE(IUOUT,31)(I,I=1,4)
IF(NSCAT*(NSCAT-21))434+432,432
432 CALL EXIT
RFE2320
RFE2330
RFE2340
RFE2350
RFE2360
RFE2370
RFE2380
RFE2390
RFE2400
RFE2410
RFE2420
RFE2430
RFE2440
RFE2450
RFE2460
RFE2470
RFE2480
RFE2490
RFE2500
RFE2510
RFE2520
RFE2530
RFE2540
RFE2550
RFE2560
RFE2570
RFE2580
RFE2590
RFE2600
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RFE2660
RFE2670
RFE2680
RFE2690
RFE2700
RFE2710
RFE2720
RFE2730
RFE2740
RFE2750
RFE2760
RFE2770
RFE2780
RFE2790
RFE2800
RFE2810
RFE2820
RFE2830
RFE2840
RFE2850
RFE2860
RFE2870
RFE2880
RFE2890

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RFNE4060 RFNE4070 RFNE4080 RFNE4090 RFNE4100 RFNE4110 RFNE4120 RFNE4130 RFNE4140 RFNE4150 RFNE4160 RFNE4170 RFNE4180 RFNE4190 RFNE4200 RFNE4210 RFNE4220 RFNE4230 RFNE4240 RFNE4250 RFNE4260 RFNE4270 RFNE4280 RFNE4290 RFNE4300 RFNE4310 RFNE4320 RFNE4330 RFNE4340 RFNE4350 RFNE4360 RFNE4370 RFNE4380 RFNE4390 RFNE4400 RFNE4410 RFNE4420 RFNE4430 RFNE4440 RFNE4450 RFNE4460 RFNE4470 RFNE4480 RFNE4490 RFNE4500 RFNE4510 RFNE4520 RFNE4530 RFNE4540 RFNE4550 RFNE4560 RFNE4570 RFNE4580 RFNE4590 RFNE4600 RFNE4610 RFNE4620 RFNE4630
MKRANK=0
NKSF=0
C GET EXTINCTION REFINEMENT SWITCHES
OO 565 I=1,6
KEXTRF(I)=U
IF(MOBI(BUFF(I+24),21,EO,0)GO TO 565
PREPARE MKRANK
MKRANK=MKRANK
565 CONTINUE
C GET SCALE FACTOR REFINEMENT SWITCHES
OO 575 I=1,NSF
JSGRF(I)=O
IF(MOBI(BUFF(I+14),21,EO,0)GO TO 575
MKRANK=MKRANK+1
JSGRF(I)=MKRANK
575 CONTINUE
C GET SPECIAL PARAMETER REFINEMENT SWITCHES
OO 577 I=1,NPAR
REAU(I,N,I)IRPAR(I),I=1,NPAR)
IF(IRPAK(I),EO,0)GO TO 577
MKRANK=MKRANK+1
PREPARI(I)=MKRANK
577 CONTINUE
OO 580 I=1,NATOM
NPAR=MPARA+5
IF(I(SOT(I))570,580,570
570 NPAR=MPARA+5
IF(I(SOT(I))-2)590,576,576
576 NPAR=MPARA+10
OO CONTINUE
580 CONTINUE
IF(PAR(I),I=1,NPAR)
WRITE(100T,9023)
IF(NPAR,GT,0)WRITE(100T,23)IRPAR(I),I=1,NPAR)
WRITE(100T,23)IRPAR(I),I=1,NPAR)
IF(IPARA(I))590,600,590
590 MKRANK=MKRANK+1
IF(MOBI(BUFF(I),21,EO,0)GO TO 600
600 CONTINUE
C READ DEPENDENT PARAMETER INFORMATION
IF(INDEG=EO,0)GO TO 610
KPARA=O
OO 602 I=O,NATOM
CALL RESET(I,KPARA)
602 CONTINUE
610 IF(MOBI(BUFF(I),21,EO,0)MOEGNO
IF(MOEGN=EO,0)MOEGNO
IF(MOEGN)612,616,612
C 612 IC=MOEGN
MENSZ=(MKRANK*LMRANK+1)/2+IC
C SET SIZE OF LEAST SQUARES MATRICES
CALL CORSTAINERSZ(I)

```

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RFNE4640 RFNE4650 RFNE4660 RFNE4670 RFNE4680 RFNE4690 RFNE4700 RFNE4710 RFNE4720 RFNE4730 RFNE4740 RFNE4750 RFNE4760 RFNE4770 RFNE4780 RFNE4790 RFNE4800 RFNE4810 RFNE4820 RFNE4830 RFNE4840 RFNE4850 RFNE4860 RFNE4870 RFNE4880 RFNE4890 RFNE4900 RFNE4910 RFNE4920 RFNE4930 RFNE4940 RFNE4950 RFNE4960 RFNE4970 RFNE4980 RFNE4990 RFNE5000 RFNE5010 RFNE5020 RFNE5030 RFNE5040 RFNE5050 RFNE5060 RFNE5070 RFNE5080 RFNE5090 RFNE5100 RFNE5110 RFNE5120 RFNE5130 RFNE5140 RFNE5150 RFNE5160 RFNE5170 RFNE5180 RFNE5190 RFNE5200 RFNE5210
OU 014 (A=1,MRANK
B(I,A)=O,0
OU 014 I=1A,MRANK
IC=IC+1
C 014 A(I,C)=U,0
INITIALIZE FOR CYCLE
C 016 NSC=NSC+1
JBUFF=162Z,NSC9
LBUFF=NSC9+LBUFF+1
NPKINT=O
SUMFC=O,0
RMINUS=O,0
RNUM(I,U)=O,0
KOEN(I,O)=O,0
IF(NSF=1)634,634,634
C *****
C THIS SECTION SHOULD PREPARE TO WRITE A STRUCTURE FACTOR FILE
FOR A FUJHIER PROGRAM
C 632 REMINO 15C6
WRITE(15C4)NSYM,VOL,((RMAT((J,K),I=1,3),J=1,3),K=1,NSYM),((TRANS
15C4)J=1,3),I=1,NSYM)
C 634 IF((BUFF(I,2)-5)1636,635,635
CHANGE REJECTION MUDE
C 635 I(BUFF(12)=1)BUFF(12)-5
DELMAX=BUFF(13)
WR(TELIOUT,9635)IREJ,DELMAX
IREJ=IRUFF(12)
9635 FORMAT('IREJ=',I2,' DELMAX=',F5,1)
C 636 IF(MEIN(I)662,662,662) FACTORS NOT TO BE READ
C 640 IF(I(FIRST)660,650,660) FIRST CYCLE, STRUCTURE FACTORS FROM SAVE TAPE
C 650 ASSIGN 700 TO INTYPE
C 660 ASSIGN 800 TO INTYPE
C 660 ASSIGN 830 TO INTYPE
GO TO 830
C 665 I(E)=I(BUFF(12)
IF(I(BUFF(11))667,666,667)
C 666 INN=IN
GO TO 668
C 667 INN=IISC3
NEW STRUCTURE FACTORS FROM UNIT 4 IISC3)
668 DELMAX=BUFF(13)
FORM=O,0
FORM=I,0E+6
FORM=1,0E+6
RDMN=1,0E+6
RNUM=U,0
RHAUIN,2)FRMT
WRITE(100T,9668)FRMT
9668 FORMAT('OFIRHAT FIR STRUCTURE FACTOR INPUT IS',I,X,1844)

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```

2280 CONTINUE
C      IF(IISOT(I)-2122*0,2281,2281)
2281   DO 2284 I=1,IU
      TEMP=UE(I,I)
      IF(IP24K4(I,K)*J20)
      IF(IJ2287,2283,2282)
2282   TEMP=BI(I,J)/DA08(I,J,1)
      SUM=SUM+ABS(TEMP)
      IFABS(TEMP)=GT,ABSISEMAX) SEMAX=TEMP
      WRITE(IOUT,80)HEAD(I,J),TEMP,B(I,J),CR(J,I),OADB(I,J,1),TEMP,
      1,I,J
      GO TO 2286
2283   GO,M=EGAL(I,1,10)
      IF(LUMAS,GT,0,000001)GO TO 6283
      WRITE(IOUT,82)HEAD(I,J,1),SAVE(I,J,1),CR(J,I)
      GO TO 2284
6283   WRITE(IOUT,82)HEAD(I,J,1),SAVE(I,J,1),CR(J,I),SIGMA
2284   CONTINUE
      IF(IISOT(I)-3122*0,2285,2290)
2285   DO 2288 I=1,IU
      TEMP=UE(I,I)
      IF(IP24K4(I,K)*J20)
      IF(IJ2287,2287,2286)
      TEMP=BI(I,J)/DA08(I,J,1)
      SUM=SUM+ABS(TEMP)
      IFABS(TEMP)=GT,ABSISEMAX) SEMAX=TEMP
      WRITE(IOUT,86)HEAD(I,J,2),TEMP,B(I,J),OK(J,I),OADB(I,J,1),TEMP,
      1,I,J
      GO TO 2288
2287   GO,M=EGAL(I,1,10)
      IF(LUMAS,GT,0,000001)GO TO 6287
      WRITE(IOUT,86)HEAD(I,J,2),TEMP,OK(J,I)
      GO TO 2288
6287   WRITE(IOUT,88)HEAD(I,J,2),TEMP,OK(J,I),SIGMA
2288   CONTINUE
2290   K=IPARA
      SUM=SUM/FLOAT(MRANK)
      WRITE(IOUT,74)SEMAX,SUM
      IFCORRELATION CORRELATION MATRIX
      L=M*SEG*1
      KNT=0
      DO 2300 I=1,20
      2300   HIB(I)=0
      DO 2320 I=1,MRANK
      DO 2310 J=1,MRANK
      B(I)=A(I,J)/(OADB(I,1)+OADB(I,1))
      IF(KNT,LT,20)KNT=KNT+1
      C      COMPARE CURRENT CORRELATIONS WITH LARGEST MAGNITUDES
      IF(KNT,LT,20)KNT=KNT+1
      DO 2301 K=1,KNT
      COMPARE CURRENT VALUE WITH LIST
      IFABS(B(I,J))-GT,AMS(HIB(K))GO TO 2303
2301   CONTINUE
      GO TO 2310
2303   L=KNT-K

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```

      IF(LL,LT,1)GO TO 2305
      C      MOVE LAST ENTRIES UP IN THE LIST
      DO 2304 M=1,L
      NKNT=M
      HIB(NP1)=HIB(N)
      HIB(N)=HIB(NKNT)
      JBI(N+1)=JBI(N)
      JBI(N)=JBI(NKNT)
      C      INSERT ENTRY
      2305   HIB(K)=B(I,J)
      KBI(K)=I
      JBI(K)=J
      2310   IJ=IJ+1
      IFCORR=EQ,0)GO TO 2320
      C      PRINT ENTIRE CORRELATION MATRIX
      WRITE(IOUT,50)1,IJ,B(I,J),J,I,MRANK
      2320   CONTINUE
      C      PRINT THE LARGEST VALUES
      WRITE(IOUT,57)TITLE,KBI(J),JBI(J),HIB(J),J=1,KNT)
      C      CHECK TO SEE IF AUXILIARY FUNCTIONS TO BE DONE
      3000   IF(MDOAN)3010,3020,3010
      3010   CALL BODAN(MDOAN)
      3020   CALL BELVIB(IRELVIB,MDOAN)
      3030   CALL HELVIB(HELVIB,MDOAN)
      3040   REWIND TSC,EG,0,AVO,HELVIB,EG,0,OR,NOEGH,EQ,0)GO TO 3042
      3042   REAOITSC,ILUEGN,IKOEGM(I),I=L,LOEGN)
      IF(ITEM1,IB)IEF,NFLAG,ITEM1,ITEM2
      IF(ITEM1,NE,0,OK,ITEM2,NE,0)ISCL=10*ITEM1+ITEM2
      C      CHECK FOR LEGAL RANGE OF 'NFLAG'
      IF(NFLAG,LT,0,OR,NFLAG,GT,3)GO TO 7086
      C      NO CARDS IF NFLAG=0
      IF(NFLAG=EQ,0)GO TO 7083
      7093   IF(NFLAG,GT,3)CARDS=7093
      IEFNFLAG,CR,EG,0,7093
      DO 7091 I=1,NATOM
      DO 7090 J=1,6
      7090   TER(J)=BETA(J,I)*EGGY(I,J)
      7091   WRITE(IPUN,7092)ITAG(J,I),J=1,2),(XYZ(J,I),J=1,3),ITAG(J,I),J=1,2)
      $,IFB
      7092   FORMAT('ATOM',3X,2A3,3F8.4,'BIJ',4X,2A3,6F8.4,1X,'*')
      7093   IF(NFLAG,LT,1)GO TO 7083
      7093   PUNCH SCALAR CARDS
      C      PUNCH SCALAR CARDS
      WRITE(IPUN,7097)ISCALE(I),I=1,NSF)
      WRITE(IPUN,27)EXTIN
      7097   FORMAT(10F8.4)
      DO 7096 I=1,NATOM
      K=0
      IF(IISOT(I)-GT,IJK=1)
      IF(UB(I)-ISOT(I)**3+6*ISOT(I)**2-2*ISOT(I)))/3
      $*I=ISOT(I)-ISOT(I)*IAG(J,I),J=1,2),STITLE,UCDDP(I),OCCT(I),IISCAT(I),
      $*I=ISOT(I)-ISOT(I)*IAG(J,I),J=1,2),STITLE,UCDDP(I),J=1,6),K
      IF(K,EQ,0)GO TO 7096
      PUNCH 360 CUMULANT
      K=ISOT(I)-2
      WRITE(IPUN,7094)ICRI(J,I),J=1,40)*K
      7094   FORMAT(9F8.6,6F6.4,12)
      IF(K,EQ,0)GO TO 7096

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C 100 COMPILER (FLD=0)
C SUBROUTINE RESPTNA,KPARA)
C SUBROUTINE TO DETERMINE THE PROPER VALUES OF CRYSTALLOGRAPHIC
C PARAMETERS THAT ARE FUNCTIONS OF OTHER PARAMETERS..
DEFINE I(K)*PDM(0,%,K)
DEFINE I2(K)*PDM(0,%,K)
DEFINE I3(K)*PDM(0,%,K)
DEFINE I4(K)*PDM(0,%,K)
INCLUDE ACMA.LIST
INCLUDE DCMA.LIST
INCLUDE XPAR.LIST
INCLUDE LSNAT.LIST
INCLUDE IN23.LIST
LDEGN=2*NDGN
IPNA),100
C IPNA),100 BY SPECIAL PARAMETERS THAT ARE THEMSELVES DEPENDENT
C ON OTHER PARAMETERS.
C LIBRATN, ETC. P2 THESE DEPENDENCIES MUST BE SIMPLE MULTIPLIERS,
C D0 90 I=1,LOBGN,2
IP1(K)(KDEGN(I)),NE,0)G0 T0 90
J=I(KDEGN(I))
IP1(PAR(J),NE,0)G0 T0 90
IP1(PAR(J),NE,0)G0 T0 90
IP1(K)(KDEGN(I))
C IF INDEPENDENT PARAMETER IS 0,0, INITIALIZE TO CONSTANT.
KK=1
IP1(K)(KDEGN(I)),NE,0)G0 T0 20
PAR(J)=AM(I+1)
IP1(K),GT,LDEGN)G0 T0 90
D0 50 K=KK,LDEGN,2
IP1(K)(KDEGN(K)),NE,0)G0,I(K)(KDEGN(K)),NE,J)G0 T0 50
IP1(K)(KDEGN(K)),NE,0)G0,I(K)(KDEGN(K)),NE,J)G0 T0 50
PAR(J)=PAR(J)*PAR(LL)MAM(K*1)
C CONTINUE
G0 95 I=1,NPAR
IF(IPAR(I),LT,0)IPAR(I)=0
CONTINUE
RETURN
C COMPUTE NEW VALUES OF PARAMETERS FOR ATOM NA.
IP1(PAR(I),LT,0)IPAR(I)=0
CONTINUE
C 100
IP1(SGT(NA),GE,1)NPAR=NPAR*5
IP1(SGT(NA),GE,2)NPAR=NPAR*10
IP1(SGT(NA),GE,3)NPAR=NPAR*15
IP1(LDEGN,LF,0)G0 T0 1001
D0 I000 J=1,NPAR
C IS PARAMETER INDEPENDENT?
IF(IPAKKPARA(J),GT,0)G0 T0 1000
C IS THIS PARAMETER DEPENDENT ON ANY OTHERS?
D0 I000 J=1,NPAR
IF(I(K)(KDEGN(K)),NE,NA)R,IA(KDEGN(L)),NE,J)G0 T0 900
DEPENDENT PARAMETER, SET IT.
C 100
IF(IPAKKPARA(J),LT,0)G0 T0 900
RSET 10
RSET 20
RSET 30
RSET 40
RSET 50
RSET 60
RSET 70
RSET 80
RSET 90
RSET 100
RSET 110
RSET 120
RSET 130
RSET 140
RSET 150
RSET 160
RSET 170
RSET 180
RSET 190
RSET 200
RSET 210
RSET 220
RSET 230
RSET 240
RSET 250
RSET 260
RSET 270
RSET 280
RSET 290
RSET 300
RSET 310
RSET 320
RSET 330
RSET 340
RSET 350
RSET 360
RSET 370
RSET 380
RSET 390
RSET 400
RSET 410
RSET 420
RSET 430
RSET 440
RSET 450
RSET 460
RSET 470
RSET 480
RSET 490
RSET 500
RSET 510
RSET 520
RSET 530
RSET 540
RSET 550
RSET 560
RSET 570
RSET 580
RSET 590
RSET 600
RSET 610
RSET 620
RSET 630
RSET 640
RSET 650
RSET 660
RSET 670
RSET 680
RSET 690
RSET 700
RSET 710
RSET 720
RSET 730
RSET 740
RSET 750
RSET 760
RSET 770
RSET 780
RSET 790
RSET 800
RSET 810
RSET 820
RSET 830
RSET 840
RSET 850
RSET 860
RSET 870
RSET 880
RSET 890
RSET 900
RSET 910
RSET 920
RSET 930
RSET 940
RSET 950
RSET 960
RSET 970
RSET 980
RSET 990
RSET1000
RSET1010
RSET1020
RSET1030
RSET1040
RSET1050
RSET1060
RSET1070
RSET1080
RSET1090
RSET1100
RSET1110
RSET1120
RSET1130
RSET1140
RSET1150
IPAR(KPARA,J)--1
TEMPAR=0.
KK=K
IF(I(K)(KDEGN(K)),NF,0)R,12(KDEGN(K)),NF,0)G0 T0 110
TEMPAR=AA(K*1)
KK=KK+2
IF(K,GT,LDEGN)G0 T0 170
D0 I000 J=1,NPAR
IF(I(K)(KDEGN(L)),NE,NA)R,IA(KDEGN(L)),NE,J)G0 T0 150
IS THE INDEPENDENT PARAMETER SPECIAL?
MK=12(KDEGN(L))
IF(I(K)(KDEGN(L)),FO,0)G0 T0 200
N0, LINEAR DEPENDENCIES ONLY, WHAT KIND OF PARAMETER?
MJ=I(KDEGN(I))
IF(MK=2)1112..
IF(MK=5)1115..
IF(MK=10)1118..
IF(MK=21)1120,129,129
TEMPAR=TEMPAR+OCCA(MJ)MAM(L*1)
ITYPE=1
G0 T0 150
TEMPAR=TEMPAR*XYZ(MK-1,MJ)MAM(L*1)
ITYPE=2
G0 T0 150
TEMPAR=TEMPAR*BETA(MK-5,MJ)MAM(L*1)
ITYPE=3
G0 T0 150
TEMPAR=TEMPAR*CH(MK-10,NJ)MAM(L*1)
ITYPE=4
G0 T0 150
TEMPAR=TEMPAR*DR(MK-20,MJ)MAM(L*1)
ITYPE=5
CONTINUE
151 G0 T0(152,154,156,158,160),ITYPE
152 OCCA(MJ)=TEMPAR
G0 T0 1000
154 G0 T0 1000,NJ=TEMPAR
G0 T0 1000
156 BETA(J=9,NA)=TEMPAR
G0 T0 1000
158 CR(J=10,NA)=TEMPAR
G0 T0 1000
160 OR(J=20,NA)=TEMPAR
G0 T0 1000
170
IF(J,GT,2)ITYPE=1
IF(J,GT,3)ITYPE=2
IF(J,GE,5)ITYPE=3
IF(J,GE,11)ITYPE=4
IF(J,GE,21)ITYPE=5
G0 T0 151
C INDEPENDENT PARAMETER SPECIAL, SET ALL DEPENDENT PARAMETERS FOR
THIS ATOM WHICH DEPEND ON THIS SET OF SPECIAL PARAMETERS.
IF(I(K)(PAR(MK)),FO,0)G0 T0 210
IF(I(K)(PAR(MK)),FO,0)G0 T0 2000
IF(I(K)(SPCLNA,PARAMR,J)
G0 T0 1000,NJ=PARAMR,J)
C DEPENDENT PARAMETER IS A LINEAR FUNCTION OF SPECIAL PARAMETERS,
D0 2100 NK=L,LOBGN,2
RSET 590
RSET 590
RSET 600
RSET 610
RSET 620
RSET 630
RSET 640
RSET 650
RSET 660
RSET 670
RSET 680
RSET 690
RSET 700
RSET 710
RSET 720
RSET 730
RSET 740
RSET 750
RSET 760
RSET 770
RSET 780
RSET 790
RSET 800
RSET 810
RSET 820
RSET 830
RSET 840
RSET 850
RSET 860
RSET 870
RSET 880
RSET 890
RSET 900
RSET 910
RSET 920
RSET 930
RSET 940
RSET 950
RSET 960
RSET 970
RSET 980
RSET 990
RSET1000
RSET1010
RSET1020
RSET1030
RSET1040
RSET1050
RSET1060
RSET1070
RSET1080
RSET1090
RSET1100
RSET1110
RSET1120
RSET1130
RSET1140
RSET1150

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COMPILER (FLD=0)
SUBROUTINE DEXTRIN(NEW7)
C GRAPHIC PARAMETERS WITH RESPECT TO THE DERIVATIVES OF DEPENDENT, CRYSTALLO-
C GRAPHIC PARAMETERS WITH RESPECT TO THE SPECIAL PARAMETERS.
DEFINE I1(K)=FLD(0,9,K)
DEFINE I2(K)=FLD(9,9,K)
DEFINE I3(K)=FLD(18,9,K)
DEFINE I4(K)=FLD(27,9,K)
INCLUDE XPAK.LIST
INCLUDE XPMAT.LIST
INCLUDE XPMAL.LIST
INCLUDE XPMAL2.LIST
INCLUDE XPMAL3.LIST
INCLUDE XPMAL4.LIST
INCLUDE XPMAL5.LIST
INCLUDE XPMAL6.LIST
INCLUDE XPMAL7.LIST
INCLUDE XPMAL8.LIST
INCLUDE XPMAL9.LIST
MDEGN=2*NDGN
I=I+2
IF(I1(KDEGN(1)),NE,0)G0 T0 1001
IF(I2(KDEGN(1)),EQ,0,PK,13(KDEGN(1)),EQ,0)G0 T0 1000
IF(I3(KDEGN(1)),EQ,0,PK,13(KDEGN(1)),EQ,0)G0 T0 1000
IF(I4(KDEGN(1)),EQ,0,PK,13(KDEGN(1)),EQ,0)G0 T0 1000
N=I1(KDEGN(1))
N=I2(KDEGN(1))
NPMIN=14(KDEGN(1))
D0 20 J=1,MDEGN,2
IF(J=2),OT,MDEGN)G0 T0 22
IF(I3(KDEGN(J=2)),NE,NA)G0 T0 22
IF(I2(KDEGN(J=2)),NE,11)G0 T0 22
CONTINUE
NPMAT=14(KDEGN(J))
PRINTS=1
PRINTS=J
SPECI=1
SPECI=J
GET SET DESIGNATOR, CLEAR AWAYS, AND COMPUTE TRANSFORMATION,
IF(I1(IPAR(1)),EQ,0)G0 T0 990
IF(I1(IPAR(1)),EQ,1)G0 T0 30
CALL SPDR{I1,NA,NPMIN,NPMAX,1,J}
G0 T0 990
ISPT=12(IPAR(1))
D0 34 K=1,3
XYZ(K)=0,
S(K,L)=0,
D0 34 L=1,3
T(K,L)=0,
EL(K,L)=0,
S(K,L)=0,
P(K,L)=0,
D0 40 K=1,NPAR
IF(I2(IPAR(K)),NE,1)SETJ06 T0 40
IF(I2(IPAR(K)),EQ,1)IPAR(K),PA(K),NA
CONTINUE
CALL EDLER(0PX(3),0XP(2),0XP(1),TRNS)
D0 WE NEED TO PILL IN KYZ
IF(NPMIN,LE,4)G0 T0 50
CALL TRNSP(TRANS,TRANSI)
CALL MULM(TRANSI,ATOK,ITRNS1)
D0 42 K=1,3
ITEM(K)=XYZ(K,NA)-0XYZ(K)
DRVS 10
DRVS 11
DRVS 12
DRVS 13
DRVS 14
DRVS 15
DRVS 16
DRVS 17
DRVS 18
DRVS 19
DRVS 20
DRVS 21
DRVS 22
DRVS 23
DRVS 24
DRVS 25
DRVS 26
DRVS 27
DRVS 28
DRVS 29
DRVS 30
DRVS 31
DRVS 32
DRVS 33
DRVS 34
DRVS 35
DRVS 36
DRVS 37
DRVS 38
DRVS 39
DRVS 40
DRVS 41
DRVS 42
DRVS 43
DRVS 44
DRVS 45
DRVS 46
DRVS 47
DRVS 48
DRVS 49
DRVS 50
DRVS 51
DRVS 52
DRVS 53
DRVS 54
DRVS 55
DRVS 56
DRVS 57
DRVS 58
DRVS 59
DRVS 60
DRVS 61
DRVS 62
DRVS 63
DRVS 64
DRVS 65
DRVS 66
DRVS 67
DRVS 68
DRVS 69
DRVS 70
DRVS 71
DRVS 72
DRVS 73
DRVS 74
DRVS 75
DRVS 76
DRVS 77
DRVS 78
DRVS 79
DRVS 80
DRVS 81
DRVS 82
DRVS 83
DRVS 84
DRVS 85
DRVS 86
DRVS 87
DRVS 88
DRVS 89
DRVS 90
DRVS 91
DRVS 92
DRVS 93
DRVS 94
DRVS 95
DRVS 96
DRVS 97
DRVS 98
DRVS 99
DRVS 100
DRVS 101
DRVS 102
DRVS 103
DRVS 104
DRVS 105
DRVS 106
DRVS 107
DRVS 108
DRVS 109
DRVS 110
DRVS 111
DRVS 112
DRVS 113
DRVS 114
DRVS 115

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C CALL MULM(VTRNSI,ITEM,SKYZ)
C WHAT KIND IS INDEPENDENT PARAMETER?
C 50 ITEM=14(IPAR(1))
IF(I2(IPAR(1)),EQ,0)G0 T0 990
IF(I2(IPAR(1)),EQ,1)CALL MULM(XTMA,TRNS,ITRNS)
G0 T0 (100,200,300,400,500,600,700,800,900,1000)
C SPECIAL ORIGIN
D0 100 D0 110 K=1,J=2
AA(K)=1*J
G0 T0 990
C ORIENTATION OF SPECIAL SYSTEM WRT CRYSTAL ORIGINORPMAL.
D0 200 K=1,INDEN=1210,230,250
C OMEGA ANGLE
D0 210 CALL OTD(OMG(0XP(3),0XP(2),0XP(1),TRNS))
D0 212 CALL MULM(XTMA,TRNS,ITRNS)
IF(NPMIN,GE,5)G0 T0 215
C DERIVATIVES OF POSITION PARAMETERS WRT OMEGA,CHI, OR PHI.
C CALL MULM(VTRNS,SKYZ,ITEM)
D0 214 IF(KK,GE,5)G0 T0 216
KK=2
KK=2)*ITEM(KK=1)
IF(K=J)214,214,990
D0 215 IF(NPMIN,GE,11)D0 T0 221
IF(NPMAX,LE,4)G0 T0 990
D0 216 DERIVATIVES OF BETAS WRT OMEGA, CHI, OR PHI.
C CORRECT SKYZ FOR LIBRATION.
CALL CORLIM(ITEM,EL,SKYZ)
D0 218 L=1,6
JK=IND2(1,L)
ITEM(L)=SKLS(ITEM,JK,JK,L,S)
D0 218 CALL TRAZ(ITRNS,ITEM,ITEM)
D0 220 KK=14(KDEGN(K))
IF(KK,GE,11)G0 T0 222
AA(K)=1)*ITEM(KK=4)
KK=2
IF(K=J)220,220,990
D0 221 CALL CORLIM(ITEM,EL,SKYZ)
D0 222 DERIVATIVES OF GAMMAS WRT OMEGA, CHI, OR PHI.
C DERIVATIVES OF GAMMAS WRT OMEGA, CHI, OR PHI.
D0 224 L=1,10
JK=IND3(1,L)
GTEM(L)=ITRNS(ITEM,JK,JK,L,S)
D0 224 CALL TRAZ(ITRNS,ITEM,ITEM)
D0 226 KK=14(KDEGN(K))
AA(K)=1)*ITEM(KK=10)
KK=2
IF(K=J)226,226,990
C CHI ANGLE
D0 230 CALL OTD(CHI(0XP(3),0XP(2),0XP(1),TRNS))
G0 T0 212
C PHI ANGLE
D0 250 CALL OTD(PHI(0XP(3),0XP(2),0XP(1),TRNS))

```

C POSITION IN SPECIAL SYSTEM
 300 K*1
 IF(NP4IN,GE,5)GO TO 350
 DP 30 L*1,3
 310 BTEM(L)*0,
 BTEM(L)*1,
 BTEM(L)*2,
 BTEM(L)*3,
 BTEM(L)*4,
 BTEM(L)*5,
 BTEM(L)*6,
 BTEM(L)*7,
 BTEM(L)*8,
 BTEM(L)*9,
 BTEM(L)*10,
 BTEM(L)*11,
 BTEM(L)*12,
 BTEM(L)*13,
 BTEM(L)*14,
 BTEM(L)*15,
 BTEM(L)*16,
 BTEM(L)*17,
 BTEM(L)*18,
 BTEM(L)*19,
 BTEM(L)*20
 320 IF(KK,GT,4)GO TO 360
 AA(K*1)*BTEM(KK-1)
 K*2
 IF(K-J)320,320,990
 C WE SHALL NOW OBTAIN THE DERIVATIVES OF BETAS AND GAMMAS WRT
 C SKYZ, ZLTHOUGH THESE MAY ACTUALLY BE IMPORTANT, WE WILL FILL THEM
 C UP WITH ZERO.
 350 KK=14(KDEGN(K))
 360 AA(K*1)*0,
 K*2
 IF(K-J)350,350,990
 KK=14(KDEGN(K))
 370 IF(KK,GT,20)GO TO 990
 AA(K*1)*0,
 K*2
 IF(K-J)365,365,990
 C ELEMENTS OF T TENSOR, ONLY BETAS INVOLVED.
 400 K*1
 IDEN=IDEN-9
 JK=IND2(1,1DEN)
 JL=IND2(2,1DEN)
 DM 410 L*1,5
 JN=IND2(1,1)
 JN=IND2(2,1)
 410 BTEM(L)*D2KDT(JM,JN,JK,JL)
 CALL FM2(TTRNS,ITEM,BTEM)
 420 KK=14(KDEGN(K))
 IF(KK,GT,10)GO TO 990
 IF(KK,GT,5)GO TO 425
 AA(K*1)*BTEM(KK-4)
 K*2
 425 K*2
 420,420,990
 C ELEMENTS OF L TENSOR, BETAS AND GAMMAS INVOLVED.
 500 K*1
 IDEN=IDEN-15
 JK=IND2(1,1DEN)
 JL=IND2(2,1DEN)
 CALL CORLIR(ITEM,EL,SKYZ)
 IF(NP4IN,GT,10)GO TO 560
 DM 510 L*1,5
 JN=IND2(1,1)
 JN=IND2(2,1)
 510 BTEM(L)*D2KDL(ITEM,EL,S,JM,JN,JK,JL)
 CALL FM2(TTRNS,ITEM,BTEM)
 520 KK=14(KDEGN(K))
 IF(KK,GT,10)GO TO 560
 IF(KK,GT,5)GO TO 525
 AA(K*1)*BTEM(KK-4)

DRVS1160
 DRVS1170
 DRVS1180
 DRVS1190
 DRVS1200
 DRVS1210
 DRVS1220
 DRVS1230
 DRVS1240
 DRVS1250
 DRVS1260
 DRVS1270
 DRVS1280
 DRVS1290
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 DRVS1370
 DRVS1380
 DRVS1390
 DRVS1400
 DRVS1410
 DRVS1420
 DRVS1430
 DRVS1440
 DRVS1450
 DRVS1460
 DRVS1470
 DRVS1480
 DRVS1490
 DRVS1500
 DRVS1510
 DRVS1520
 DRVS1530
 DRVS1540
 DRVS1550
 DRVS1560
 DRVS1570
 DRVS1580
 DRVS1590
 DRVS1600
 DRVS1610
 DRVS1620
 DRVS1630
 DRVS1640
 DRVS1650
 DRVS1660
 DRVS1670
 DRVS1680
 DRVS1690
 DRVS1700
 DRVS1710
 DRVS1720
 DRVS1730

575 K*2
 580 570 L*1,10
 JM=IND3(1,1)
 JN=IND3(2,1)
 570 GTFM(L)*D3KDL(ITEM,EL,S,JM,JN,JK,JL)
 CALL FM3(TTRNS,ITEM,BTEM)
 530 IF(AA,GT,20)GO TO 990
 AA(K*1)*GTEM(KK-10)
 K*2
 IF(K-J)530,530,990
 ELEMEN OF S TENSOR,
 K*1
 DEN=IDEN-31
 CALL CORLIR(ITEM,EL,SKYZ)
 IF(IDEN,GT,6)GO TO 605
 JK=IND2(1,1DEN)
 JL=IND2(2,1DEN)
 GM 610 L*1,6
 JN=IND2(1,1)
 JN=IND2(2,1)
 610 ITEL(L)*D2KDS(ITEM,EL,S,JM,JN,JK,JL)
 CALL FM2(TTRNS,ITEM,BTEM)
 620 KK=14(KDEGN(K))
 IF(KK,GT,10)GO TO 650
 IF(KK,GT,5)GO TO 625
 AA(K*1)*BTEM(KK-4)
 K*2
 625 K*2
 620,620,990
 DM 660 L*1,10
 JM=IND3(1,1)
 JN=IND3(2,1)
 660 GTFM(L)*D3KDS(ITEM,EL,S,JM,JN,JK,JL)
 CALL FM3(TTRNS,ITEM,BTEM)
 670 IF(KK,GT,20)GO TO 990
 IF(KK,GT,10)GO TO 990
 K*2
 IF(K-J)670,670,990
 T-J
 990 IF(1'-2-MDEGN)10,
 1000 CONTINUE
 C IF THERE ARE ANY SPECIAL PARAMETERS THAT DEPEND ON OTHER SPECIAL
 C PARAMETERS, THE DERIVATIVES MUST FIRST BE CORRECTED SO THAT ALL
 C DERIVATIVES REFLECT ALL DEPENDENCIES, FIRST SAVE THE UNALTERED
 C VALUES OF THE SPECIAL PARAMETERS.
 C REWIND DISC
 WRITE(LSCS)MDEGN,(KDEGN(1),1'-1,MDEGN)
 IF(INPAR,NE,0)PARNEW7,NE,0CALL PDEGN(NEW7)
 IF(INPAR,EO,0)GO TO 2001
 DM 2000 1'-1,MDEGN,2
 IF(1'(KDEGN(1)),NE,0)GO TO 2002

DRVS1740
 DRVS1750
 DRVS1760
 DRVS1770
 DRVS1780
 DRVS1790
 DRVS1800
 DRVS1810
 DRVS1820
 DRVS1830
 DRVS1840
 DRVS1850
 DRVS1860
 DRVS1870
 DRVS1880
 DRVS1890
 DRVS1900
 DRVS1910
 DRVS1920
 DRVS1930
 DRVS1940
 DRVS1950
 DRVS1960
 DRVS1970
 DRVS1980
 DRVS1990


```

56 OR0(N)=0.0
60 TU 80
60 IF((SOT(L))80,70=80
C CALCULATE ISOTHERMIC TEMPERATURE FACTOR
70 TF=EXP(-BETAI,1)*RHJ(1)*H*SYMMETRY OPERATIONS
C START LOOP THROUGH SYMMETRY OPERATIONS
80 ARG=TPR(IA)
00 90 I0=1,3
HPR(I0)=HPR(IA)
90 ARG=ARG+HPR(I0)*XYZ(I0+L)
CUM3=0.0
IF(I0SOT(L))100,130,100
C GENERATE TRANSFORMED INDEX PRODUCTS FOR ANISO. ATOMS
130 HPR(I0)=HPR(I0)*BETA(I0+L)
110 HHJ(I0)=HPR(I0)**2
HHJ(6)=2.0*HPR(1)*HPR(2)
HHJ(5)=2.0*HPR(1)*HPR(3)
HHJ(6)=2.0*HPR(2)*HPR(3)
C CALCULATE ANISOTROPIC TEMPERATURE FACTOR
TEMP=0.0
00 120 I0=1,6
TEMP=TEMP+HHJ(I0)*BETA(I0+L)
IF(I0SOT(L))120,129,129,122
C CALCULATE THERO CUMULANT INJEX PRODUCTS
122 00 123 I0=1,3
123 HHHJ(I0)=HPR(I0)*HHJ(I0)
HHJ(6)=3.0*HHJ(1)*HPR(2)
HHJ(5)=3.0*HHJ(2)*HPR(1)
HHJ(6)=3.0*HHJ(1)*HPR(3)
HHJ(7)=3.0*HHJ(3)*HPR(1)
HHJ(8)=3.0*HHJ(2)*HPR(3)
HHJ(11)=3.0*HHJ(4)*HPR(3)
00 124 I0=1,10
124 CDM3=CDM3+HHJ(I0)*GR(I0+L)
IF(I0SOT(L))21129,129,125
C CALCULATE FODRTH CUMULANT INDEX PRODUCTS
125 00 126 I0=1,3
126 HHHH(I0)=HHJ(I0)**2
HHH(4)=4.0*HHH(1)*HPR(2)
HHH(5)=6.0*HHH(1)*HPR(3)
HHH(7)=12.0*HHH(1)*HPR(2)*HPR(3)
HHH(8)=6.0*HHH(1)*HHJ(3)
HHH(9)=4.0*HHH(1)*HHJ(3)
HHH(10)=12.0*HHH(2)*HPR(1)*HPR(3)
HHH(11)=12.0*HHH(3)*HPR(1)*HPR(2)
HHH(12)=4.0*HHH(3)*HPR(1)
HHH(13)=4.0*HHH(2)*HPR(3)
HHH(15)=6.0*HHH(2)*HHJ(3)
HHH(16)=6.0*HHH(3)*HPR(2)
00 127 I0=1,15
127 CUM4=CUM4+HHH(I0)*GR(I0+L)
C CALCULATE TEMPERATURE FACTOR
129 EXP1J=EXP(TEMP/CUM4)
130 T=T*HOP1*ARG=CDM3

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SFAC1160
SFAC1170
SFAC1180
SFAC1190
SFAC1200
SFAC1210
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SFAC1400
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SFAC1470
SFAC1480
SFAC1490
SFAC1500
SFAC1510
SFAC1520
SFAC1530
SFAC1540
SFAC1550
SFAC1560
SFAC1570
SFAC1580
SFAC1590
SFAC1600
SFAC1610
SFAC1620
SFAC1630
SFAC1640
SFAC1650
SFAC1660
SFAC1670
SFAC1680
SFAC1690
SFAC1700
SFAC1710
SFAC1720
SFAC1730

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COSIJ=COS (I)*EXP(IJ
SINIJ=SIN (I)*EXP(IJ
AAIN=AAIN0+COSIJ
IFFICIENT140,150,140
140 BBIN=BBIN0+SINIJ
150 IFMSEL=1,TEMP3=190
C CALCULATE POSITIVE THERMAL DERIVATIVES
190 OAX(IAA)=OAX(IAA)-HPR (IAA)*SINIJ
IFFICIENT210,230,210
00 220 IAB=1,3
220 OBX(IAB)=OBX(IAB)+HPR(IAB)*COSIJ
230 IFFISOT(L)240,280,240
C CALCULATE THERMAL DERIVATIVES FOR ANISOTROPIC ATOMS
240 OAH(IAC)=OAH(IAC)-HHJ(IAC)*COSIJ
250 OAB(IAC)=OAB(IAC)-HHJ(IAC)*COSIJ
IFFICIENT260,270,260
260 00 265 I0=1,6
265 OBH(I0)=OBH(I0)-HHJ(I0)*SINIJ
270 IFFISOT(L)-1)280,280,271
C CALCULATE THERO CUM. DERIVS.
271 00 272 I0=1,10
272 OAC(I0)=OAC(I0)+HHHJ(I0)*SINIJ
273 IFFICIENT273,275,275
274 OBC(I0)=OBC(I0)-HHHJ(I0)*COSIJ
275 IFFISOT(L)-2)280,280,276
C CALCULATE FODRTH CUMULANT DERIVS.
276 00 277 I0=1,15
277 OAO(I0)=OAO(I0)+HHHH(I0)*COSIJ
IFFICIENT278,280,278
279 00 279 I0=1,15
280 CONFINCATE(L)
IY2=ISCATE(L)
TEMPA=IF*S(TE(L)
IF(IY2)370,380,370
C EVALUATE SCATTERING FACTOR FOR MULTIPLE OCCUPANCY
370 OCC=UCCUPL(L)-OCCAL)
REAL=SCAT(IY1)
REAL=SCAT(IY2)
TEMP=UCCAL*RFALL+OCCB*REAL2
TEMP2=REAL*TEMP2+IY1)*OCCB*ANUM2, (IY2)
TEMP3=REAL+R*EAL2
GO TO 390
C EVALUATE SCATTERING FACTOR FOR SINGLE OCCUPANCY
380 REAL=SCAT(IY1)
TEMP=UCCUPL(L)*REAL
TEMP3=ANUM2, (IY1)
TEMP1=OCCUPL(L)*TEMP3
TEMP2=TEMP2+TEMP1
88ING=EF15C*BBIN0
IF(MSEL)392,396,392
C EVALUATE DERIVATIVES WITH RESPECT TO OCCUPANCY
0A00(L)=TEMP*(TEMP2*AAIN0-TEMP3*BBIN0)
UB00(L)=TEMP*(TEMP2*BBIN0+TEMP3*AAIN0)

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IFIFISGN-EO-DJGO TU 396
C EVALUATE STRUCTURE FACTOR FOR HANATLORPHIC ORIENTATION
AMINUS=TEMP*(1-TEMP)*BB1*OAI*AMINUS
BMINUS=TEMP*(1-TEMP)*BB1*OAI*AMINUS
C EVALUATE INDIVIDUAL ATOM CONTRIBUTIONS
396 AINOL(L)=TEMP*(TEMP*AA1IND-TEMP*BB1IND)
BINOL(L)=TEMP*(TEMP*AA1IND-TEMP*BB1IND)
ACALC=ACALC+AINOL(L)
BCALC=BCALC+BINOL(L)
IF MFSEL=1400+450+400
MODIFY DERIVATIVES
C 400 TEMPS=1400+TEMP*4
00 410 IAG=1+3
OAOI(IAG,L)=TEMP*(TEMP*OAOI(IAG)-TEMP*OBB(IAG))
OAOI(IAG,L)=TEMP*(TEMP*OAOI(IAG)-TEMP*OBB(IAG))
IF (ISOT(L)) 430,420,430
C 420 OAOBI(L,L)=--RHO*BINOL(L)
OAOBI(L,L)=--RHO*BINOL(L)
C 430 DERIVATIVES WITH RESPECT TO ANISOTROPIC TEMPERATURE FACTOR
00 440 IAH=1+6
OAOI(IAH,L)=TEMP*(TEMP*OAOI(IAH)-TEMP*OBB(IAH))
OAOI(IAH,L)=TEMP*(TEMP*OAOI(IAH)-TEMP*OBB(IAH))
IF (ISOT(L)) 450,450,441
C 441 00 442 IO=1,10
OAOI(IO,L)=TEMP*(TEMP*OAOI(IO)-TEMP*OBB(IO))
OAOI(IO,L)=TEMP*(TEMP*OAOI(IO)-TEMP*OBB(IO))
IF (ISOT(L)) 450,450,443
C 443 00 444 IO=1,15
OAOI(IO,L)=TEMP*(TEMP*OAOI(IO)-TEMP*OBB(IO))
OAOI(IO,L)=TEMP*(TEMP*OAOI(IO)-TEMP*OBB(IO))
450 CONTINUE
470 MFSEL=ISAVE
RETURN
ENTRY EXCALC
C CALCULATE EXTINCTION FACTOR
IF (TEXT) 1010,1000,1010
C ISOTROPIC FORM
1000 EXX=EXBETA*EXTIN(1)*FCALC
OROE(1)=1.0
RETURN
C ANISOTROPIC EXTINCTION - CALCULATE TRIG FUNCTIONS OF ANGLES
1010 SCA=SNUEXANG(1)
GCHE=CGUS*EXANG(1)
SPHI=SIN(EXANG(2))
CPHI=CGUS*EXANG(2)
IF (TEXT)-1) 1030,1020,1030
C TYPE 1 CORRECTION
1020 V(1)=SPHI*SCHE
V(2)=--CPHI*SCHE
V(3)=--GCHE
GO TO 1040
C TYPE 2 ANISOTROPIC
1030 SNU=SIN(EXANG(3))

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SFAC1740
SFAC1760
SFAC1770
SFAC1780
SFAC1790
SFAC1800
SFAC1810
SFAC1820
SFAC1830
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SFAC1850
SFAC1860
SFAC1870
SFAC1880
SFAC1890
SFAC1900
SFAC1910
SFAC1920
SFAC1930
SFAC1940
SFAC1950
SFAC1960
SFAC1970
SFAC1980
SFAC1990
SFAC2000
SFAC2010
SFAC2020
SFAC2030
SFAC2040
SFAC2050
SFAC2060
SFAC2070
SFAC2080
SFAC2090
SFAC2100
SFAC2110
SFAC2120
SFAC2130
SFAC2140
SFAC2150
SFAC2160
SFAC2170
SFAC2180
SFAC2190
SFAC2200
SFAC2210
SFAC2220
SFAC2230
SFAC2240
SFAC2250
SFAC2260
SFAC2270
SFAC2280
SFAC2290
SFAC2300
SFAC2310

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CNU=COS(EXANG(3))
V(1)=CGUS*SPHI*CNUS-SNU*CPHI
V(2)=--CPHI*CNUS-SNU*SPHI
V(3)=--SGH*CNUS
FOR PRODUCTS OF COEFFICIENTS
1040 UD 1050 I=1+3
1050 V(1)=V(1)*I**2
V(4)=2.0*V(1)*V(2)
V(5)=2.0*V(1)*V(3)
V(6)=2.0*V(2)*V(3)
SUM=0.0
I=1+6
1060 SUM=SUM+V(1)*EXTIN(I)
IF (SUM-LE-0.0) SUM=1.0
TEMP=-1.0/SORT(SUM)
EXX=EXBETA*FCALC*ABS(TEMP)
C CALCULATE DERIVATIVES OF THE FORM DF=STAR/OF-LJ
00 1070 I=1+6
1070 UROET(I)=0.5*VV(1)*TEMP/SUM
RETURN
END
SFAC2320

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```

IJ*IPARA(IK)
  IF(IJ)232,233,232
  232 DERIV(IJ)*ACALC=OAOCL(L,J)*HCALC=OHOCL(L,J)
  2322 IF(I1,LOEGR(I1))-I1J,2326,233
  2324 II=I1*2
  2326 CALL MDPHY(ORIV(IJ),I3(LOEGR(I1)),I4(LDEGR(I1)),A(I1*1))
  233 CONTINUE
  234 O6 DERIVATIVES WRT TO THE F6UKTH CUMULANT
  IF(I8RT(IJ)-2)240,240,234
  L=I1*1
  IJ*IPARA(IK)
  IF(IJ)235,236,235
  235 OBR IV(IJ)*ACALC=DADD(L,J)*HCALC=OHDRL(L,J)
  2352 IF(I1-MOEGN),,236
  2354 II=I1*2
  2356 CALL MDPHY(ORIV(IJ),I3(LOEGR(I1)),I4(LDEGR(I1)),A(I1*1))
  236 CONTINUE
  236 O6 TO 2354
  240 CONTINUE
C
  FORM MATRICES
  INDEX=MDEGN*1
  TEMP=DERIV(IJ)*WT
  O6 260 M=1,MRANK
  250 INDEX=INDEX*MRANK-M*1
  O6 TO 260
  260 A(INDEX)=A(INDEX)*TEMP=ORIV(N)
  270 INDEX=INDEX*1
  280 CONTINUE
  RETURN
  END

```

```

MATX1150
MATX1170
MATX1190
MATX1200
MATX1210
MATX1220
MATX1230
MATX1240
MATX1250
MATX1260
MATX1270
MATX1280
MATX1290
MATX1300
MATX1310
MATX1320
MATX1330
MATX1350
MATX1370
MATX1380
MATX1390
MATX1400
MATX1410
MATX1420
MATX1430
MATX1440
MATX1450
MATX1470
MATX1490
MATX1490
MATX1500
MATX1510
MATX1520
MATX1530
MATX1540

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```

SUBROUTINE MDPHY(ORIV,NA,NP,TEMP)
  INCLUDE OCM,LIST
  IF(NP,GE,2)GOTO 100
  OERIV=ORIV*TEMP*(ACALC=OAOH(NA)*HCALC=OHOH(NA))
  RETURN
  100 IF(NP,GE,5)GOTO 200
  OERIV=ORIV*TEMP*(ACALC=OAOX(NP-1,NA)*HCALC=OHOX(NP-1,NA))
  RETURN
  200 IF(NP,GE,11)GOTO 300
  OERIV=ORIV*TEMP*(ACALC=DAUHK(NP-4,NA)*HCALC=OHDHK(NP-4,NA))
  RETURN
  300 IF(NP,GE,21)GOTO 400
  OERIV=ORIV*TEMP*(ACALC=OADC(NP-10,NA)*HCALC=OADC(NP-10,NA))
  RETURN
  400 OERIV=ORIV*TEMP*(ACALC=OADD(NP-20,NA)*HCALC=OHOCD(NP-20,NA))
  RETURN
  END

```

```

C
DUMMY SUBROUTINES SPVAL AND SPOERI
SUBROUTINE SPVAL
  RETURN
ENTRY SPOERI
  RETURN
  END

```

```

MDPY 10
MDPY 20
MDPY 30
MDPY 40
MDPY 50
MDPY 60
MDPY 70
MDPY 80
MDPY 90
MDPY 100
MDPY 110
MDPY 120
MDPY 130
MDPY 140
MDPY 150
MDPY 160
MDPY 170

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```

SPVL 10
SPVL 20
SPVL 30
SPVL 40
SPVL 50
SPVL 60

```



```

C
SUBROUTINE EULER(PBI,CBI,OMEGA,TRANS)
SUBROUTINE TO GENERATE THE MATRIX B-INVERSE FROM THE EULERIAN
ANGLES PHI,CHI,AND OMEGA.
DATA RAO/57.2557792/
DIMENSION TRANS(3,3)
ASSIGN 10 TO KGG
GO TO 100
TRANS(1,1)=CP*CX*CG-SP*SG
TRANS(1,2)=-CP*CX*SG+SP*CG
TRANS(1,3)=CP*SX
TRANS(2,1)=SP*CX*CG+CP*SG
TRANS(2,2)=SP*CX*SG+CP*CG
TRANS(3,1)=-SX*CG
TRANS(3,2)=-SX*SG
TRANS(3,3)=CX
ENTRY OTDPHI(PBI,CBI,OMEGA,TRANS)
ASSIGN 20 TO KGG
GO TO 100
TRANS(1,1)=-SP*CX*CG-CP*SG
TRANS(1,2)=SP*CX*SG-CP*CG
TRANS(1,3)=SP*SX
TRANS(2,1)=CP*CX*CG-SP*SG
TRANS(2,2)=-CP*CX*SG+SP*CG
TRANS(2,3)=CP*SX
D6 23 I=1,3
D6 23 J=1,2
23 TRANS(J,1)=TRANS(J,I)/RAD
TRANS(3,1)=0.
25 RETURN
ENTRY DTPCHI(PBI,CBI,OMEGA,TRANS)
ASSIGN 30 TO KGG
GO TO 100
TRANS(1,1)=-CP*SY*CG
TRANS(1,2)=CP*SX*SG
TRANS(1,3)=CP*CX*SG
TRANS(2,1)=-SP*SX*CG
TRANS(2,2)=SP*SX*SG
TRANS(2,3)=SP*CX
TRANS(3,1)=-CX*CG
TRANS(3,2)=CX*SG
TRANS(3,3)=SX
D6 33 I=1,3
D6 33 J=1,3
3S TRANS(I,J)=TRANS(I,J)/RAD
RETURN
ENTRY OTDOMG(PBI,CBI,OMEGA,TRANS)
ASSIGN 40 TO KGG
GO TO 100
TRANS(1,1)=-CP*CX*SG-SP*CG
TRANS(1,2)=CP*CX*SG+SP*CG
TRANS(1,3)=CP*SX*SG+SP*CG
TRANS(2,1)=SP*CX*CG-CP*SG
TRANS(2,2)=SP*CX*SG+CP*SG
TRANS(3,1)=-SX*CG
TRANS(3,2)=-SX*SG
D6 AS I=1,3
GO TO 100
END

```

```

EKCL 10
C
SUBROUTINE EULER(PBI,CBI,OMEGA,TRANS)
SUBROUTINE TO GENERATE THE MATRIX B-INVERSE FROM THE EULERIAN
ANGLES PHI,CHI,AND OMEGA.
DATA RAO/57.2557792/
DIMENSION TRANS(3,3)
ASSIGN 10 TO KGG
GO TO 100
TRANS(1,1)=CP*CX*CG-SP*SG
TRANS(1,2)=-CP*CX*SG+SP*CG
TRANS(1,3)=CP*SX
TRANS(2,1)=SP*CX*CG+CP*SG
TRANS(2,2)=SP*CX*SG+CP*CG
TRANS(3,1)=-SX*CG
TRANS(3,2)=-SX*SG
TRANS(3,3)=CX
ENTRY OTDPHI(PBI,CBI,OMEGA,TRANS)
ASSIGN 20 TO KGG
GO TO 100
TRANS(1,1)=-SP*CX*CG-CP*SG
TRANS(1,2)=SP*CX*SG-CP*CG
TRANS(1,3)=SP*SX
TRANS(2,1)=CP*CX*CG-SP*SG
TRANS(2,2)=-CP*CX*SG+SP*CG
TRANS(2,3)=CP*SX
D6 23 I=1,3
D6 23 J=1,2
23 TRANS(J,1)=TRANS(J,I)/RAD
TRANS(3,1)=0.
25 RETURN
ENTRY DTPCHI(PBI,CBI,OMEGA,TRANS)
ASSIGN 30 TO KGG
GO TO 100
TRANS(1,1)=-CP*SY*CG
TRANS(1,2)=CP*SX*SG
TRANS(1,3)=CP*CX*SG
TRANS(2,1)=-SP*SX*CG
TRANS(2,2)=SP*SX*SG
TRANS(2,3)=SP*CX
TRANS(3,1)=-CX*CG
TRANS(3,2)=CX*SG
TRANS(3,3)=SX
D6 33 I=1,3
D6 33 J=1,3
3S TRANS(I,J)=TRANS(I,J)/RAD
RETURN
ENTRY OTDOMG(PBI,CBI,OMEGA,TRANS)
ASSIGN 40 TO KGG
GO TO 100
TRANS(1,1)=-CP*CX*SG-SP*CG
TRANS(1,2)=CP*CX*SG+SP*CG
TRANS(1,3)=CP*SX*SG+SP*CG
TRANS(2,1)=SP*CX*CG-CP*SG
TRANS(2,2)=SP*CX*SG+CP*SG
TRANS(3,1)=-SX*CG
TRANS(3,2)=-SX*SG
D6 AS I=1,3
GO TO 100
END

```

```

EKCL 20
C
SUBROUTINE EULER(PBI,CBI,OMEGA,TRANS)
SUBROUTINE TO GENERATE THE MATRIX B-INVERSE FROM THE EULERIAN
ANGLES PHI,CHI,AND OMEGA.
DATA RAO/57.2557792/
DIMENSION TRANS(3,3)
ASSIGN 10 TO KGG
GO TO 100
TRANS(1,1)=CP*CX*CG-SP*SG
TRANS(1,2)=-CP*CX*SG+SP*CG
TRANS(1,3)=CP*SX
TRANS(2,1)=SP*CX*CG+CP*SG
TRANS(2,2)=SP*CX*SG+CP*CG
TRANS(3,1)=-SX*CG
TRANS(3,2)=-SX*SG
TRANS(3,3)=CX
ENTRY OTDPHI(PBI,CBI,OMEGA,TRANS)
ASSIGN 20 TO KGG
GO TO 100
TRANS(1,1)=-SP*CX*CG-CP*SG
TRANS(1,2)=SP*CX*SG-CP*CG
TRANS(1,3)=SP*SX
TRANS(2,1)=CP*CX*CG-SP*SG
TRANS(2,2)=-CP*CX*SG+SP*CG
TRANS(2,3)=CP*SX
D6 23 I=1,3
D6 23 J=1,2
23 TRANS(J,1)=TRANS(J,I)/RAD
TRANS(3,1)=0.
25 RETURN
ENTRY DTPCHI(PBI,CBI,OMEGA,TRANS)
ASSIGN 30 TO KGG
GO TO 100
TRANS(1,1)=-CP*SY*CG
TRANS(1,2)=CP*SX*SG
TRANS(1,3)=CP*CX*SG
TRANS(2,1)=-SP*SX*CG
TRANS(2,2)=SP*SX*SG
TRANS(2,3)=SP*CX
TRANS(3,1)=-CX*CG
TRANS(3,2)=CX*SG
TRANS(3,3)=SX
D6 33 I=1,3
D6 33 J=1,3
3S TRANS(I,J)=TRANS(I,J)/RAD
RETURN
ENTRY OTDOMG(PBI,CBI,OMEGA,TRANS)
ASSIGN 40 TO KGG
GO TO 100
TRANS(1,1)=-CP*CX*SG-SP*CG
TRANS(1,2)=CP*CX*SG+SP*CG
TRANS(1,3)=CP*SX*SG+SP*CG
TRANS(2,1)=SP*CX*CG-CP*SG
TRANS(2,2)=SP*CX*SG+CP*SG
TRANS(3,1)=-SX*CG
TRANS(3,2)=-SX*SG
D6 AS I=1,3
GO TO 100
END

```

```

D6 43 I=1,2
43 TRANS(I,J)=TRANS(I,J)/RAD
45 RETURN I, J=0.
45
100
CF=COS(PBT/RAD)
CX=COS(CBT/RAD)
CG=CSH(OMEGA/RAD)
SF=SHI(PBT/RAD)
SX=SHI(CBT/RAD)
GO=SHI(OMEGA/RAD)
GO=TO AGR(10,20,30,40)
END

SUBROUTINE MULMM(A,B,C)
MULTIPLY 2 3X3 MATRICES TOGETHER.
DIMENSION A(3,3),B(3,3),C(3,3),D(3,3),E(3)
D6 10 I=1,3
D6 10 J=1,3
D6 10 K=1,3
C(I,J)=0.
C(I,J)=C(I,J)+A(I,K)*B(K,J)
ENTX MULMM(A,B,E)
E(I)=0.
D6 20 J=1,3
D6 20 I=1,3
E(I)=E(I)+A(I,J)*D(J)
RETURN
END

D6 43 I=1,2
TRANS(I,J)=0.
RETURN I, J=0.
CF=COS(PBT/RAD)
CX=COS(CBT/RAD)
CG=CSH(OMEGA/RAD)
SF=SHI(PBT/RAD)
SX=SHI(CBT/RAD)
GO=SHI(OMEGA/RAD)
GO=TO AGR(10,20,30,40)
END

SUBROUTINE TEMZ(T,A,B)
INCLUDE IND23,LIST
COMMON /IND23/ C(10),DK(10),T(3,3),GTEM(3,3,3),J(3)
EQUIVALENCI(GTEM(1,1),GTEM(1,1,1)),(I,J(1)),J(2),J(2)),J(3),J(3,3)
DATA PI/3.14159265/
D6 10 I=1,6
D6 5 K=1,2
J(K)=IND2(K,I)
ITEM(J1,J2)=A(I)
ITEM(J2,J1)=A(I)
CONTINUE
D6 10 I=1,6
D6 15 K=1,2
J(K)=IND2(K,I)
D6 18 K=1,3
D6 18 L=1,3
H(I)=H(I)+T(J1,K)*T(J2,L)*ITEM(K,L)
RETURN TEMZ(T,C,0)
D6 30 I=1,3
D6 25 K=1,3
J(K)=IND3(K,I)
GTEM(J1,J2,J3)=C(I)
GTEM(J2,J3,J1)=C(I)
GTEM(J3,J1,J2)=C(I)
GTEM(J2,J1,J3)=C(I)
GTEM(J1,J3,J2)=C(I)
D6 10 I=1,10
D6 35 K=1,3
J(K)=IND3(K,I)
D6 38 K=1,3
D6 38 L=1,3
D6 38 M=1,3
D(I)=D(I)+T(J1,K)*T(J2,L)*T(J3,M)*GTEM(K,L,M)
RETURN
END

```

```

EULR 580
EULR 590
EULR 600
EULR 610
EULR 620
EULR 630
EULR 640
EULR 650
EULR 650
EULR 660
EULR 680
EULR 690

```

```

MULM 10
MULM 20
MULM 30
MULM 40
MULM 50
MULM 60
MULM 80
MULM 90
MULM 100
MULM 110
MULM 120
MULM 130
MULM 140
MULM 150
MULM 160

```

```

TFM 10
TFM 20
TFM 30
TFM 40
TFM 50
TFM 60
TFM 70
TFM 80
TFM 90
TFM 100
TFM 110
TFM 120
TFM 130
TFM 140
TFM 150
TFM 160
TFM 170
TFM 180
TFM 190
TFM 200
TFM 210
TFM 220
TFM 230
TFM 240
TFM 250
TFM 260
TFM 270
TFM 280
TFM 290
TFM 300
TFM 310
TFM 320
TFM 330
TFM 340
TFM 350
TFM 360
TFM 370
TFM 380
TFM 390
TFM 400
TFM 410

```


D3DL 10 PUNCTION D3KDLR,EL,S,I,J,K,L,M)

D3DL 20 DIMENSION R(3),EL(3,3),S(3,3)

D3DL 30 DEFINE ABK(J,K,L,M,N)*2=AIJ(R,J,L)*BIJK(R,K,M,N)

D3DL 40 DEFINE AAB(I,J,K,L,M,N)*AIJ(R,I,L)*AIJ(R,J,N)*BIJK(R,K,M,N)

D3DL 50 INTEGER P

D3DL 60 DEFINE P(I,J,K,L,M)*PIJKLM(R,I,J,K,M,L)

D3DL 70

D3DL 80 Dg 1000 N=1,3

D3DL 90 SUM-SDM*(N,I)*(ABG(J,K,L,M,N)*ABB(K,J,L,M,N)*ABB(J,K,M,L,N)*ABB(KD3DL 90

D3DL 100 1 *J,M,L,N)*S(N,J)*(ABB(I,K,L,M,N)*ABB(K,I,L,M,N)*ABB(I,K,M,L,N)*N3DL 100

D3DL 110 2 *ABB(K,I,M,L,N)*S(N,K)*(ABB(I,J,L,M,N)*ABB(J,I,L,M,N)*ABB(I,

D3DL 120 3 *J,M,L,N)*ABB(J,I,M,L,N))

D3DL 130 Dg 1000 P=1,3

D3DL 140 SUM-SDM*(N,J)*S(P)*P(I,N,P,L,M)*S(N,I)*S(P,E)*P(I,N,P,L,M)

D3DL 150 1 *S(N,I)*S(P)*P(I,N,P,L,M)*S(N,I)*S(P,E)*P(I,N,P,L,M)

D3DL 160 2 *S(N,I)*S(P)*P(I,N,P,L,M)*S(N,I)*S(P,E)*P(I,N,P,L,M)

D3DL 170 3 *ABK(I,K,L,M,N)*P(I,M)*ABB(J,K,I,M,P,L,M)

D3DL 180

D3DL 190 CONTINUE

D3DL 200 D3KDL=SUM

D3DL 210 IP(L,EO,M)D3KDL=SUM/2.

D3DL 220 RETURN

END

D3DS 10 FUNCTION D3KDS(R,EL,S,I,J,K,L,M)

D3DS 20 DIMENSION R(3),EL(3,3),S(3,3)

D3DS 30 INTEGER P

D3DS 40 DEFINE BR(K,L,M)*2=EBIK(R,K,L,M)

D3DS 50 DEFINE ABB(J,K,L,M,N)*2=AIJ(R,J,L)*BIJK(R,K,M,N)

D3DS 60 SUM=0.

D3DS 70 Dg 1000 L=1,3

D3DS 80 Dg 1000 M=1,ND,I,EO,MP)SUM=SUM*(M,J)*BR(K,L,M)*S(M,K)*BR(J,L,M)

D3DS 90 IF(M,EO,LP,AND,J,EO,MP)SUM=SUM*(L,I)*BR(K,L,M)

D3DS 100 IF(L,EO,LP,AND,K,EO,MP)SUM=SUM*(L,I)*BR(J,L,M)*S(L,J)*BR(I,L,M)

D3DS 110 IF(L,EO,LP,AND,J,EO,MP)SUM=SUM*(M,K)*BR(I,L,M)

D3DS 120 Dg 1000 N=1,3

D3DS 130 IP(L,NE,LP)Gg Td 500

D3DS 140 IP(I,EO,MP)SUM=SUM*(L,M,N)*(ABB(J,E,M,L,N)*ABB(K,E,J,M,L,N))

D3DS 150 IP(J,EO,MP)SUM=SUM*(L,M,N)*ABB(I,K,M,L,N)*ABB(K,I,M,L,N)

D3DS 160 IP(K,EO,MP)SUM=SUM*(L,M,N)*ABB(I,K,M,L,N)*ABB(J,I,M,L,N)

D3DS 170 IP(I,EO,MP)SUM=SUM*(L,M,N)*ABB(I,K,M,L,N)*ABB(J,I,M,L,N)

D3DS 180 IP(J,EO,MP)SUM=SUM*(L,M,N)*S(M,K)*PIJKLM(R,I,L,M,N,P)*S(M,J)*

D3DS 190 IP(I,EO,MP)SUM=SUM*(L,M,N,P)

D3DS 200 Dg 1000 LP)Gg Td 750

D3DS 210 IP(K,NE,LP)Gg Td 1000

D3DS 220 1 PIJKLM(R,K,L,M,N,P)

D3DS 230

D3DS 240

D3DS 250

D3DS 260

D3DS 270

D3DS 280

D3DS 290

D3DS 300

1000 CONTINUE

D3KDL=SUM

IP(L,EO,M)D3KDL=SUM/2.

RETURN

END

D3DS 10 FUNCTION D3KDS(R,EL,S,I,J,K,L,M)

D3DS 20 DIMENSION R(3),EL(3,3),S(3,3)

D3DS 30 INTEGER P

D3DS 40 DEFINE AAB(I,J,K,L,M,N)*AIJ(R,I,L)*AIJ(R,J,N)*BIJK(R,K,M,N)

D3DS 50 SUM=0.

D3DS 60 IF(I,NE,LP)Gg Td 1000

D3DS 70 Dg 500 M=1,3

D3DS 80 SUM-SDM*(I,N)*S(N,I)*S(P)*P(I,N,P,L,M)*S(N,I)*S(P,E)*P(I,N,P,L,M)

D3DS 90 500 SUM-SDM*(I,N)*S(N,I)*S(P)*P(I,N,P,L,M)*S(N,I)*S(P,E)*P(I,N,P,L,M)

D3DS 1000 IF(J,NE,LP)Gg Td 2000

D3DS 1500 Dg 1500 M=1,3

D3DS 2000 SUM-SDM*(EL(M,N)*CCC(I,K,M,N)

RETURN

END

D3DS 10 FUNCTION TKTL(S,I,J,K,EL,S)

D3DS 20 DIMENSION R(3),EL(3,3),S(3,3)

D3DS 30 INTEGER P

D3DS 40 DEFINE BK(L,M)*BIJK(R,K,L,M)

D3DS 50 SUM=0.

D3DS 60 Dg 1000 I=1,3

D3DS 70 SUM-SDM*(S(L,I)*S(M,M)*S(L,I)*S(M,M)*S(L,I)*S(M,M)*S(L,I)*S(M,M)

D3DS 80 1 *S(M,M)*S(L,I)*S(M,M)*S(L,I)*S(M,M)*S(L,I)*S(M,M)*S(L,I)*S(M,M)

D3DS 90 2 *S(M,M)*S(L,I)*S(M,M)*S(L,I)*S(M,M)*S(L,I)*S(M,M)*S(L,I)*S(M,M)

D3DS 100 3 *S(M,M)*S(L,I)*S(M,M)*S(L,I)*S(M,M)*S(L,I)*S(M,M)*S(L,I)*S(M,M)

D3DS 110 CONTINUE

D3DS 120 TKTL=SUM

D3DS 130 RETURN

D3DS 140 END

D3DS 10 FUNCTION TKTL(S,I,J,K,EL,S)

D3DS 20 DIMENSION R(3),EL(3,3),S(3,3)

D3DS 30 INTEGER P

D3DS 40 DEFINE BK(L,M)*BIJK(R,K,L,M)

D3DS 50 SUM=0.

D3DS 60 Dg 1000 I=1,3

D3DS 70 SUM-SDM*(S(L,I)*S(M,M)*S(L,I)*S(M,M)*S(L,I)*S(M,M)*S(L,I)*S(M,M)

D3DS 80 1 *S(M,M)*S(L,I)*S(M,M)*S(L,I)*S(M,M)*S(L,I)*S(M,M)*S(L,I)*S(M,M)

D3DS 90 2 *S(M,M)*S(L,I)*S(M,M)*S(L,I)*S(M,M)*S(L,I)*S(M,M)*S(L,I)*S(M,M)

D3DS 100 3 *S(M,M)*S(L,I)*S(M,M)*S(L,I)*S(M,M)*S(L,I)*S(M,M)*S(L,I)*S(M,M)

D3DS 110 CONTINUE

D3DS 120 TKTL=SUM

D3DS 130 RETURN

D3DS 140 END

```

FUNCTION DIJKLM(R,I,J,K,L,M)
DIMENSION R(3)
IN=J+K+L+M
IF(MOD(IN,6).EQ.0.AND.IN.LE.18)GG T6 1000
IF(IN.EQ.6.OR.IN.EQ.9.OR.IN.EQ.12)GG T6 1050
IF(JI.NE.KI.OR.KI.NE.LI.OR.LI.NE.MI)GG T6 1040
GG T6 1100
1040 DIV*4, I100
1060 DIV*6, I100
GG T6 1100
1080 DIV*12, I100
IF(MOD(IN,3).NE.0)GG T6 1500
M3
IN/3
L*3
IF(MOD(IN,3).NE.0)GG T6 1250
L*3
IF(MOD(IN,3).NE.0)GG T6 1185
K*3
J-IN/3
GG T6 1900
1125 IF(MOD(IN,2).NE.0)GG T6 1150
J-IN/2
GG T6 1900
1150 K*1
J*1
GG T6 1900
1250 IF(MOD(IN,2).NE.0)GG T6 1375
L*2
IN/2
IF(MOD(IN,2).NE.0)GG T6 1150
K*2
J-IN/2
GG T6 1900
1375 L*1
1500 IF(MOD(IN,2).NE.0)GG T6 1750
M*2
IN/2
M*1
GG T6 1250
1750 M*1
1900 GG T6 1375
GG T6 (100,200,300),I
100 GG T6 (110,150,2000),J
110 GG T6 (120,140,3000),K
120 GG T6 (125,130,2000),L
125 GG T6 (100,2000,1000),M
130 IF(L-2)1000,145,4000
145 IF(M-2)1000,4000,3000
150 IF(K-2)1000,150,1000
160 IF(L-2)1000,170,5000
170 IF(M-2)1000,2000,1000
200 GG T6 (210,250,2000),J

```

```

D1JK 10
D1JK 20
D1JK 30
D1JK 40
D1JK 50
D1JK 60
D1JK 70
D1JK 80
D1JK 90
D1JK 100
D1JK 110
D1JK 120
D1JK 130
D1JK 140
D1JK 150
D1JK 160
D1JK 170
D1JK 180
D1JK 190
D1JK 200
D1JK 210
D1JK 220
D1JK 230
D1JK 240
D1JK 250
D1JK 260
D1JK 270
D1JK 280
D1JK 290
D1JK 300
D1JK 310
D1JK 320
D1JK 330
D1JK 340
D1JK 350
D1JK 360
D1JK 370
D1JK 380
D1JK 390
D1JK 400
D1JK 410
D1JK 420
D1JK 430
D1JK 440
D1JK 450
D1JK 460
D1JK 470
D1JK 480
D1JK 490
D1JK 500
D1JK 510
D1JK 520
D1JK 530
D1JK 540
D1JK 550
D1JK 560
D1JK 570

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210 GG T6 (220,240,1000),K
220 GG T6 (225,230,3000),L
230 IF(M-2)1000,2000,8000
240 IF(L-2)1000,345,3000
245 IF(M-2)1000,3000,1000
250 IF(K-2)1000,260,4000
260 IF(L-2)1000,270,2000
270 IF(M-2)1000,1000,4000
300 GG T6 (310,350,1000),J
310 GG T6 (315,340,3000),L
325 GG T6 (2200,1000,4000),M
330 IF(M-2)1000,5000,3000
340 IF(L-2)1000,345,1000
345 IF(M-2)1000,1000,4000
350 IF(K-2)1000,360,3000
360 IF(L-2)1000,370,2000
370 IF(M-2)1000,2000,3000
1000 RETURN
2000 FAC=1.
2010 DIJKLM=FAC*R(I)/(24.*DIVY)
RETURN
3000 MM=MOD(I,3)*1
3010 DIJKLM=(MM)/(24.*DIVY)
4000 MM=MOD(I,3)+1
GG T6 3010
5000 GG T6 2010
END

```

```

FUNCTION FLJKLM(R,I,J,K,L,M)
DIMENSION R(3)
DEFINE DJ,K,L,M)*DIJKLM(R,I,J,K,L,M)
RETURN
END

```

```

FLJK 10
FLJK 20
FLJK 30
FLJK 40
FLJK 50
FLJK 60
FLJK 70
FLJK 80
FLJK 880
FLJK 890

```

```

2100 DIJKLM=FAC*R(I)/(24.*DIVY)
RETURN
3000 MM=MOD(I,3)*1
3010 DIJKLM=(MM)/(24.*DIVY)
4000 MM=MOD(I,3)+1
GG T6 3010
5000 GG T6 2010
END

```



```

06 TO 410
330 CONTINUE
C NEW ATOM, COMPUTE DISTANCE
S=0.0
340 TP(K)=XYZ(K,11)-XYP(K) D6 340 K=1,3
XZP=0.0 D6 360 N=1,3
350 XZP=XZP+TP(K)*G(K,N) D6 350 K=1,3
360 TP(K)=(S-S*(EN-S))*(10.410.370
370 S=SQRT(S)
C CHECK IF LIST ARRAYS FULL
IF(LIST-300)390,3E0,390
380 WRITE(IGOUT,8)
06 TO 410
C ADD ATOM TO LIST
LIST=LIST+64*JJ+J
390 IF(MBODAN-1)440,440,450 D6 400 K=1,3
400 XYP(K,LIST)=XYP(K)
402 IF(MBODAN)410,402,402
410 CONTINUE
41D CONTINUE
420 CONTINUE
430 IF(MBODAN-1)440,440,450
440 RETURN COMPUTE BAND ANGLES
450 WRITE(IGOUT,10)TITLE
IJ=LIST-1
C L6GF THROUGH ATOMS
D6 560 I=1,NATOM
WRITE(IGOUT,12)TAG(K,1),K=1,2),(XYZ(I,J),J=1,3)
C FIRST LOOP THROUGH LIST
D6 580 J=1,IJ
D6 460 K=1,3
460 XPK(I)=XPK(K,J)-XYZ(K,I)
XPK(M)=0.0
D6 480 N=1,3
470 KFP(N)=XPK(I)+G(K,N)*XPK(K) D6 470 K=1,3
480 B=S*XPK(N)*EP(N)
490 S=1./D/SGRT(S)
NAT=NOMB(J)/64
II=J+1
C SECOND LOOP THROUGH LIST
D6 570 K=IE,LIST
S2=0.0
D6 500 N=1,3
500 TP(N)=XPR(N,K)-XYZ(N,I)
D6 520 N=1,3
XZP=0.0
D6 510 M=1,3
510 XZP=XZP+TP(N)*G(M,N)
520 B2=S2*XZP*TP(N)

```

```

IF(S2-SX)*(SN-S2)J570,570,530
S2=S/SQRT(S2)
D6 540 M=1,3
CTH=0.0
D6 540 M=1,3
540 CTH=CTH+XXP(M)*YPI(M)
TEMP=ABS(CTH)
IF(TEMP-1.0)560,560,550
550 CTH=CTH/TEMP
560 CTH=CTH*0.99ACOS(CTH)/PI
570 CONTINUE
580 RETURN
END

```

```

EODN1160
EODN1170
EODN1180
EODN1190
EODN1200
EODN1210
EODN1220
EODN1230
EODN1240
EODN1250
EODN1260
EODN1270
EODN1280
EODN1290
EODN1300
EODN1310
EODN1320
EODN1330
EODN1340
EODN1350
EODN1360
EODN1370
EODN1380
EODN1390
EODN1400
EODN1410
EODN1420
EODN1430
EODN1440
EODN1450
EODN1460
EODN1470
EODN1480
EODN1490
EODN1500
EODN1510
EODN1520
EODN1530
EODN1540
EODN1550
EODN1560
EODN1570
EODN1580
EODN1590
EODN1600
EODN1610
EODN1620
EODN1630
EODN1640
EODN1650
EODN1660
EODN1670
EODN1680
EODN1690
EODN1700
EODN1710
EODN1720
EODN1730

```



```

FUNCTION ALJ(R,I,J)
DIMENSION R(3)
G6 T6 (10,20,30),I
G6 T6 (100,200,300),J
G6 T6 (10,20,30),I
G6 T6 (200,300,100),J
ALJ=0.
RETURN
MM=MGD(I,1,3)*1
ALJ=R(MM)
RETURN
MM=MGD(I,3)*1
ALJ=R(MM)
RETURN
END
300

FUNCTION BIJK(R,I,JJ,KK)
DIMENSION R(3)
IF(JJ.EQ.KK)DIV=1.
IF(JJ.EQ.KK)DIV=1.
K=MINO(JJ,KK)
K=MAX(JJ,KK)
G6 T6 (10,20,30),I
G6 T6 (100,200,300),J
G6 T6 (10,20,30),I
G6 T6 (200,300,100),J
BIJK=0.
RETURN
MM=MBDI(I,3)*1
BIJK=S*(MM)/DIV
RETURN
MM=MBDI(I,3)*1
BIJK=S*(MM)/DIV
RETURN
END
400

FUNCTION CIJEL(R,I,JJ,KK,LL)
DIMENSION R(3)
IF(JJ.EQ.KK.AND.JJ.EQ.LL)G6 T6 7
IF(JJ.EQ.KK.AND.JJ.NE.LL.AND.KK.NE.LL)G6 T6 B
IF(JJ.NE.KK.I,2,3
1 J=JJ
L=KK
K=LL
GB TB 4
2 J=MINO(JJ,LL)
K=KK
L=MAXO(JJ,LL)
G6 T6 4
G6 T6 4
K=LL
L=JJ
4 DIV=3.
G6 T6 9
7 J=JJ
K=JJ
DIV=1.
G6 T6 9
8 J=1
K=2
L=3
DIV=6.
G6 T6 (10,20,30),I
G6 T6 (12,15,30),J
G6 T6 (13,100,100),K
G6 T6 (100,200,300),L
IF(K=2)G6 T6 1,2,3,4,5,6,7,8,9,10
IF(K=2)G6 T6 1,2,3,4,5,6,7,8,9,10
G6 T6 (23,24,300),K
G6 T6 (300,100,200),L
IF(L=2)G6 T6 100,100,100
IF(L=2)G6 T6 26,26,100
G6 T6 (32,35,100),J
G6 T6 (33,34,200),K
G6 T6 (300,200,100),L
IF(L=2)G6 T6 100,100,100
IF(L=2)G6 T6 36,36,300
IF(L=2)G6 T6 300,300,100
CIJKL=0.
RETURN
MM=MGDI(I,1,3)*1
CIJEL=R(NM)/(G,*DIV)
RETURN
MM=MGDI(I,3)*1
CIJEL=R(NM)/(G,*DIV)
RETURN
END
200
300

```

```

CIJK 10
CIJK 20
CIJK 30
CIJK 40
CIJK 50
CIJK 60
CIJK 70
CIJK 80
CIJK 90
CIJK 100
CIJK 110
CIJK 120
CIJK 130
CIJK 140
CIJK 150
CIJK 160
CIJK 170
CIJK 180
CIJK 190
CIJK 200
CIJK 210
CIJK 220
CIJK 230
CIJK 240
CIJK 250
CIJK 260
CIJK 270
CIJK 280
CIJK 290
CIJK 300
CIJK 310
CIJK 320
CIJK 330
CIJK 340
CIJK 350
CIJK 360
CIJK 370
CIJK 380
CIJK 390
CIJK 400
CIJK 410
CIJK 420
CIJK 430
CIJK 440
CIJK 450
CIJK 460
CIJK 470
CIJK 480
CIJK 490
CIJK 500
CIJK 510
CIJK 520
CIJK 530
CIJK 540

```



```

9220 FORMAT(1X,5(I3,F10.4))
1*5
IF(LILE,NDENJG) T0 210
RETURN
END

SUBROUTINE WEIGHT
C THIS ROUTINE REVISED AN/O/R RESEQUENCE ON HCT, 28, 1968

C DUMMY ROUTINE
ENTRY REJECT
DUMMY ROUTINE
RETURN
END

XPAR
PPRC
COPMN/XPARK/HPAR,ATGX(3,3),XTRAI(3,3),PARM(60),PARNAM(2,60),IPAR(60)
1,IRPAR(60),GXIZ(3),SKYZ(3),GXPR(3),T(L3,3),SL(3,3),TRNE(3,3)
2,ITRNS(3,3),TRANSI(3,3),ITRNSI(3,3),RTEH(3),DTEH(6),GTEN(10)
END
TAPE
PPRC
COPMN/TAPE/IN,INN,IOUT,ISCI,ISC2,ISC3,ISC4,ISCS,IPUN
END
LSWT
PPRC
COPMN/LSWT/M(200),TEXT,IPARA(1000),WRANK,RCYCL,LABEL(3),JSCRE(10)
1,NESE, SIGMA, NDEGN, A(200)
END
ACPN
PPRC
COPMN/A/BETA(6,60),G(3,3),ISHT(60),NATOM,TAR(2,60),TITLE(18),XXYZ
13,60),P,CK(10,60),OR(15,60)
END
DCM
PPRC
COPMN/O/CALC,AINO(60),ANW(2,20),ICALC,RI NH(60),DADM(6,60),DADM
1 60),DAXI(3,60),DROH(6,60),DRPM(60),DRDM(3,60),IR(3),IR(3),ISCAT(2,
2 60),ISCL,MSEL,OCCL(60),OCUP(60),SCALE(10),SCAT(20),SITE(60)
3,DARCI(0,60),DRUC(10,60),DADD(15,60),DRDD(15,60),AMINUS,HTINUS
4,DRDEL(6),NOECN
DIMENSION SAVE(60),KDEGN(2640),AK(2640)
FOUVALENCE (SAVE,AINO),(KDEGN,AA,OADCI(1,37))
END
IN23
PPRC
COPMN/IN23/IN2(2,6),IND(3,10)
END

```

```

* ROUTINE TO ADJUST THE SIZE OF THE MEMORY FIELD OF AN ACTIVE PROGRAM
* CALLING SEQUENCE
* CALL CORSZ(ARRAY(N))
* ARRAY I MUST BE AT THE END OF THE I+ OR I+ BANK OF THE PROGRAM.
* N IS THE LARGEST INDEX REQUIRED BY THE PROGRAM.
*
$(( )
CORSZ* L AO,0,X11 * GET FINAL ADDRESS
TNE AO,LAST * SAME SIZE AS BEFORE?
J 2,X11 * YES - RETURN,
L AI,LAST
L AD,AI
TG AD,AI * NEED MORE CORE?
ER CORSES * YES - RETURN,
J 2,X11 * NO - REDUCE NEEDS.
CORSZ1 ER MOPRES * GET MORE.
LAST J 2,X11
*0
END

```

```

POGN 320
POGN 330
POGN 340
POGN 350
POGN 360
DUMMY 1D
DUMMY 2D
DUMMY 3D
DUMMY 4D
DUMMY 5D
DUMMY 6D
DUMMY 7D
DUMMY 8D
DUMMY 9D
DUMMY 10D

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SUBROUTINE STMINV (A,MRANK,SCR,MCS,B,EFS,DET,FRANK)
C THIS ROUTINE REVISED AND/OR RESEQUENCED OCT. 2E, 1968
C
C ARGUMENT LIST
C A - INPUT AND OUTPUT ARRAY - STORED BY ROWS WITH ONLY THE
C UNIQUE PORTION IN STORAGE
C MRANK - INPUT SIZE OF SYSTEM OF EQUATIONS
C SCR - A SCALAR ARRAY OF DIMENSION MRANK
C E - MATRIX TO BE PERMULTIPLIED BY THE INVERSE OF A
C B,E - SIZE OF SMALLEST ELEMENT TO BE USED AS A PIVOT
C DET - OUTPUT VALUE OF THE DETERMINANT OF A
C FRANK - ACTUAL RANK OF A ( THIS IS AN OUTPUT VALUE.)
C
C DIMENSION A(1),MRANK(1),SCR(1)
C
C INITIALIZE
DET=1.0
DO 100 I=1,MRANK
100 SCR(I)=START MASTER LOOP
DO 280 I=1,MRANK
C SEARCH FOR PIVOT TESTING ONLY THE DIAGONAL ELEMENTS
C EIG=0.0
C PRESET INDEX AND STEP FOR DIAGONAL ELEMENTS
J=MRANK
LJ=MRANK+1
DO 130 M=1,MRANK
K=J
J=J-EJ
K=K-EJ-1
C CHECK IF THIS ELEMENT ALREADY USED AS PIVOT
IF(EGCR(K))130,110,110
J INOXES A(M,K)
C 110 TEMP=ABS(A(J))
IF(TEMP-EIG)130,130,120
EIG=TEMP
K=LJ
K=LJ
C 130 CONTINUE
C COMPARE LARGEST DIAGONAL ELEMENT WITH EPS
IF(EIG<EPS)140,150,150
SINGULARITY RETURN
C 140 FRANK=I-1
RETURN
C 150 SCR(I)=1.0
K=L INOXES A(M,K)
DET=DET*(A(M))
Q=1.0/(A(L))
C SET UP INDEXING FOR ELIMINATION STEPS
J=K-MRANK
NJ=NAME*1
I=0
J=K-1
IF(I)210,210,160
160 DO 200 N=1,K

```

```

STMV 10
STMV 20
STMV 30
STMV 40
STMV 50
STMV 60
STMV 70
STMV 80
STMV 90
STMV 100
STMV 110
STMV 120
STMV 130
STMV 140
STMV 150
STMV 160
STMV 170
STMV 180
STMV 190
STMV 200
STMV 210
STMV 220
STMV 230
STMV 240
STMV 250
STMV 260
STMV 270
STMV 280
STMV 290
STMV 300
STMV 310
STMV 320
STMV 330
STMV 340
STMV 350
STMV 360
STMV 370
STMV 380
STMV 390
STMV 400
STMV 410
STMV 420
STMV 430
STMV 440
STMV 450
STMV 460
STMV 470
STMV 480
STMV 490
STMV 500
STMV 510
STMV 520
STMV 530
STMV 540
STMV 550
STMV 560
STMV 570

```

```

MJ=NJ-1
C J INOXES A(KE,N)
TEMP=OP(A(J))
MJ=NJ
DO 170 M=N,IK
E=E*1
C J INOXES A(M,K)
K INOXES A(M,N)
KJ=J-1
170 J=NJ
C J INOXES A(KE,M)
A(J)=TEMP
L=EL
IF(JK=NRANK)180,180,200
DO 190 M=J,MRANK
E=E*1
K INOXES A(M,N)
L INOXES A(M,K)
190 A(E)=(E)-TEMP*SCR(M)=A(J)
200 CONTINUE
210 E=EL+NRANK-EK
220 DO 240 M=J,MRANK
J=J+1
C J INOXES A(M,KE)
TEMP=SCR(N)=A(J)*Q
MJ=NJ
DO 230 M=N,MRANK
E=E*1
C K INOXES A(M,N)
K INOXES A(M,KE)
A(J)=A(E)-TEMP*A(K)
230 J=NJ
240 J=NJ
250 E=EL
C K INOXES A(KE,K)
A(K)=Q
260 DO 270 M=J,MRANK
E=E*1 INOXES A(M,KE)
270 A(E)=OP(A(K))
280 CONTINUE
C INVERSION COMPLETE, EXIT IF INVERSION ONLY
IF(MCR)>360.360,290
290 DO 300 I=1,NCE
O=O+MRANK
160 DO 200 N=1,K

```



```

32 TP(I,I-1) = 0
GG TO 20
C
31 TM 2,1 = TM 2,1
TM 3,2 = TM 2,1
TM 3,3 = TM 2,1
NL P=3
TM 2,2 = 2./3.
TM 3,1 = TM 2,2
C
20 IF IERR.EQ.0,GG TO 101
      REAO CELL SIGMAS AND CORRELATION MATRIX, CHANGE TO VAR-COV
      REAO CELL SIGMAS AND CORRELATION MATRIX, CHANGE TO VAR-COV
C
100 REAO CELL SIGMAS AND CORRELATION MATRIX, CHANGE TO VAR-COV
      CONVERT SIGMA OF ANGLES TO SIGMA OF COSINE
      DO 102 I=4,5
102 SIG(I)=SIG(I)*SIG(I)*PI/180.0
      WRITER IOUT,106,NCCELL,(SIG(I),I=1,6)
      DO 200 I=1,6
      REAO IN,34,(SIG(I),J=1,I)
      SIG(I,I)=1.0
      WRITER IOUT,201,(CELL(I),J=1,3),(SIG(I),J=1,I)
      SIG(I,I)=SIG(I,I)*SIG(I,I)
      SIG(I,I)=SIG(I,I)*SIG(I,I)
200 SIG(I,I)=SIG(I,I)*SIG(I,I)
101 WRITER IOUT,109,JPGE,JBETA
      IO=IN
C
      IF IERR.NE.2,GG TO 300
      SET TO BEAO AUXILIARY INPUT UNIT
      IO=IN
C
300 IO=BEAO STRUCTURE PARAMETERS
      REAO IN,50,(ATOM(J),J=1,2),(XYZI(J),J=1,3),ITP(I),(BETA(J),I),J=
      1,6)
      IF ITP(I)112,113,112
112 WRITER IOUT,110,(ATOM(J),J=1,2),(XYZI(J),J=1,3),(BETA(J),I),J=1,
      1)
      GG TO 6
113 WRITER IOUT,111,(ATOM(J),J=1,2),(XYZI(J),J=1,3),BETA(I,I)
6 CONTINUE
      EQ.0,4R,(ILV,EG,U,ANO,IERR,NE,2)) GG TO 103
      REAO TEMPERATURE FACTOR SIGMAS AND CORR. MATRIX
C
      DO 41 I1=1,NA
      I1=I1
      IF ITP(I)142,41,42
42 REAO I1,50,(SIG(J),J=1,6)
      WRITER IOUT,202,(ATOM(J),J=1,2),JBETA,(SIG(J),J=1,6)
      DO 43 J1=6,SIGEL(J,K,I),K=1,J)
      SIGEL(J,I)=1.0
      WRITER IOUT,204,(BETA(J),I),(SIG(J,K,I),K=1,J)
C
      DO 45 K=1,J
      SIGEL(J,K,I)=SIGEL(J,K,I)*SIG(J,I)
203 SIGEL(K,I)=SIGEL(J,K,I)
41 CONTINUE
103 IF IERR.EQ.0,4R,(IERR,EG,0,ANO,IERR,NE,2)) GG TO 105
      REAO ATOM POSITION SIGMAS AND CORRELATION MATRIX

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```

      NA=38NA
      NA=38NA
      DO 205 I=1,NA
      J1=I+1
      J1=I+2
205 WRITER IOUT,207,(ATOM(J,I),J=1,2),(SIG(I),J=1,I),J1
      WRITER IOUT,208
      L=0.
      DO 223 I=1,NA
      DO 225 J=1,3
      IJ=3*(I-1)+J
      SIG(I,J)=0
      SIG(I,J)=1.0
      WRITER IOUT,209,(ATOM(K,I),K=1,2),(SIG(I),K=1,I),J)
      GG TO 216
215 IF (J.NE.I)GG TO 21E
      WRITER IOUT,209,(ATOM(K,I),K=1,2),(SIG(I),K=1,I),J)
      GG TO 221
21E IF (I,0E,4)GG TO 220
      GG TO 216
      GG TO 216
220 WRITER IOUT,210,(JFGS(J),(SIG(I),K=1,I),K=1,10)
221 WRITER IOUT,211,(SIG(I),K=1,I),J)
C
      CONVERT CORRELATION MATRIX TO VARIANCE-COVARIANCE MATRIX
216 DO 222 K=1,I
222 SIG(I,K)=SIG(I,K)*SIG(I)*2
      DO 223 K=1,I
      DO 225 L=1,I
      CORR(L,I)=SIG(I,K)*SIG(I,L)
105 IF (IERR.EQ.0)GG TO 44
C
43 CALL E90(ANO,IERR)
44 IF (ILV)45,46,45
44 CALL E90(ANO,IERR)
C
45 CALL BLVIE
C
      EMO OF CALCULATION, TERMINATE PROGRAM
46 CALL BLT
      END

```



```

380 KA*KA*1
390 DO 410 L=1,3
C IC-IC*JP
JP*JP*1
IF(IPAR*(KPAR))400,410,400
IF(CV(KC)*CV(KA))400,410,400
C 400 CV(KC)*CV(KA)
KA*KA*1
410 CONTINUE
L=IIP(K)
NG*NCN(I,L))
C 440 DO 460 L=1,N9
KPAR=KPAR*1
IF(KPAR*(KPAR))450,460,450
ADVANCE COUNTER
C 450 KA*KA*1
460 CONTINUE
470 CONTINUE
480 NP*NP*1
C LOOP ITEMP=008 VAR-COV MVS FOR ATOM I TEMP FACTORS
DO 530 J=1,N81
IF(KPAR*(KPAR))520,530,520
IF(KPAR*(KPAR))520,530,520
ADVANCE INDEX AND REDUCE INCREMENT
C 520 KA*KA*INCR
530 INCR=INCR*1
540 CONTINUE
C ATOM VARIANCE-COVARIANCE MATRIX IS EXTRACTED, NOW MODIFY FOR
CONSTRAINTS
IF(MDSON.EQ.0) GO TO 570
N9=308
DO 565 I=1,MDSON,2
IPAR=I*(CNSTR(I))
IF(IPAR.LT.2)9R,IPAR,GT.4)GO TO 565
IAT=I*(CNSTR(I))
I=I*(CNSTR(I))
IPAR=3*(IAT-1)*IPAR-1
DO 560 J=1,N8
IF(KPAR*(KPAR))550,560,560
COMPLETE COVARIANCE OF POSITION WITH A GEPINDED POSITION,
KA*INDEX(I,J),JNT(K)
CV(KB)*CV(KB)*CV(KA)*CNSDON(I+1)
C 560 CONTINUE
DO 563 I=1,MDSON,2
IF(KPAR*(KPAR))550,560,560
IF(KPAR.LT.2)9R,IPAR,GT.4)GO TO 563
JAT=J*(CNSTR(K))
L=I*(CNSTR(K))
IFPAR=3*(JAT-1)*IPAR-1
KA*INDEX(O,J,L)
EG=INDELL(IPAR,IPAR)
CV(KB)*CV(KB)*CNSDON(I+1)*CNSDON(KK+1)*CV(KA)
ERR 2320
ERR 2330
ERR 2340
ERR 2350
ERR 2360
ERR 2370
ERR 2380
ERR 2390
ERR 2400
ERR 2410
ERR 2420
ERR 2430
ERR 2440
ERR 2450
ERR 2460
ERR 2470
ERR 2480
ERR 2490
ERR 2500
ERR 2510
ERR 2520
ERR 2530
ERR 2540
ERR 2550
ERR 2560
ERR 2570
ERR 2580
ERR 2590
ERR 2600
ERR 2610
ERR 2620
ERR 2630
ERR 2640
ERR 2650
ERR 2660
ERR 2670
ERR 2680
ERR 2690
ERR 2700
ERR 2710
ERR 2720
ERR 2730
ERR 2740
ERR 2750
ERR 2760
ERR 2770
ERR 2780
ERR 2790
ERR 2800
ERR 2810
ERR 2820
ERR 2830
ERR 2840
ERR 2850
ERR 2860
ERR 2870
ERR 2880
ERR 2890
ERR 2320
ERR 2330
ERR 2340
ERR 2350
ERR 2360
ERR 2370
ERR 2380
ERR 2390
ERR 2400
ERR 2410
ERR 2420
ERR 2430
ERR 2440
ERR 2450
ERR 2460
ERR 2470
ERR 2480
ERR 2490
ERR 2500
ERR 2510
ERR 2520
ERR 2530
ERR 2540
ERR 2550
ERR 2560
ERR 2570
ERR 2580
ERR 2590
ERR 2600
ERR 2610
ERR 2620
ERR 2630
ERR 2640
ERR 2650
ERR 2660
ERR 2670
ERR 2680
ERR 2690
ERR 2700
ERR 2710
ERR 2720
ERR 2730
ERR 2740
ERR 2750
ERR 2760
ERR 2770
ERR 2780
ERR 2790
ERR 2800
ERR 2810
ERR 2820
ERR 2830
ERR 2840
ERR 2850
ERR 2860
ERR 2870
ERR 2880
ERR 2890
563 CONTINUE
565 CONTINUE
570 K8=MKL*1
DO 590 I=1,LEZY
SIG(K8(I))*CV(K8)
C 590 CALL CONTRACT MATRIX TO T88 MINIMUM REQUIRED
790 CALL CORSEZ(BIG(LITZ))
C READ AND CONVERT CELL ERROR MATRIX
READ IN,6N(SIG(J,I)),I,6,I*1,6) *
I8R*1
DO 800 I=1,3
ANG(1)=G(I,1)
ANG(2)=G(I,2)/((A(1)*A(1))
ANG(3)=G(I,3)/((A(1)*A(1))
DO 810 I=1,3
910 S(I)=SQRT(1.0-ANG(I)**2)
DO 840 I=1,6
IF(L.E.3.AND..J.E.3) GO TO 840
SIG(J,I)=800.99)*S(I-3)
GO TO 840
820 SIG(J,I)=SIG(J,I)*S(I-3)
830 SIG(J,I)=SIG(J,I)*S(I-3)*S(J-3)
840 SIG(I,J)=SIG(J,I)
850 IF(ICENT)860,860,880
C 860 EXPAND SYMMETRY OPERATORS FOR A CENTRIC CRYSTAL
DO 870 I=1,N8S
DO 870 J=1,N8S
TS(J,ITEMP)--TS(J,I)
DO 870 K=1,3
870 R8(K,J,ITEMP)--R8(K,J,I)
N8S=ITEMP
880 COMPUTE BOND FUNCTIONS
890 CALL GORDAN(MODAN,9)
900 IF(MODAN)910,910
C 910 CALL SLVTS
920 CALL END OF JOB
ERR 2900
ERR 2910
ERR 2920
ERR 2930
ERR 2940
ERR 2950
ERR 2960
ERR 2970
ERR 2980
ERR 2990
ERR 3000
ERR 3010
ERR 3020
ERR 3030
ERR 3040
ERR 3050
ERR 3060
ERR 3070
ERR 3080
ERR 3090
ERR 3100
ERR 3110
ERR 3120
ERR 3130
ERR 3140
ERR 3150
ERR 3160
ERR 3170
ERR 3180
ERR 3190
ERR 3200
ERR 3210
ERR 3220
ERR 3230
ERR 3240
ERR 3250
ERR 3260
ERR 3270
ERR 3280
ERR 3290
ERR 3300
ERR 3310
ERR 3320
ERR 3330
ERR 3340
ERR 3350
ERR 3360
ERR 3370
ERR 3380
ERR 3390
ERR 3400

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SUBROUTINE BODAM (BOD)
C TBIS ROUTING REVISED AND/OR RESUBROUTED ON OCT. 26, 1966
C BOND DISTANCE AND ANGLE SUBPROGRAM WITH ERRORS
C
COMMON/ABLE/XYZ(3,60),BBT(6,60),AL(3),ANCI(3),AS(3),CR(3),ATOM(2,
1 60),SIGMA(6,6),SIGM(6,60),RS(3,3),TF(6,3),TF(6,3),TF(6,3),
2 NA,NSB,VDLIMIT(3),PI,CI(3,3),NLE,IBRR,TITLE(10),CORE(1)
COMMON/SABE/XYZP(3,1000),IATP(100)
DIMENSION YR(3),XYZ(3),YR(3),SIGM(6,6),DLDI(6),DSDX(9,2),YF(3),
1 DLDA(6,2),BIQY(9,9),DNDA(6),DNDI(9),DTBDA(6),PTBDX(9),XZP(3),
2 X(3,3),NXX(6,3),DX(3),DY(3),DZX(3),DDBD(3)
EQUILALNCEB (DLDA,DSDX),NXX(1),NXX(2),NXX(3),NXX(4),NXX(5),NXX(6),NXX(7),NXX(8),NXX(9),NXX(10),NXX(11),NXX(12),NXX(13),NXX(14),NXX(15),NXX(16),NXX(17),NXX(18),NXX(19),NXX(20),NXX(21),NXX(22),NXX(23),NXX(24),NXX(25),NXX(26),NXX(27),NXX(28),NXX(29),NXX(30),NXX(31),NXX(32),NXX(33),NXX(34),NXX(35),NXX(36),NXX(37),NXX(38),NXX(39),NXX(40),NXX(41),NXX(42),NXX(43),NXX(44),NXX(45),NXX(46),NXX(47),NXX(48),NXX(49),NXX(50),NXX(51),NXX(52),NXX(53),NXX(54),NXX(55),NXX(56),NXX(57),NXX(58),NXX(59),NXX(60),NXX(61),NXX(62),NXX(63),NXX(64),NXX(65),NXX(66),NXX(67),NXX(68),NXX(69),NXX(70),NXX(71),NXX(72),NXX(73),NXX(74),NXX(75),NXX(76),NXX(77),NXX(78),NXX(79),NXX(80),NXX(81),NXX(82),NXX(83),NXX(84),NXX(85),NXX(86),NXX(87),NXX(88),NXX(89),NXX(90),NXX(91),NXX(92),NXX(93),NXX(94),NXX(95),NXX(96),NXX(97),NXX(98),NXX(99),NXX(100),NXX(101),NXX(102),NXX(103),NXX(104),NXX(105),NXX(106),NXX(107),NXX(108),NXX(109),NXX(110),NXX(111),NXX(112),NXX(113),NXX(114),NXX(115),NXX(116),NXX(117),NXX(118),NXX(119),NXX(120),NXX(121),NXX(122),NXX(123),NXX(124),NXX(125),NXX(126),NXX(127),NXX(128),NXX(129),NXX(130),NXX(131),NXX(132),NXX(133),NXX(134),NXX(135),NXX(136),NXX(137),NXX(138),NXX(139),NXX(140),NXX(141),NXX(142),NXX(143),NXX(144),NXX(145),NXX(146),NXX(147),NXX(148),NXX(149),NXX(150)
DATA IOUT/6/
1002 PERMAT(4X,2A3,4F10.5,10X,18)
8999 PERMAT(31B,THE ATOM ARRAY IS OVERFLOWING, //15X,5A8EDEDUB TBB LINGDN 210
ITTS OF THE BOND DISTANCE AND TRY AGAIN.)
9000 PERMAT(1B1,18A4/25B BOND DISTANCES BETWEEN *P5,2,5B AND *P5,2,5B AND *P5,2,10BOND 230
1 ANGSTROMS//10X,6BATOM 1,7XHX,9X,18X,9X,1RZ,2X,6BATOM 2,7X,18X,9X,BOND 240
2,1RZ,9X,1RZ,4X,9BDISTANCE,3XSBERRR,8X,6BNUMBER//10X2A3,3P10.5,6X3BOND 250
3,1E1)
9001 PERMAT(10X2A3,3P10.5,50X10)
9002 PERMAT(1B1,18A4/59B BOND ANGLES AND BERRS FOR ATOMS WITH INTERATOM 260
2,5B AND *P5,2,5B AND *P5,2,10BOND 270
20GL IS ATOM-CENTRAL ATOM *P5,2, THE NUMBER POINTS TO AN EXTRA 280
3 IN THE BOND DISTANCE OUTPUT.)
9003 PERMAT(15X,2A3,16,12X,2A3,16,P17.2,P10+2)
9005 PERMAT(46X2A3,5F10.5,10)
9010 PERMAT(//10X,12BCENTRAL ATOM,5X2A3,3P10.5//15X,6BATOM 1,2X,6BNUMBER 340
1ER,10XBATOM 2,2X,6BNUMBER,10X,5BANCLB,5X,5BERRR/)
WRITE(OUT,9000)TITLE,DLIMIT(1),DLIMIT(3),(ATOM(J,1),J=1,2),(XYZ(J,BOND 370
1,1),J=1,2) PRELIMINARY INFORMATION FOR SEARCHING FOR ATOMS
PROGRAM(1)M(4)M(3)
D6 61 J=1,3
XYZP(J,1)=XYZ(J,1)
DBD(J)=PBD(AI,J)
D61 DIX(J)=ABC(J)DLIMIT(3)
C 61 DIX(J)=ABC(J)DLIMIT(3)
C
C THE INTG TBB GENERATED ATOM LIST
C
C THE ELEMENTS OF THE GREAT IATP ARE 6A*ATOM NUMBER + D*HEMISTRY NODDN 470
M(A)=3MA
IATP(1)=65
D6 37 I=1,9
D6 37 J=1,2
37 DBDI(I,J)=0
EATON=1
SN=DLIMIT(1)+2
SI=DLIMIT(3)+2
C
C LOOP THROUGH THE ATOMS IN THE ASYMMETRIC UNIT
D6 I I=1,NA

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ELVR2320
ELVR2330
ELVR2340
ELVR2350
ELVR2360
ELVR2370
ELVR2380
ELVR2400
ELVR2410
ELVR2420
ELVR2430
ELVR2440
ELVR2450
ELVR2460
ELVR2470
ELVR2480
ELVR2490
ELVR2500
ELVR2510
ELVR2520
ELVR2530
ELVR2540
ELVR2550
ELVR2560
ELVR2570
ELVR2580
ELVR2590
ELVR2600
ELVR2610
ELVR2620
ELVR2630
ELVR2640

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ELVR1740
ELVR1750
ELVR1760
ELVR1770
ELVR1780
ELVR1790
ELVR1800
ELVR1810
ELVR1820
ELVR1830
ELVR1840
ELVR1850
ELVR1860
ELVR1870
ELVR1880
ELVR1890
ELVR1900
ELVR1910
ELVR1920
ELVR1930
ELVR1940
ELVR1950
ELVR1960
ELVR1970
ELVR1980
ELVR1990
ELVR2000
ELVR2010
ELVR2020
ELVR2030
ELVR2040
ELVR2050
ELVR2060
ELVR2070
ELVR2080
ELVR2090
ELVR2100
ELVR2110
ELVR2120
ELVR2130
ELVR2140
ELVR2150
ELVR2160
ELVR2170
ELVR2180
ELVR2190
ELVR2200
ELVR2210
ELVR2220
ELVR2230
ELVR2240
ELVR2250
ELVR2260
ELVR2270
ELVR2280
ELVR2290
ELVR2300
ELVR2310

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ELVR2320
ELVR2330
ELVR2340
ELVR2350
ELVR2360
ELVR2370
ELVR2380
ELVR2400
ELVR2410
ELVR2420
ELVR2430
ELVR2440
ELVR2450
ELVR2460
ELVR2470
ELVR2480
ELVR2490
ELVR2500
ELVR2510
ELVR2520
ELVR2530
ELVR2540
ELVR2550
ELVR2560
ELVR2570
ELVR2580
ELVR2590
ELVR2600
ELVR2610
ELVR2620
ELVR2630
ELVR2640

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SUBROUTINE CRRM1(SIGZ,NN,II,JJ,CORR,KK,LL,MM)
C THIS ROUTINE REVISED ANO/GR RESEQUENCED ON OCT. 2E, 1968
C THIS ROUTINE EXTRACTS THE COVARIANCE ELEMENTS BETWEEN TWO ATOMS
C SIGZ(NN,II) IS THE COVARIANCE ELEMENTS BY NN
C IJ = ATOM NUMBER OF FIRST ATOM
C KI = ATOM NUMBER OF SECOND ATOM
C JJ = ATOM NUMBER OF SECOND NUMBER
C CORR IS THE WAGLE POSITION VAR-COV MATRIX
C KK AND LL DESCRIBE THE BLOCK OF SIGZ TO BE FILLED
C MM = THE NUMBER OF ATOMS (NEEDED TO COMPUTE THE BARK OF CORR)
C
DIMENSION SIGZ(NN,NN),CORR(7260)
IK=MM
IL=II-2
IJ=3*IJ-2
KI=KK-1
LI=LL-1
IP(II-JJ),I,2,3
IX=IJ
1 JI=((II-I)*IL)/2+IJ
GO TO 4
3 JI=((II-I)*IL)/2+IJ
4 DO 5 I=1,3
L=JI
I1=LI
D6 6 J=1,3
J1=JKI
SIGZ(I1,J1)=CORR(L)
6 L=L+1
5 JI=JI-IX+I-1
2 SIGZ(I1+1,KI+1)=SIGZ(KI+1,I1+1)
D6 7 I=2,3
I1=LI
I2=LI+1
J1=I1+KI
SIGZ(I1,J1)=SIGZ(J1,I1)
IX=I-1
D6 7 J=1,IX
J2=JKI
SIGZ(I1,J2)=SIGZ(J1,I2)
7 SIGZ(I2,J1)=SIGZ(I1,I2)
RETURN
END

```

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CRR1 10
CRR1 20
CRR1 30
CRR1 40
CRR1 50
CRR1 60
CRR1 70
CRR1 80
CRR1 90
CRR1 100
CRR1 110
CRR1 120
CRR1 130
CRR1 140
CRR1 150
CRR1 160
CRR1 170
CRR1 180
CRR1 190
CRR1 200
CRR1 210
CRR1 220
CRR1 230
CRR1 240
CRR1 250
CRR1 260
CRR1 270
CRR1 280
CRR1 290
CRR1 300
CRR1 310
CRR1 320
CRR1 330
CRR1 340
CRR1 350
CRR1 360
CRR1 370
CRR1 380
CRR1 390
CRR1 400
CRR1 410
CRR1 420
CRR1 430
CRR1 440
CRR1 450
CRR1 460
CRR1 470

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SUBROUTINE CELLDASDA,A,ANG,AS,CS,VGL)
C THIS ROUTINE REVISED AND/OR RESEQUENCED ON OCT. 2E, 196E
C
DIMENSION A(3),ANG(3),AS(3),CS(3),DASDA(6,6),SH(3)
C ROUTINE TO COMPUTE THE DERIVATIVES OF THE RECIPROCAL LATTICS
C PARAMETERS WITH RESPECT TO THE REAL CELL PARAMETERS.
C OASDA(I,J)= DERIVATIVE OF RECIPROCAL PARAMETER I WITH RESPECT
C TO REAL CELL PARAMETER J.
TEMP=(A(1)+A(2)+A(3))/VGL**2
SNPRG0=1.0
C COMPUTE SINES OF REAL SPACE ANGLES AND PRODUCT OF SINES
DO 100 I=1,3
SN(I)=SQRT(1.0-ANG(I)**2)
100 SNPRG=SN(I)*SNPRG
C REAL CELL DERIVATIVE ARRAY
DO 110 I=1,6
DO 110 J=1,6
110 DASDA(I,J)=0.0
C COMPUTE DERIVATIVES
DO 120 I=1,3
TEMP1=TEMP*AS(I)
J=MOD(I,3)+1
I=I+1
DASDA(I,I)=-AS(I)/A(I)
DASDA(I,L)=-TEMP1*SN(J)*SN(K)*CS(K)*-AS(L)*ANG(L)/SN(L)**2
DASDA(I,3,I+3)=-SN(I)/SNPRG
DASDA(I,J+3)=-TEMP1*SN(I)*SN(K)*CS(K)
DASDA(L,I+3)=-TEMP1*SN(I)*SN(J)*CS(J)
DASDA(L,J+3)=-SN(L)*ANG(K)/SNPRG+CS(I)*ANG(K)/SN(K)**2
RETURN
END

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CELD 10
CELD 20
CELD 30
CELD 40
CELD 50
CELD 60
CELD 70
CELD 80
CELD 90
CELD 100
CELD 110
CELD 120
CELD 130
CELD 140
CELD 150
CELD 160
CELD 170
CELD 180
CELD 190
CELD 200
CELD 210
CELD 220
CELD 230
CELD 240
CELD 250
CELD 260
CELD 270
CELD 280
CELD 290
CELD 300
CELD 310
CELD 320
CELD 330
CELD 340
CELD 350
CELD 360

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SUBROUTINE DERDHT(A,B,C)
C THIS ROUTINE REVISOR AND/OR RESEQUENCED ON OCT. 2R, 1968
C
C THIS ROUTINE COMPUTES THE DERIVATIVE OF A DETERMINANT
DIMENSION A(6),B(3,3),C(6,3,3)
DO 4 I=1,6
  A(I)=0
DO 4 J=1,3
  B=MOD(J,3)+1
  4 A(I)=A(I)+C(I,J)*B(B(N),B(N))-B(N,M)*B(M,N)
  1 -C(I,J)*B(B(M),B(M))-B(M,N)*B(N,J)
  2 -B(J,M)*B(M,N)-B(N,M)*B(M,J)
RETURN
END

SUBROUTINE VARIAN(A,B,C,D,E,I)
C THIS ROUTINE REVISOR AND/OR RESEQUENCED ON OCT. 2R, 1968
DIMENSION B(6),C(6),D(6,6),E(6,6,6)
N=II
P=B(1)*E2*D(1,1)+C(1)*E2*B(1,1)*N
DO 1 I=2,6
  F=F+B(1)*E2*D(I,1)+C(I)*E2*B(I,1)*N
  1 J=I-1
  I F=F+E*B(I)*E(J)+D(I,J)*E2+O(C(1)*E2*B(J)*E(I,J)*N
  2 I(F)*E2,3,3
RETURN
EN*

COMPILE(FLD=C)
SUBROUTINE LBCR(XYZ,PAR,EPAR,NPAR,G,NA,MDECN,ANSTR)
SUBROUTINE TO APPLY THE LIBRATION CORRECTION TO THE POSITION
PARAMETERS, IN PREPARATION FOR CALCULATION OF BOND DISTANCES AND
ANGLES. IT IS ASSUMED THAT THE CONTRIBUTIONS TO THE ERRORS IN
DISTANCES AND ANGLES DUE TO THE ERRORS IN DETERMINATION OF THE
LIBRATION PARAMETERS IS NEGLECTABLE COMPARED WITH THE ERRORS IN
THE DETERMINATION OF THE POSITION PARAMETERS.
C
C LIBRATION PARAMETERS ARE:
  12(K)=FLD(9,K)
  OFFINE 12(K)=FLD(9,K)
  DEFINE 13(K)=FLD(18,9,K)
  DFFINE 14(K)=FLD(27,9,K)
  DIMENSION XYZ(3,6),PAR(60),EPAR(60),C(3,3),ANSTR(MDECN),ATGX(6)
  1,XTGA(G),RC(13),R(3),BL(3,3),XYZI(3),SYZ(3),LI(6)
  COMPUTE TRANSFORMATION FROM CRYSTAL TO ORTHORHOMAL AND BACK.
  ATGX(1)=SORT(G(1,1))
  ATGX(5)=C(1,2)/ATGX(1)
  ATGX(4)=C(1,3)/ATGX(1)
  ATGX(6)=SORT(G(2,2))-ATGX(2)*E2
  ATGX(5)=(C(2,3)-ATGX(2)*ATGX(3))/ATGX(4)
  XTGA(6)=1./ATGX(4)
  XTGA(4)=1./ATGX(4)
  XTGA(6)=1./ATGX(6)
  XTGX(2)=-ATGX(2)/ATGX(4)
  XTGX(3)=-ATGX(3)/ATGX(4)
  XTGA(3)=(ATGX(2)*ATGX(5)+ATGX(3)*ATGX(3))/ATGX(4)
  DETERMINE WHETHER ANY SPECIAL PARAMETERS ARE LIBRATION ELEMENTS.
  IBRT=99
  IST=1
  50 DO 100 I=1,NPAR
    IF(I*(EPAR(1)),RO,1-AND,(14*(EPAR(1)),OB,-16,AND,14*(EPAR(1)),LE,21)
    1.,AND,12*(EPAR(1)),NE,ISBT) GO TO 110
    100 CONTINUE
  C THERE IS AT LEAST 1 SET OF LIBRATION ELEMENTS, FIND THE MEMBERS OF
  THE SET AND FILL THEM IN.
  C
  110 ISBT=12*(EPAR(1))
  OXYZ(J)=0.
  DO 120 J=1,3
    OXYZ(J)=0.
  120 EL(J,K)=0.
  I=130, J=1, NPAR
  IF(12*(EPAR(J)),NE,ISBT,EP,11*(EPAR(J)),NR,1) GO TO 130
  IDRN=14*(EPAR(J))
  IF(IDRN,GE,1-AND,IDEN,LB,3)GO TO 124
  IF(IDRN,CE,16-AND,IDEN,LB,21)GO TO 126
  GO TO 130
  124 OXYZ(IDEN)=PAR(J)
  GO TO 130
  126 IF(IDRN,LE,15)
    EL(IDEN, IDEN)=PAR(J)
    GO TO 129
  128 JJ=1
    128 JJ=1
  EN*3
LBCR 10
LBCR 20
LBCR 30
LBCR 40
LBCR 50
LBCR 60
LBCR 70
LBCR 80
LBCR 90
LBCR 100
LBCR 110
LBCR 120
LBCR 130
LBCR 140
LBCR 150
LBCR 160
LBCR 170
LBCR 180
LBCR 190
LBCR 200
LBCR 210
LBCR 220
LBCR 230
LBCR 240
LBCR 250
LBCR 260
LBCR 270
LBCR 280
LBCR 290
LBCR 300
LBCR 310
LBCR 320
LBCR 330
LBCR 340
LBCR 350
LBCR 360
LBCR 370
LBCR 380
LBCR 390
LBCR 400
LBCR 410
LBCR 420
LBCR 430
LBCR 440
LBCR 450
LBCR 460
LBCR 470
LBCR 480
LBCR 490
LBCR 500
LBCR 510
LBCR 520
LBCR 530
LBCR 540
LBCR 550
LBCR 560
LBCR 570

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DERD 10
DERD 20
DERD 30
DERD 40
DERD 50
DERD 60
DERD 70
DERD 80
DERD 90
DERD 100
DERD 110
DERD 120
DERD 130
DERD 140
DERD 150
DERD 160
DERD 170
DERD 180

VARN 10
VARN 20
VARN 30
VARN 40
VARN 50
VARN 60
VARN 70
VARN 80
VARN 90
VARN 100
VARN 110
VARN 120
VARN 130
VARN 140
VARN 150
VARN 160
VARN 170
VARN 180

SUBROUTINE DERDHT(A,B,C)
C THIS ROUTINE REVISOR AND/OR RESEQUENCED ON OCT. 2R, 1968
C
C THIS ROUTINE COMPUTES THE DERIVATIVE OF A DETERMINANT
DIMENSION A(6),B(3,3),C(6,3,3)
DO 4 I=1,6
  A(I)=0
DO 4 J=1,3
  B=MOD(J,3)+1
  4 A(I)=A(I)+C(I,J)*B(B(N),B(N))-B(N,M)*B(M,N)
  1 -C(I,J)*B(B(M),B(M))-B(M,N)*B(N,J)
  2 -B(J,M)*B(M,N)-B(N,M)*B(M,J)
RETURN
END

SUBROUTINE VARIAN(A,B,C,D,E,I)
C THIS ROUTINE REVISOR AND/OR RESEQUENCED ON OCT. 2R, 1968
DIMENSION B(6),C(6),D(6,6),E(6,6,6)
N=II
P=B(1)*E2*D(1,1)+C(1)*E2*B(1,1)*N
DO 1 I=2,6
  F=F+B(1)*E2*D(I,1)+C(I)*E2*B(I,1)*N
  1 J=I-1
  I F=F+E*B(I)*E(J)+D(I,J)*E2+O(C(1)*E2*B(J)*E(I,J)*N
  2 I(F)*E2,3,3
RETURN
EN*

LBCR 10
LBCR 20
LBCR 30
LBCR 40
LBCR 50
LBCR 60
LBCR 70
LBCR 80
LBCR 90
LBCR 100
LBCR 110
LBCR 120
LBCR 130
LBCR 140
LBCR 150
LBCR 160
LBCR 170
LBCR 180
LBCR 190
LBCR 200
LBCR 210
LBCR 220
LBCR 230
LBCR 240
LBCR 250
LBCR 260
LBCR 270
LBCR 280
LBCR 290
LBCR 300
LBCR 310
LBCR 320
LBCR 330
LBCR 340
LBCR 350
LBCR 360
LBCR 370
LBCR 380
LBCR 390
LBCR 400
LBCR 410
LBCR 420
LBCR 430
LBCR 440
LBCR 450
LBCR 460
LBCR 470
LBCR 480
LBCR 490
LBCR 500
LBCR 510
LBCR 520
LBCR 530
LBCR 540
LBCR 550
LBCR 560
LBCR 570

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00 112 K=1,3
112 IHKK)=RMAT(J,K,I)
CALL SECT1(SECT,INH)
00 113 K=1,3
113 (RMAT(J,K,I)=IHKK)
MAXREFL=0
00 120 I=1,6
120 JEXTR(I)=0
INDEX=1
NREFL=0
NFR=1000
IF (LSPC=0) GO TO 125
IF (LSPC=1) SPACE THE MAP
LSPC=1SPC
GO TO 130
C
C 125 SINGLE SPACE THE MAP
125 LSPC=IBNK
C
C 130 REAR REFLECTION DATA
NFR=NFR+10
JF(NFR=500) 150,140,140
JF(NFR=100) 130,130,130
FORS=FRUF(NFR+4)
JF(IH(1)=59) 160,600,160
NFR=0
IH(1)=IFRUF(NFR+1)
IH(2)=IFRUF(NFR+2)
IH(3)=IFRUF(NFR+3)
FORS=FRUF(NFR+4)
JF(IH(1)=59) 160,600,160
NFR=0
CHECK P REJECTED
NFR=NFR+10,170,180,170
170 IF (KSEJ) 130,180,130
REFLECTION NOT REJECTED
180 NREFL=NREFL+1
JF(NREFL=MAXREFL) 200,200,190
EXPANO MAXIMUM SIZE
190 MAXREFL=MAXREFL+100
CALL CORSZ(ARRAY3+MAXREFL)
200 IF (NREFL=200,220,210)
IF (NREFL=200,220,210)
FORS=FORS+FRUF(NFR+5)
CALCULATE PHASE ANGLE
220 IF (ICENT) 230,225,230
225 FRUF(NFR+7)=0
230 ARRAY(INDEX-1)=ATAN2(FRUF(NFR+7),FRUF(NFR+6))
C
C 280 IF (IH(1)) 350,280,350
IF (IH(1)) 350,280,350
EXPANO MAXIMUM SIZE
280 IF (IH(1)) 350,280,350
EXPANO MAXIMUM SIZE
290 IC=2
GO TO 530
300 JF (IH(3)) 320,310,320
GO TO 530
C
C 310 IC=1
GO TO 530
C
C 320 IF (IH(2)) 340,330,340
IF (IH(2)) 340,330,340
EXPANO MAXIMUM SIZE
330 IC=8
UNK REFLECTION
GO TO 530
C
C 340 IC=5
OKL REFLECTION
GO TO 530
350 JF (IH(2)) 410,360,410
360 JF (IH(3)) 380,370,380
HOO REFLECTION
370 IC=1
GO TO 530
380 JF (IH(1)-IH(3)) 400,390,400
HOM REFLECTION
390 IC=7
GO TO 530
C
C 400 IC=4
HOL REFLECT(UN
GO TO 530
410 JF (IH(3)) 450,420,450
420 JF (IH(1)-IH(2)) 440,430,440
HHO REFLECTION
430 IC=6
GO TO 530
C
C 440 IC=3
HKO REFLECTION
GO TO 530
450 JF (IH(1)-IH(2)) 490,460,490
460 JF (IH(1)-IH(3)) 480,470,480
HHH REFLECTION
470 IC=9
GO TO 530
C
C 480 IC=10
HML REFLECTION
GO TO 530
490 JF (IH(2)-IH(3)) 510,500,510
HKK OR HKH REFLECTION
500 IC=11
GO TO 530
510 JF (IH(1)-IH(3)) 520,500,520
HKL REFLECTION
520 IC=12
HKL REFLECTION
530 ARRAY(INDEX-2)=EXPAGCFMUL(I,C)+FORS
ARRAY(INDEX-3)=I*(IH(1)*256*(IH(2)))+256*(IH(3))+6579300
C
C 540 JH(J)=JH(I)+HMAT(K,J,I)*IH(K)
JH(J)=0
00 540 J=1,3
JH(J)=0
540 JH(J)=JH(I)+HMAT(K,J,I)*IH(K)
JH(J)=0
JF (JH(J)-IEXTR(L)) 570,570,560
SET NEW MAXIMUM
560 IEXTR(L)=JH(L)
GO TO 590
570 JF (JH(J)-IEXTR(L)*3) 580,590,590
SET NEW MINIMUM
580 IEXTR(L)*3)=JH(J)
590 CONTINUE
GO TO 600
C
C 600 JARRAY(INDEX)=0
FOUR 580
FOUR 590
FOUR 610
FOUR 620
FOUR 630
FOUR 640
FOUR 650
FOUR 660
FOUR 670
FOUR 680
FOUR 690
FOUR 700
FOUR 710
FOUR 720
FOUR 730
FOUR 740
FOUR 750
FOUR 760
FOUR 770
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FOUR 1080
FOUR 1090
FOUR 1100
FOUR 1110
FOUR 1120
FOUR 1130
FOUR 1140
FOUR 1150
FOUR 1160
FOUR 1170
FOUR 1180
FOUR 1190
FOUR 1200
FOUR 1210
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FOUR 1280
FOUR 1290
FOUR 1300
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FOUR 1360
FOUR 1370
FOUR 1380
FOUR 1390
FOUR 1400
FOUR 1410
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FOUR 1470
FOUR 1480
FOUR 1490
FOUR 1500
FOUR 1510
FOUR 1520
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FOUR 1570
FOUR 1580
FOUR 1590
FOUR 1600
FOUR 1610
FOUR 1620
FOUR 1630
FOUR 1640
FOUR 1650
FOUR 1660
FOUR 1670
FOUR 1680
FOUR 1690
FOUR 1700
FOUR 1710
FOUR 1720
FOUR 1730

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C      READ SECTION
35  READ(I,SCJ)(BUFF(I),I=1,NUM)
   DO 90 I=1,IZA
   JZC=I+IZI-1
   IZC=JZC
   C      GET Z INTO ACTUAL SET COMPUTED
343  IF(JZC-GE=JZI-ANO-JZC-LE-JZPJGD TO 3 44
   JZC=JZC+1 TO 20
   JZC=JZC-1SIGN(IZ,JZC)
   GO TO 343
344  IF(JZC-NE-KZCJGD TO 90
   JSECT(I+NUMZ)=0
   IYC=IYI
40  IF(IYC-GT-IVFJGD TO 90
   JYC=IYC
   C      Y INTO ACTUAL SET COMPUTED
   SEC=JZC-ANO-JYC-LE-JYFJGD TO 42
41  IF(IJYC-GE=JYI-ANO-JYC-LE-JYFJGD TO 42
   IF(IJYC-NE-0JGD TO 320
   JYC=JYC-1SIGN(IY,JYC)
   GO TO 41
42  INOEX=NUM*(IZC-IZI)+IYA+IVC-IVI+I
   X=A(2)+IVC+A(3)+IZC+A(4)
   J=(JYC-JYI)*JXA-IXI+I
   IWK=I
   JOEX(1)=I-1
   JOEX(2)=I
   JOEX(3)=I+1
   JOEX(4)=I+2
   DO 60 I=1,+4
50  IF(JOEX(I))-GE-IXI-ANO-JOEX(I)-LE-IXFJGD TO 60
   IF(IJYC-NE-0JGD TO 70
   JOEX(I)=JOEX(I)-1SIGN(IX,JOEX(I))
   GO TO 60
60  JOEX(I)=J+JOEX(I)
   AA=-ILINE(IP1)/6+*ILINE(IP2)/2--ILINE(IP3)/2+*ILINE(IP4)/6-
   BB=ILINE(IP1)/2--ILINE(IP2)+*ILINE(IP3)/2-
   CC=-ILINE(IP1)/3--ILINE(IP2)/2+*ILINE(IP3)--ILINE(IP4)/6-
   BUFF(INDEX)=EIAA*FX+BB)*FX+CC)*FX+ILINE(IP2)
   GO TO 80
70  BUFF(INDEX)=IIIIII-
   IJYC=IYC+1
   DO 80 I=1,IZI
   GO TO 90
90  CONTINUE
   C      CHECK IF ANY SECTIONS LEFT TO FIND
   DO 91 I=1,IZA
   IF(JSECT(I+NUMZ))30,91,30
91  CONTINUE
100  N=0
   DO 120 I=1,IYA+30
   I=MIMO30+IYA-I+I
   J=I+IVI-1
   M=0
   DO 105 K=1,L+2
   M=M+I
105  FYIMJ=J+K-1
   WRITE(IOUT,4)TITLE,N,IZO,(FY(K),K=1,N)

```

```

00 120 J=L,IZA
K=NUM*(J-1)+IYA+I
KK=K+L-1
DO 110 M=K,KK
110  LLINE(M-K+1)=BUFF(M)+SIGN(.5,BUFF(M))
IY=J+IZI-1
IY=IY+IYI-1
IF(IY-LE=0JGD TO 15
K=NUM+1
L=1000
WRITE(I,SCJ)IYA,IZA,IZO,L,IX,IXI,IXF,IV,IVF,IZI,IZF
WRITE(I,SCJ)I(BUFF(M)+M=K+NUMZ)
GO TO 15
900  STOP
END

```



```

146 CALL PLOT1146+120+120
STOP
157 FORMAT(20A4,F5.0,15,3F5.0,615,F5.0,215)
158 FORMAT(10A4,F4.0,10,3F4.0,610,F4.0,210)
159 FORMAT(10A4,F4.0,10,3F4.0,610,F4.0,210)
160 FORMAT(11H, 22H NO CONTOURS SPECIFIED)
161 FORMAT(11H, 22H NO CONTOURS SPECIFIED)
162 FORMAT(11H, 22H NO CONTOURS SPECIFIED)
163 FORMAT(11H, 22H NO CONTOURS SPECIFIED)
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174 FORMAT(11H, 22H NO CONTOURS SPECIFIED)
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203 FORMAT(11H, 22H NO CONTOURS SPECIFIED)
204 FORMAT(11H, 22H NO CONTOURS SPECIFIED)
205 FORMAT(11H, 22H NO CONTOURS SPECIFIED)
206 FORMAT(11H, 22H NO CONTOURS SPECIFIED)

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131 CALL PLOT(WK,WY,IPEN)
134 IF INCROSS=LE-0J GO TO 137
00 136 I=1,NCROSS
IF BX(I)-LT-0.01GO TO 137
IF BY(I)-LT-0.01GO TO 137
XX=BY(I)*AAR*CALF+X1
CALL PLOT(XX-SCROSS,YY,3)
CALL PLOT(XX*SCROSS,YY,2)
CALL PLOT(XX,YY-SCROSS,2)
CALL PLOT(XX,YY*SCROSS,2)
136 CONTINUE
137 IF (TLEHT-LE-0.01GO TO 1369
00 1360 I=1,120
CONTINUE
1360 GO TO 1369
1361 I=1,120
CONTINUE
1361 GO TO 1369
TEMP=(I-1)*24.*TLEHT/7.
CALL SYMBOL(TLEHT,TEMP,TLEHT,ATTITLE(I),90.,.4)
TEMP=0.5*TLEHT*(TLEHT-2.*TEMP-TMSECTION,90.-7)
CALL SYMBOL(TLEHT,TEMP,TLEHT,ATTITLE(I),90.,.4)
1369 IF (NLAB-ED-0JGO TO 1371
CALL SYMBOL(TLEHT,TEMP,TLEHT,ATTITLE(I),90.,.4)
C
00 1370 I=1,NLAB
READ(I,N,178)WK,WY,OK,OY,TEMP,LABL
XX=WX*PB+MY*AAR*CALF+X1+OX
YY=MY*PB+SALF+Y1+OY
CALL SYMBOL(XX,YY,TEMP,LABL,90.,.6)
1371 I=1,NLAB
CONTINUE
1371 GO TO 1369
138 GRFG=AMIN1(SREG(I),SLIM(I))
CLIM=AMAX1(SREG(I),SLIM(I))
ACSTEP=AMAX1(LI,ABS(GSTEP))
IF (CBEG-GT,BMAX,OR,CLIM-LT,BMIN) GO TO 142
0=CBEG+ACSTEP
IF (CGGT-CLIM) GO TO 140
BREG=0
GO TO 139
140 IF (CLIM-LE,BMAX) GO TO 141
0=CLIM-ACSTEP
IF (O-LE-CBEG) GO TO 141
CLIM=0
GO TO 140
141 ICG=1
GO TO 140
NOL=NS/ICG(I)
IF (ICGT-LE,NCOL,OR,NSO,NCUSO,CBEG,CLIM,ACSTEP)
GO TO 143
142 WRITE(IOUT,176) CBEG,CLIM,BMIN,BMAX
143 IF (I-LE,NCNT) GO TO 138
IF (ICG-GT-0J GO TO 144
WRITE(IOUT,177)
144 CALL PLOT(XFIN,0.,-3)

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C
146 CALL PLOT1146+120+120
STOP
157 FORMAT(20A4,F5.0,15,3F5.0,615,F5.0,215)
158 FORMAT(10A4,F4.0,10,3F4.0,610,F4.0,210)
159 FORMAT(10A4,F4.0,10,3F4.0,610,F4.0,210)
160 FORMAT(11H, 22H NO CONTOURS SPECIFIED)
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204 FORMAT(11H, 22H NO CONTOURS SPECIFIED)
205 FORMAT(11H, 22H NO CONTOURS SPECIFIED)
206 FORMAT(11H, 22H NO CONTOURS SPECIFIED)

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CPLT 580
CPLT 590
CPLT 600
CPLT 610
CPLT 620
CPLT 630
CPLT 640
CPLT 650
CPLT 660
CPLT 670
CPLT 680
CPLT 690
CPLT 700
CPLT 710
CPLT 720
CPLT 730
CPLT 740
CPLT 750
CPLT 760
CPLT 770
CPLT 780
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CPLT 970
CPLT 980
CPLT 990
CPLT1000
CPLT1010
CPLT1020
CPLT1030
CPLT1040
CPLT1050
CPLT1060
CPLT1070
CPLT1080
CPLT1090
CPLT1100
CPLT1110
CPLT1120
CPLT1130
CPLT1140
CPLT1150

VA=XAI(1)
VB=YA(1)
J=1
UD 115 I=2,ICOUNT
IF (ABS(XAI(1))-VA(1-GT-JA)) GO TO 114
IF (ABS(XAI(1))-VB(1-GT-JB)) GO TO 114
GO TO 115
J=J+1
114
VA=XAI(1)
VB=YA(1)
XA(J)=VA
YB(J)=VB
YA(J)=VB
115 CONTINUE
XAI(J)=XAI(ICOUNT)
YAI(J)=YAI(ICOUNT)
VK(J)=VK(ICOUNT)
VY(J)=VY(ICOUNT)
IN=J
IF (IN-GT-2) CALL PREPLT
XAI(1)=XAI(ICOUNT)
YAI(1)=YAI(ICOUNT)
ICOUNT=1
GO TO (102,104,1050,123),IRET
116
VY(1)=YAI(2)-YAI(1)*JUNIT
VX(ICOUNT)=(XAI(ICOUNT)-XAI(ICOUNT-1))*JUNIT
VY(ICOUNT)=(YAI(ICOUNT)-YAI(ICOUNT-1))*JUNIT
GO TO 113
117 IF (ISAVE.NE.ICOUNT) GO TO 118
GO TO (102,104,1050,123),IRET
118 LOG4=0
X=ABS(XAI(1))-XAI(ISAVE+1)
Y=ABS(YAI(1))-YAI(ISAVE+1)
IF (X+Y.GT-4*Y1.GT-1.E-4) GO TO 122
IF (ISAVE/2
K=ISAVE
K=1+AVE
00 119 J=1,1
X=XAI(J)
XAI(J)=XAI(K)
XAI(K)=X
Y=YAI(J)
YAI(K)=Y
YAI(J)=YAI(K)
YAI(K)=Y
119 K=K-1
ICOUNT=ICOUNT-1
K=ISAVE+1
120 00 121 J=ISAVE,ICOUNT
XAI(J)=XAI(K)
YAI(J)=YAI(K)
121 K=K+1
ISAVE=0
K=ISAVE+6
122 K=K-1,IRET
KCOUNT=ICOUNT
KSAVE=ISAVE
ICOUNT=KSAVE
IRET=4
GO TO 116

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CPLT 10
CPLT 20
CPLT 30
CPLT 40
CPLT 50
CPLT 60
CPLT 70
CPLT 80
CPLT 90
CPLT 100
CPLT 110
CPLT 120
CPLT 130
CPLT 140
CPLT 150
CPLT 160
CPLT 170
CPLT 180
CPLT 190
CPLT 200
CPLT 210
CPLT 220
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CPLT 460
CPLT 470
CPLT 480
CPLT 490
CPLT 500
CPLT 510
CPLT 520
CPLT 530
CPLT 540
CPLT 550
CPLT 560
CPLT 570

SUBROUTINE CPLOT (IPLOT,ROB,COL,LEVEL)
COMMON /81/ A,B,ALF,NA,NB,AA,AB,AA*,AY,AF, BF,X1,X2,Y1,Y2,CALF,SALF
1 ATTITLE(20)
COMMON /PLOT/ ITOT,IN,IP,IT,NT,UNIT,LOG1,LOG2,L,LOG3,LOG4,ICOUNT,NCOCPLT
UNIT,XO1,G
X1=XCOL,ROB+ROB*AA+CALF*X1
X2=XCOL,ROB+ROB*AA+CALF*X1
Y1=YROW,AA+SALF*Y1
IF (IPLOT-1) 101,103,106
101 IF (ICOUNT.LE.1) GO TO 102
IRET=1
GO TO 107
102 IF (LOG4.EQ.1) GO TO 103
ICOUNT=0
IF (ICOUNT.LT.NCOUNT) GO TO 104
IRET=5
GO TO 107
104 ICOUNT=ICOUNT+1
XAI(ICOUNT)=XXX
YAI(ICOUNT)=YYY
C
C
NOTE INTERCHANGE OF X AND Y
1050 RETURN
IF (NOT(CE.OJCALL NUMBER(XXX,YYY,1,LEVEL,90.0,NOIG))
RETURN
106 IRET=3
IF (LOG4.EQ.1) GO TO 118
107 IF (LOG4.EQ.1) GO TO 117
X=ABS(XAI(1))-XAI(ICOUNT)
Y=ABS(YAI(1))-YAI(ICOUNT)
IF (X+Y.GT-4*Y1.GT-1.E-6) GO TO 112
LOG3=0
Y=YAI(1)
Y=YAI(1)
108 BY=Y-Y1
IF (AMIN(LABS(8Y1),ABS(Y-Y2))-L.E.-4) GO TO 110
BY=BY+CALF/SALF
IF (AMIN(LABS(X-X1)-BY),ABS(X-X2-BY))-L.E.-4) GO TO 110
IF (LOG3.GT.0) GO TO 116
LOG3=1
X=XAI(ICOUNT)
Y=YAI(ICOUNT)
GO TO 108
110 IF (LOG3.EQ.2) GO TO 116
IF (LOG3.EQ.1) GO TO 111
LOG3=2
GO TO 109
111 LOG4=1
ISAVE=ICOUNT
IF (LOG2.EQ.1050,123),IRET
112 VX(ICOUNT)=(XAI(2)-XAI(ICOUNT-1))*0.5*JUNIT
VY(1)=VY(ICOUNT)
VY(ICOUNT)=(YAI(2)-YAI(ICOUNT-1))*0.5*JUNIT
113 UA=AA*JUNIT*0.7
UB=BB*JUNIT*0.7

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C      ICNT 580
C      ICNT 590
C      ICNT 600
C      ICNT 610
C      ICNT 620
C      ICNT 630
C      ICNT 640
C      ICNT 650
C      ICNT 660
C      ICNT 670
C      ICNT 680
C      ICNT 690
C      ICNT 700
C      ICNT 710
C      ICNT 720
C      ICNT 730
C      ICNT 740
C      ICNT 750
C      ICNT 760
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C      ICNT 950
C      ICNT 960
C      ICNT 970
C      ICNT 980
C      ICNT 990
C      ICNT1000
C      ICNT1010
C      ICNT1020
C      ICNT1030
C      ICNT1040
C      ICNT1050
C      ICNT1060
C      ICNT1070
C      ICNT1080
C      ICNT1090
C      ICNT1100
C      ICNT1110
C      ICNT1120
C      ICNT1130
C      ICNT1140
C      ICNT1150

C      THE LEAST SIGNIFICANT BIT OF DATA(I) IS USED TO MARK THE LEFTHAND
C      EDGE OF THE COUNTER WHEN IT CROSSES THAT ROW.
C      SEARCH SCANS THE ROWS FROM LEFT TO RIGHT, AND BOTTOM TO TOP.
C      LOOKING FOR THE FIRST POINT ON THE XLEV COUNTER.
C
103 IUP=JUP
    ILOOP=JLOOP
    RT=1
    IF (IX-MAXX) I04,I13,I212
    IJUMP=0
    IF (IX-MAXX) I04,I13,I212
104 L=1+NR0M*(IY-1)
    IY,IY AFTER THE LAST POINT THAT WAS SEARCHED, TO RESTART THE
    SEARCH AFTER FINISHING THE CURRENT COUNTER LINE.
C
105 OIA1=OATAIL)
    OJAI=UNMARK(OIA1)
    IF (OJAI-XLEV) I06,I116,I106
106 IF (IX-1) I213,I07,I116
107 IF (IY-1) I214,I112,I108
108 LMX=L-NR0M*(IX)
    OI2=UNMARK(OJAI2)
109 IF (OI2-XLEV) I11,I109,I111
110 YPT=IY-1
    GO TO I15
111 IF (IY-MAXY) I12,I116,I215
C
C      LOOKING FOR AN INTERSECTION IN THE LEFT-HAND COLUMN BEFORE
C      SCANNING FOR INTERSECTIONS IN THE CURRENT ROW.
C
112 LPX=L-NR0M
    OI0=UNMARK(OIATLPXI)
113 IF (OI0-XLEV) I13,I116,I113
    IF (OI0-XLEV)*(OJAI-XLEV) I14,I114,I116
C
C      ARE BOTH OI0 AND OJAI ON THE SAME SIDE OF THE COUNTER
C
114 OEL=OIF(OJAI)
    IF (OEL-OI0) I15,I115
    XPT=FOIAT(IY)I4XLEV-OJAI/I/OEL
115 XPT=L
    XI=XPT
    YI=YPT
    ILOOP=0
    IF (OI0-DATA(LPX)) I130,I138,I130
C
C      IF TWO ROWS ARE EACH FILLED WITH HIGH AND LOW NUMBERS RESPECTIVELY,ICNT1070
C      GO TO 207
C      IF TWO ROWS ARE EACH FILLED WITH HIGH AND LOW NUMBERS RESPECTIVELY,ICNT1080
C      GO TO 207
C
116 OIA2=DATA(I+1)
    OJAI2=UNMARK(OIA2)
117 IF (OIA1-OJAI) I130,I117,I130
118 IF (OJAI-XLEV) I29,I118,I128
119 XPT=IX
    IJUP=ILOOP

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ICNT1160
ICNT1170
ICNT1180
ICNT1190
ICNT1200
ICNT1210
ICNT1220
ICNT1230
ICNT1240
ICNT1250
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ICNT1290
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ICNT1390
ICNT1400
ICNT1410
ICNT1420
ICNT1430
ICNT1440
ICNT1450
ICNT1460
ICNT1470
ICNT1480
ICNT1490
ICNT1500
ICNT1510
ICNT1520
ICNT1530
ICNT1540
ICNT1550
ICNT1560
ICNT1570
ICNT1580
ICNT1590
ICNT1600
ICNT1610
ICNT1620
ICNT1630
ICNT1640
ICNT1650
ICNT1660
ICNT1670
ICNT1680
ICNT1690
ICNT1700
ICNT1710
ICNT1720
ICNT1730

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```

C      IF IIX-1) 216,I20,I137
C      ILOOP=0
C      GO TO 137
C      I21 IF (IIX-MAXX+1) I30,I22,I22
C      I22 IF (IYY-1) I217,I30,I123
C
C      FINING THE LOWER OR UPPER CORNER OF A PLATEAU THAT HITS THE
C      RIGHT EDGE.
C
123 IF (OJAI2-OJAI2) I31,I26,I131
124 L=L+1-NR0M
    LMX=L-NR0M
    OIA2=UNMARK(OIATLPXI)
    OJAI2=UNMARK(OIATLIMXI)
    IF (OJAI2-XLEV) I25,I26,I25
125 IUP=0
    GO TO I27
126 IF (OJAI2-XLEV) I27,I31,I27
C
C      IF BOTH UPPER AND LOWER POINTS ARE ALSO ON, THEN DUMP THIS ONE.
C
127 IRT=0
    ILOOP=0
    XPT=MAXX
    XI=XPT
    GO TO I37
C
C      SKIPS ANY BLOCK OF ALL XLEV
C      FOR 1ST POINT GREATER THAN XLEV
C
128 IF (XLEV-OJAI2) I30,I30,I36
C
C      FOR 1ST POINT LESS THAN XLEV
C
129 IF (XLEV-OJAI2) I36,I30,I30
C
C      OMTS ANY RIGHT HAND EDGE COLUMN OF ALL XLEV
C
130 IF (IIX-MAXX+1) I35,I31,I31
C
C      IF IX = MAXX-1 WE JUST SCANNED THE LAST COLUMN-GAP...MUST SWITCH
C      ROWS.
C
131 IF (IYY-MAXY) I33,I32,I218
C
C      IF IY = MAXY, WE ARE AT THE TOP ROW ALSO AND COUNTERING IS DONE.
C
132 IJUMP=1
    GO TO 207
133 IY=1
    IY=IY+1
    L=IX+NR0M*(IY-1)
    IF (IYY-MAXY) I05,I134,I219
134 JLOOP=0
    IJUP=ILOOP

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```

175 IF (IXPT+IRT-MAXX) 172,172,176
176 IDENT=IDENT+2
GO TO 171
C
C Y-LIMIT CHECK
C
177 IF (IYPT+IUP-2) 173,172,178
178 IF (IYPT+IUP-MAXY) 172,172,173
179 XPT=IXA
YPT=IYA
GO TO 194
180 XPT=IX8
YPT=IY8
GO TO 194
181 XPT=IXC
YPT=IYC
IF (IDENT) 182,194,194
C
C DON'T CHANGE DIRECTION IF IT'S AN *ON-TO-ON**
C
182 IF (IIND-1) 183,192,183
183 IRT=1-IRT
GO TO 194
184 DEL=DI8-DIA
DEL=DEL-DIC/DEL
IF (IIND-2) 185,186,185
185 XPT=FLOAT(IXA)+DEL*FLOAT(IRT+IRT-1)
YPT=IYA
GO TO 194
186 YPT=FLOAT(IYA)+DEL*FLOAT(IUP+IUP-1)
XPT=IXA
GO TO 194
187 DEL=DI8-DIC
DEL=DEL-DIC/DEL
IF (IIND-2) 188,189,188
188 XPT=FLOAT(IYC)+DEL*FLOAT(IUP+IUP-1)
YPT=IX8
GO TO 194
189 XPT=FLOAT(IXC)+DEL*FLOAT(IRT+IRT-1)
YPT=IY8
GO TO 194
190 XPT=IXA
YPT=IYA
DEL=DEL-DIC/DEL
IF (IIND-2) 191,193,191
191 XPT=FLOAT(IXC)-DEL*FLOAT(IRT+IRT-1)
YPT=IYC
GO TO 194
192 IUP=1-IUP
GO TO 194
193 XPT=FLOAT(IYC)-DEL*FLOAT(IUP+IUP-1)
YPT=IY8
GO TO 183
194 CALL GPLOTT (I,XPT,YPT,XLEV)
C
C PLOTS A LINE TO THIS LOCATION.
C
ICNT3480
ICNT3490
ICNT3500
ICNT3510
ICNT3520
ICNT3530
ICNT3540
ICNT3550
ICNT3560
ICNT3570
ICNT3580
ICNT3590
ICNT3600
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ICNT3950
ICNT3960
ICNT3970
ICNT3980
ICNT3990
ICNT4000
ICNT4010
ICNT4020
ICNT4030
ICNT4040
ICNT4050

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IF (ILOOP=3) 195,204,206
195 IYI=YPT
IYI=IF(XPT)*ROWD*(IYPT-1)
IF(ABS(IYPT-FLOAT(IYPT))-0.01)196,196,198
C
C IF YPT IS AN INTEGER, MARK THE POINT IMMEDIATELY TO THE LEFT. IF IT IS ALREADY MARKED, THIS HAS BEEN PLOTTED BEFORE.
C
196 IF(DATA(I)-UNMARK(DATA(I)))202,197,202
C
C IF THIS POINT HAS BEEN TRAVELED BEFORE...
C
197 DATA(I)=MARK(DATA(I))
C
C IF NOT, KEYS THIS POINT FOR FUTURE REFERENCE.
C
198 IF(XPT-1,0)221,2040,199
199 IF (XPT-FLOAT(MAXX)) 200,204,222
200 IF (IYPT-1,1) 223,204,201
201 IF (IYPT-FLOAT(MAXY)) 141,204,224
202 IF (XPT-XI) 204,203,204
203 IF (IYPT-YI) 204,206,204
C
C IF CONTOUR HAS COME FULL CIRCLE, THAT'S ALL...
C
2040 DATA(I)=MARK(DATA(I))
204 IF (ILOOP-1) 206,205,206
C
C IF THE CONTOUR HITS EITHER ANY EDGE OR (ITSELF IN THE MIDDLE), IT RETURNS ONCE TO THE STARTING POINT AND BEGINS CONTOURING IN THE OTHER DIRECTION. (IF THE STARTING POINT IS ON AN EDGE, IT'S THE END OF THE CONTOUR LINE.
C
205 IRT=0
IUP=0
ILOOP=2
XPT=XI
YPT=YI
CALL GPLOTT (0,XPT,YPT,XLEV)
C
C MOVES THE PEN BACK TO STARTING POINT WITHOUT PLOTTING.
C
GO TO 141
C
206 CALL GPLOTT (2,XPT,YPT,XLEV)
C
C TO NUMBER EACH SECTION OF A CONTOUR
C
GO TO 103
C
ILOOP=0, MORE TO CONTOUR...1, END OF MAP, NO MORE...
3, ONE-POINT CONTOUR.
C
207 IF (ICSTP) 208,210,208
208 IF (ICTR+GSTP-CLIM)*SIGN1.*SIGN1.*GSTP) 209,209,210
209 CTR=CTR+GSTP
GO TO 101
210 CALL GPLOTT (0,0,0,0,0.)

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C      MAKE SURE ALL POINTS HAVE BEEN PLOTTED
C      RETURN
C      TRAPS TO OUTPUT A WARNING IF ANY BOUNDARY IS CROSSED.
C      STOP
211  WRITE(6,226)IT,IX,MAXX,IY,MAXY,XPT,YPT
212  WRITE(6,226) IT,IX,MAXX,IY,MAXY
    GO TO 131
213  WRITE(6,226) IT,IX,MAXX,IY,MAXY
    GO TO 116
214  IT=I05
    WRITE(6,226) IT,IX,MAXX,IY,MAXY
    GO TO 111
215  IT=I09
    WRITE(6,226) IT,IX,MAXX,IY,MAXY
    GO TO 116
216  WRITE(6,226) IT,IX,MAXX,IY,MAXY
    GO TO 137
217  IT=I19
    WRITE(6,226) IT,IX,MAXX,IY,MAXY
    GO TO 123
218  IT=I28
    WRITE(6,226) IT,IX,MAXX,IY,MAXY
    GO TO 132
219  IT=I30
    WRITE(6,226) IT,IX,MAXX,IY,MAXY
    GO TO 105
220  IT=I35
    WRITE(6,226) IT,IX,MAXX,IY,MAXY
    GO TO 140
221  IT=I303
    GO TO 211
222  IT=I305
    GO TO 211
223  IT=I305
    GO TO 211
224  IT=I306
    GO TO 211
C      226  FORMAT(I,X,5I6,2F10.3)
C      FUNCTION UNMARK(I)
      DATA MASK/077777777777/
      UNMARK=AND(I,MASK)
      RETURN
      REAL FUNCTION MARK(I)
      MARK=OR(I,1)
      RETURN
      ENDO

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ICNT4060
ICNT4070
ICNT4080
ICNT4090
ICNT4100
ICNT4110
ICNT4120
ICNT4130
ICNT4140
ICNT4150
ICNT4160
ICNT4170
ICNT4180
ICNT4190
ICNT4200
ICNT4210
ICNT4220
ICNT4230
ICNT4240
ICNT4250
ICNT4260
ICNT4270
ICNT4280
ICNT4290
ICNT4300
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ICNT4320
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ICNT4370
ICNT4380
ICNT4390
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ICNT4550
ICNT4560
ICNT4570
ICNT4580
ICNT4590
ICNT4600

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SUBROUTINE INTPLT
C      USING RATIONAL POLYN. SPLINE INT. OF 0 V AHUJA 1 8 M SYST J 1968
C      P.208-217
C      DIMENS(CON,X(400),Y(400)
COMMON /PLT2/ C(400),XA(400),YA(400),VX(400),VY(400)
COMMON /PLT1/ ITOT,IN,NP,IT,NT,U(NT,LOG(6)
EQUIVALENCE (X,XA), (Y,YA)
LOG(6)=400
NT=L0G(6)
ITOT=NI
CA=C(1)
CA=C(1)+I*5
LOG(5)=0
LOG(4)=LOG(5)
LOG(3)=LOG(4)
LOG(2)=LOG(3)
LOG(1)=LOG(2)
DO 101 I=2,ITOT
  CA=C(I)/(I-CA)
101  RETURN
ENTRY PREPLT
NC=IN-2
NV=IN-1
NV=IN
OX=VX(IN)
OO=VY(IN)
OX=C(INC)*I3.*(Y(INV)-Y(NV-2))-OX)
OY=C(INC)*I3.*(Y(INV)-Y(NV-2))-OY)
VY(INV)=OY
NC=NC-1
NV=NV-1
GO 102
102  GO TO I2,N
OX=C(INC)*I3.*(X(INV)-X(NV-2))-OX)
OY=C(INC)*I3.*(Y(INV)-Y(NV-2))-OY)
VY(INV)=OY
NC=NC-1
NV=NV-1
GO 102
102  GO TO I2,N
VX(INV)=OX
VY(INV)=OY
XIG=C(I1)*I3.*(X(I3)-X(I1))-OY-VX(I1)
YIG=C(I1)*I3.*(Y(I3)-Y(I1))-OY-VY(I1)
XIG=X(I1)
YIG=Y(I1)
CALL PLOT(XIG,YIG,C,3)
IC=1
AA9=VX(IC)
AA10=YI(IC)
XIG=X(IC+1)
YIG=Y(IC+1)
YIG=YI(IC+1)
AA9=AA9
AA10=AA10
AA10=YI(IC+1)
AA11=XI(IC+1)
AA12=YI(IC+1)
AA13=XI(IC+1)+AA9+AA10
AA14=YI(IC+1)+AA10+AA11

```

```

INTP 10
INTP 20
INTP 30
INTP 40
INTP 50
INTP 60
INTP 70
INTP 80
INTP 90
INTP 100
INTP 110
INTP 120
INTP 130
INTP 140
INTP 150
INTP 160
INTP 170
INTP 180
INTP 190
INTP 200
INTP 210
INTP 220
INTP 230
INTP 240
INTP 250
INTP 260
INTP 270
INTP 280
INTP 290
INTP 300
INTP 310
INTP 320
INTP 330
INTP 340
INTP 350
INTP 360
INTP 370
INTP 380
INTP 390
INTP 400
INTP 410
INTP 420
INTP 430
INTP 440
INTP 450
INTP 460
INTP 470
INTP 480
INTP 490
INTP 500
INTP 510
INTP 520
INTP 530
INTP 540
INTP 550
INTP 560
INTP 570

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A5=3.*(Y1C-YC1)-A9-A9-AA9
A6=4.*(Y1C-YC1)-A10-A10-AA10
I=1
U=0.
104 U=U+UNIT
WK=(I+I*U+A5)*U+A9)*U+XC
WY=(I+I*U+A6)*U+A10)*U+YC
CALL PLOT(WX,WY,Z)
I=I+1
IF (I+.L.E..NP) GO TO 104
I=I-1
IF (I<1) GO TO 103
RETURN
END

```

C COMMENT CARDS FOR FINGFC
C MBS SEPTEMBER 1971
C THIS PROGRAM IS AN ADAPTION OF THE KEAY 67 PROGRAM LIST FC. IT HAS
C BEEN ALTERED TO STAND ALONE AND READ THE FOURIER OUTPUT TAPES WRITTEN
C REFIN. THE LEAST SQUARES PROGRAM WRITTEN BY L. W. FINGER AT TBB
C GEOPHYSICAL LAB. CARNEGIE INSTITUT OF WASHINGTON.
C THE OUTPUT OF THE PROGRAM HAS BEEN CHANGED SO THAT THE #FHASB IN
C MILLICYLES HAS BEEN REPLACED BY STOMA(FG), SCALED UP BY A FACTOR OF
C 10 TO MAKE IT CONSISTENT WITH FG.
C CARD ONE BACKGROUND IDENTIFICATION, 7-7B ANY TITLE
C CARD TWO
C 14 (11/12/13) FOR K INDEX VARIES (MOST)(NEXT MOST)(LEAST) RAPIDLY
C (CODE TO TELL HOW INPUT DATA ARE SORTED)
C 15 SORTING FREQUENCY FOR K INDEX
C 16 SORTING FREQUENCY FOR L INDEX
C (NOTE THAT SUM AND PRODUCT OF NUMBERS IN COLUMNS 1,15, AND 16 MUST
C EQUAL 6)
C 17-20 NUMBER OF LINES PER -LISTFC- PAGE
C 21-24 NUMBER OF LINES PER (COLUMNS) ARGUMENT (DO NOT INTERMEDIATELY
C AS EVEN AS POSSIBLE AS EVEN AS POSSIBLE
C 22-24 NUMBER OF LIST COLUMNS PER -LISTFC- PAGE
C NOTE THE PRODUCT OF THE NUMBER OF LINES AND THE NUMBER OF COLUMNS
C -LISTFC- PAGE CANNOT EXCEED 3000. THAT IS, NO MORE THAN 3000 FOR
C TOTAL OF REFLECTIONS AND READINGS (WITH THEIR SPACES), FOR PAGE.
C ZERO (OR BLANK) IN ANY OF THE FIVE FOLLOWING FIELDS MEANS JUST
C 26 NUMBER OF BLANK PRINT COLUMNS BEFORE THE LISTFC COLUMN
C 27 NUMBER OF BLANK PRINT COLUMNS AFTER THE LISTFC COLUMN
C 30 NUMBER OF PRINT COLUMNS FOR PG TIMES 10
C 32 NUMBER OF PRINT COLUMNS FOR FC TIMES 10
C 34 NUMBER OF PRINT COLUMNS FOR SIDE0 TIMES 10
C 36 SPECIAL FLAG FOR LESS THAN*(BLANK = *)*(JC0DB = 2)
C 38 SPECIAL FLAG FOR EXTRACT*(BLANK = B)*(JC0DE = 3)
C 40 SPECIAL FLAG FOR SPECIAL REFLECTION (JC0DE=4)
C THE NEXT NINE FIELDS ARE (BLANK)/(1) FOR (DO NOT)/(DO)
C 42 PRINT SYMBOL FOR LESS THAN OR EXTRACT REFLECTIONS
C 43 THE NUMBER OF LINES PER ONE PRINT COLUMN
C 44 FOR CHEMICAL STRUCTURES, ATTACH SIGN OF A FC.
C 46 DOUBLE SPACE THE LINES.
C 48 RESTORE EACH -LISTFC- PAGE TO BE THE TOP OF A PRINTER PAGE
C 50 PRINT CURRENT-TITLE* AT TOP OF EACH PRINTER PAGE
C 52 PUNCH A SET OF -FCARD-CARDS (HAS H.K.L.F.G.F.C.A.B.J.C0DB, AND
C LEVEL INDICATORS)
C 56 PRINT MINUS SIGN ON THE PG OF THE REFLECTIONS WHICH ARE LEBTS
C 58 WRITE A SEPARATE COPY OF THE FC LIST ON TAPB A
C 62 NUMBER OF LINES PER PAGE OF ALL COLUMNS
C 64 (11/12/13) FOR HEADINGS SEPARATE FROM BLANK LINES/1 BLANK
C LINE ABOVE/(1) ABOVE AND 1 BELOW) (BLANK = 3)
C 65-72 FACTOR F'S ARE TO BE MULTIPLIED BY, BLANK = 10
C 73-80 FACTOR SIG(PG) IS TO BE MULTIPLIED BY, BLANK = 10
C AS PRESENTLY WRITTEN, THE PROGRAM WILL NOT READ F VALUES FROM
C BUT THIS CAN EASILY BE ARRANGED BY MAKING A USBD SPECIFIC
C OF SUBROUTINE FINGC
C
C C---VERSION AND UPDATING ESTABLISHED 1 JUN 69
C ALTERATIONS MADE AS FOLLOWS... 20 JUN 69, 23 SEP 69

C-----CHECK IF OUTPUT OMS ON TWO SEPARATE FILES
 95 CONTINUE IF (ITWOT) 99,99,95
 C-----MAKE SURE THEY ARE NOT THE SAME
 96 IF (NTRUM-TAPED) 96,97,98
 97 CONTINUE
 100 FORMAT(22OUTOUT AND NPILED ARE THE SAME, REQUEST FOR SPECIAL OUTPUT) LSTP1240
 LSTP1250
 LSTP1260
 LSTP1270
 LSTP1280
 LSTP1290
 LSTP1300
 LSTP1310
 LSTP1320
 LSTP1330
 LSTP1340
 LSTP1350
 LSTP1360
 LSTP1370
 LSTP1380
 LSTP1390
 LSTP1400
 LSTP1410
 LSTP1420
 LSTP1430
 LSTP1440
 LSTP1450
 LSTP1460
 LSTP1470
 LSTP1480
 LSTP1490
 LSTP1500
 LSTP1510
 LSTP1520
 LSTP1530
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 LSTP1560
 LSTP1570
 LSTP1580
 LSTP1590
 LSTP1600
 LSTP1610
 LSTP1620
 LSTP1630
 LSTP1640
 LSTP1650
 LSTP1660
 LSTP1670
 LSTP1680
 LSTP1690
 LSTP1700
 LSTP1710
 LSTP1720
 LSTP1730

C-----CALCULATE THE STORAGE REQUIRED FOR THE LINES AND COLUMNS REQUESTED
 102 IF (MATRIX-ITWTR) 102,401,401
 103 CONTINUE
 C-----INITIALIZE COUNTS AND SIGNALS
 104 WRITE (NTOUT,104)
 NGOR = 0
 C-----CALCULATE THE NUMBER OF TYPE POSITIONS PER LIST COLUMN
 105 FORMAT (120X)
 IPERC=IBLANK * IIN + IFPC + IPCC + IPHC
 C-----TEST IF LESS THAN TO BE MARKED BY SIGN ON PG
 106 IF (ISIGN) 107,107,108
 C-----CONTINUE...SET APPROPRIATE QUANTITIES
 107 CONTINUE
 108 CONTINUE
 109 IF (IPLLT=IBLANK) 111,110,111
 110 IFLLT = ICAB(3)
 111 IFLEX=IBLANK) 113,112,113
 112 IFLEX = ICAB(4)
 113 CONTINUE
 114 CONTINUE
 115 IPERC=IPERC + 1
 116 IF (ICAB(2) = ICAB(2))
 117 CONTINUE
 118 CONTINUE
 119 IF (IPLLT=IBLANK) 111,110,111
 120 IFLLT = ICAB(3)
 121 IFLEX=IBLANK) 113,112,113
 122 IFLEX = ICAB(4)
 123 CONTINUE
 124 CONTINUE
 125 IF (IPERC=IPERC + 1)
 126 CONTINUE
 127 CONTINUE
 128 IF (IPERC=IPERC + 1)
 129 CONTINUE
 130 CONTINUE
 131 CONTINUE
 132 CONTINUE
 133 CONTINUE
 134 CONTINUE
 135 CONTINUE
 136 CONTINUE
 137 CONTINUE
 138 CONTINUE
 139 CONTINUE
 140 CONTINUE
 141 CONTINUE
 142 CONTINUE
 143 CONTINUE
 144 CONTINUE
 145 CONTINUE
 146 CONTINUE
 147 CONTINUE
 148 CONTINUE
 149 CONTINUE
 150 CONTINUE
 151 CONTINUE
 152 CONTINUE
 153 CONTINUE
 154 CONTINUE
 155 IF (ISPAZ-3) 157,157,155
 156 IF (ISPAZ-3)
 157 CONTINUE
 C-----TEST THE NUMBER OF SHEETS PER PAGE THAT WILL BE REQUIRED
 158 CONTINUE
 C-----CALCULATE NUMBER OF SHEETS REQUIRED

C-----CALCULATE NUMBER OF SHEETS REQUIRED

C-----CALCULATE NUMBER OF SHEETS REQUIRED

C-----CALCULATE NUMBER OF SHEETS REQUIRED

C-----CALCULATE NUMBER OF SHEETS REQUIRED

C-----CALCULATE NUMBER OF SHEETS REQUIRED


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LSTF2900      ISGRKP=I
LSTF2910      ISRLR=3
LSTF2920      C---- IN A FINAL SET IF TRG HEADING ARRAY IX MAY LOOK AS FOLLOWS
LSTF2930      C IX(1)=28KX
LSTF2940      C IX(2)=BLANKS
LSTF2950      C IX(3)=BLANKS
LSTF2960      C IX(4)=EN
LSTF2970      C IX(5)=IHH
LSTF2980      C IX(6)=2HK,
LSTF2990      C IX(7)=2HK,
LSTF3000      C IX(8)=BLANKS
LSTF3010      C IX(9)=NX
LSTF3020      C IX(10)=BLANKS ICAR(12)=2HK,
LSTF3030      C IX(11)=IHN
LSTF3040      C IX(12)=ICAB(11)
LSTF3050      C IX(13)=ICAB(12)
LSTF3060      GO TO 421
LSTF3070      C-----IT MUST BE L
LSTF3080      412 ISETI=4
LSTF3090      ISETI=6
LSTF3100      ISGRHP=2
LSTF3110      ISGRKE=3
LSTF3120      ISGRLE=1
LSTF3130      C-----ICAB(15)=I, ICAB(14)=2H,L
LSTF3140      IX(15)= ICAB(13)
LSTF3150      IX(17)= ICAB(14)
LSTF3160      421 CONTINUE
LSTF3170      IF (ICAO) 451,451,425
LSTF3180      C-----INITIALIZE THE SCALE HAND TO I.0
LSTF3190      425 CONTINUE
LSTF3200      C-----IMPRESSION FROM TAPE
LSTF3210      451 ICONTINUE
LSTF3220      NP=I
LSTF3230      IFT=500
LSTF3240      C TOP OF PAGE
LSTF3250      4001 CONTINUE
LSTF3260      DB 4002 J=I, ITPTR
LSTF3270      IF(6LJ)--2
LSTF3280      4002 CONTINUE
LSTF3290      IF(6LJ) * + 1) = -2
LSTF3300      IFT=9559
LSTF3310      IFT=9599
LSTF3320      IFT=9599
LSTF3330      ICONT=0
LSTF3340      C-----TRF BF LMPH FOR STORING REFLECTIONS
LSTF3350      C-----DATA ON BINARY TAPE.....READ IT .
LSTF3360      4501 CONTINUE
LSTF3370      IF (IFT.LT.500)GO TO 4502
LSTF3380      IFT=0
LSTF3390      C-----FIND(NYAPE,6UFI6)
LSTF3400      4502 CONTINUE
LSTF3410      IF (IFT.GE.500)GO TO 4501
LSTF3420      IH = I6BUFI IFT+1)
LSTF3430      IF (IH.EQ.99) GO TO 4503
LSTF3440      IK = I6BUFI IFT+2)
LSTF3450      IL = I6BUFI IFT+3)
LSTF3460      IEL = I6BUFI(IFT+4)
LSTF3470      JCMOE = I6BUFI(IFT + 8)
LSTF3480      JCODE=JCMOE
LSTF3490      C-----REPLACE PHASE BY SIGNA(F9) SCALED BY FACTOR OF I.O.
LSTF3500      LSIG(ICOUNT)=LSIG(JCMOE)
LSTF3510      ALPFA*6UFI(IFT + 9)
LSTF3520      IPNS(ICOUNT)=ALPFA*SGSCAL *+5
LSTF3530      IFT=IFT + 10
LSTF3540      JCODE=JCMOE
LSTF3550      C-----REFL SIGN OF A TO FC
LSTF3560      66 TO 4532
LSTF3570      4531 REFL(ICOUNT) = SIGN(FC*FSCAL*+5,A)
LSTF3580      4532 CONTINUE
LSTF3590      JCODE=JCMOE
LSTF3600      C-----DO NOT PLACE SIGN OF A ON FC
LSTF3610      4530 CONTINUE
LSTF3620      IF(ICOUNT) = FC*FSCAL *+5
LSTF3630      66 TO 4532
LSTF3640      4531 REFL SIGN OF A TO FC
LSTF3650      4532 CONTINUE
LSTF3660      JCODE=JCMOE
LSTF3670      C-----REPLACE PHASE BY SIGNA(F9) SCALED BY FACTOR OF I.O.
LSTF3680      LSIG(ICOUNT)=LSIG(JCMOE)
LSTF3690      ALPFA*6UFI(IFT + 9)
LSTF3700      IPNS(ICOUNT)=ALPFA*SGSCAL *+5
LSTF3710      IFT=IFT + 10
LSTF3720      JCODE=JCMOE
LSTF3730      C-----REFL SIGN OF A TO FC
LSTF3740      66 TO 4532
LSTF3750      4521 REFL(ICOUNT) = SIGN(FC*FSCAL*+5,A)
LSTF3760      4522 CONTINUE
LSTF3770      4523 N666 = I
LSTF3780      ICONT = ICONT - I
LSTF3790      IREFL = IREFL - I
LSTF3800      ICONT = ICONT + ISPAZ
LSTF3810      ICONT = ICONT + ISPAZ/2 - ISPAZ
LSTF3820      IPI = IINO(2)
LSTF3830      IP2 = IIND(3)
LSTF3840      INDEX(1) = IIND(2)
LSTF3850      IP6(1) = -I
LSTF3860      IFC(1) = IINO(3)
LSTF3870      4525 CONTINUE
LSTF3880      C-----DATA
LSTF3890      IPRK(ICOUNT) = FC*FSCAL*+5
LSTF3900      INDEX(ICOUNT) = IINO(1)
LSTF3910      IPI SIGNC) 4530,4530,4531
LSTF3920      IPI SIGNC) 4530,4530,4531
LSTF3930      C-----DO NOT PLACE SIGN OF A ON FC
LSTF3940      4530 CONTINUE
LSTF3950      IFC(ICOUNT) = FC*FSCAL *+5
LSTF3960      66 TO 4532
LSTF3970      4531 REFL SIGN OF A TO FC
LSTF3980      4532 CONTINUE
LSTF3990      JCODE=JCMOE
LSTF4000      C-----REPLACE PHASE BY SIGNA(F9) SCALED BY FACTOR OF I.O.
LSTF4010      LSIG(ICOUNT)=LSIG(JCMOE)
LSTF4020      ALPFA*6UFI(IFT + 9)
LSTF4030      IPNS(ICOUNT)=ALPFA*SGSCAL *+5
LSTF4040      IFT=IFT + 10
LSTF4050      JCODE=JCMOE

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<p>17. KEY WORDS (six to twelve entries; alphabetical order; capitalize only the first letter of the first key word unless a proper name; separated by semicolons)</p> <p>Computer programs; contour plotting; constrained refinement; crystallographic calculations; Fourier section; Fourier synthesis; least squares.</p>			
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